0 00000															
0.0.0															
0.01															
											0	0.0			
								2.0	2.0		2			9.0	
										20		76			00
											<u> </u>	7 -			
								0.0			DEDA	TION	IS C	OPP	
										0	EUN	lion	v3 C	Unr.	
the state of the state of the															
		1	2	-	1000	_									_



The Conklin SAGD Project; The application of Simultaneous inversion to pre-stack gathers

• Ronald M. Weir *

• P. Geoph. (Alberta), Professional Geoscientist (Texas)





Contents

- Regional Setting
- Geological/ Geophysical Challenges
- Post Stack Seismic Inversion
- Pre Stack Seismic inversion
- Geological model without seismic.
- Results of the Pre Stack seismic Inversion
- The Potential reserve addition using The Pre Stack Inversion





Area of Alberta, South of Fort McMurray







Geological Cross Section







Korea National Oil Corporation



McMurray Outcrop







Australia Example, Estuary



Horizontal Well Pairs







SAGD Schematic







Project area Detail



• Appraisal Well: 140

Legend

Drilled 2009

Core Well

Project Area Lease

3D Seismic 2007

Drilled Before 2003 Drilled 2004 Drilled 2005 Drilled 2006 Drilled 2007

Ground Water Well Water Source Well

- Water Source Well: 12
- Ground Water Monitoring: 4
- 3D Seismic: 23km² (9 Sections)





3-D outline with well control



Harvest

Seismic Survey







Horizontal Program Plan With Seismic Cross Section







Core Showing Shale / Sand interface







Two Key Well Ties Initial well plan, Seismc cross section







07-12-







11-12







Shale plug defined by geomodeling, McMurray isopach.



Korea National Oil Corporation

General Seismic Correlation







11-12 and 04-13 stack comparison







Post stack (zero offset) equation

Post-stack seismic inversion

$$S_t = W_t * r_t$$

$$r_{Pi} = \frac{Z_{Pi+1} - Z_{Pi}}{Z_{Pi+1} + Z_{Pi}},$$

$$Z_{P_{i+1}} = Z_{P_i} \left[\frac{1 + r_{P_i}}{1 - r_{P_i}} \right]$$





Post stack inversion was not diagnostic of lithology in this case







P and S-Wave Velocities

This lead to two different types of velocities: *P-wave, or compressional wave velocity*, in which the direction of particle motion is in the same direction as the wave movement. *S-wave, or shear wave velocity*, in which the direction of particle motion is at right angles to the wave movement.







P and S-Wave Velocities

•Unlike density, *seismic velocity* involves the deformation of a rock as a function of time. As shown below, a cube of rock can be *compressed*, which changes its volume and shape or *sheared*, which changes its shape but not its volume.



After Goodway (CSEG Recorder 06/2001)





What causes the AVO Effect?



•The traces in a seismic gather reflect from the subsurface at increasing angles of incidence *q*. The first order approximation to the reflection coefficients as a function of angle is given by adding a second term to the zero-offset reflection coefficient: $R(\theta) = R_0 + B \sin^2 \theta$

B is a gradient term which produces the AVO effect. It is dependent on changes in density, ρ , P-wave velocity, V_P , and S-wave velocity, V_S .











Aki-Richards equation

We start with Fatti's version of the Aki-Richards' equation. This models reflection amplitude as a function of incident angle:

where:

$$\begin{bmatrix}
 R_{PP}(\theta) = c_1 R_P + c_2 R_S + c_3 R_D \\
 c_1 = 1 + \tan^2 \theta \\
 c_2 = -8\gamma^2 \sin^2 \theta \\
 c_3 = -\frac{1}{2} \tan^2 \theta + 2\gamma^2 \sin^2 \theta \\
 \gamma = \frac{V_S}{V}
 \end{bmatrix}
 \begin{bmatrix}
 R_P = \frac{1}{2} \left[\frac{\Delta V_P}{V_P} + \frac{\Delta \rho}{\rho} \right] \\
 R_S = \frac{1}{2} \left[\frac{\Delta V_S}{V_S} + \frac{\Delta \rho}{\rho} \right] \\
 R_D = \frac{\Delta \rho}{V_S}.
 \end{bmatrix}$$





Korea National Oil Corporation A problem with this equation is that the coefficients are not equal in size. This makes the solution for R_s and Density unstable at small angles:

$$c_{1} = 1 + \tan^{2} \theta$$

$$c_{2} = -8\gamma^{2} \sin^{2} \theta$$

$$c_{3} = -\frac{1}{2} \tan^{2} \theta + 2\gamma^{2} \sin^{2} \theta$$

$$\gamma = \frac{V_{s}}{V_{p}} = 0.5$$

$$\begin{array}{l} \theta = 30^{\circ} \\ \theta = 60^{\circ} \\ 1.330 \\ \theta = 60^{\circ} \\ 4.000 \\ -1.500 \\ -1.125 \end{array}$$

<u>Conclusion</u>: the direct solution can be unstable.





Transforming variables

Relationship of Variables

We want to use the fact that the basic variables, Z_P , Z_S , and ρ are related.

We start with two relationships which should hold for the background "wet" trend:

$$V_S/V_P = \gamma = \text{constant}$$

 $\rightarrow \ln(Z_S) = \ln(Z_P) + \ln(\gamma)$

Constant y

and:

$$\rho = aV_P^b$$

$$\rightarrow \ln(\rho) = \frac{b}{1+b}\ln(Z_P) + \frac{\ln(a)}{1+b}$$

Generalized Gardner





Transforming variables

Model constraints

Both these relationships lead us to the more general model for the background trend:

$$\ln(Z_S) = k \ln(Z_P) + k_c + \Delta L_S$$
$$\ln(\rho) = m \ln(Z_P) + m_c + \Delta L_D$$







The new equation

Normalised Equation

This changes Fatti's equation to:

$$\mathbf{R}(\theta) = \tilde{c}_1 W(\theta) DL_P + \tilde{c}_2 W(\theta) D\Delta L_S + c_3 W(\theta) D\Delta L_D$$

where:

$$\tilde{c}_{1} = (1/2)c_{1} + (1/2)kc_{2} + mc_{3}$$

$$\tilde{c}_{2} = (1/2)c_{2}$$

$$W(\theta) = \text{wavelet at angle } \theta$$

$$D = \text{Derivative operator}$$

$$L_{p} = \ln(Z_{p})$$











Processing Considerations

- The 3-D was reprocessed in 2011 using an AVO compliant flow.
- The data was normalized to the bin center using 5-C interpolation. This served to condition the data for AVO and removed the acquisition footprint.
- 72 Synthetic seismograms were used for the McMurray Surface correlation
- The McMurray top was picked on the seismic data using the well control, this was used to constrain the pre stack inversion.





Well:







W4/0 AVO Model

10-01 location used for inversion







Gathers used for inversion input







Near surface velocity inversion

AVO scaled stack







Beaver Hill Lake Time Structure







McMurray Time Structure







Clearwater Time Structure







Beaverhill Lake Depth Map







Prestack Inversion Output Before scaling







Clearwater B 83 AMP Inversion Time Slice







3-D Volume using density







07-12- W4 Inversion PS







11-12-













Horizontal plan







Shale Plug defined by seismic







Shale plug defined by geomodeling







Change of Trajectories using seismic and geomodeling







Reserve add using seismic and geomodeling







Benefits of 3-D

- Based on the mapping, the repositioning of the well added reserves
 - 400 m X 200 m X 35 m pay X 30 % porosity, using a 50 % recovery factor.
 - \sim .84 million cubic meters or 5.7 million barrels in place.
 - Depending on recovery factor and oil price, this alone adds 50 to 100 million in value to the project
- The seismic benefits the well planning by avoiding shale hazards and improving well positioning





Conclusion

- Post Stack inversion was not useful for this project, even when constrained by interpretation and well control.
- The Geomodel in itself cannot accurately predict the nature of shale channels, reserves may be left behind.
- Conventional Seismic interpretation is not useful in the differentiation of Sand and Shale in the McMurray formation in this area
- Pre stack inversion is very useful, careful attention must be paid to the colour scheme to bring out the correct level of detail. It combines geological and geophysical data to make a complete picture.
- There is a major value add in using Prestack inversion in the McMurrary.





References

SAGD Fundamentals – Application of core and outcrop analogues, geology, geophysics and geochemistry to oil sands recovery.

Strobl, R.S., Short course presentation, CSPG may 2011

Simultaneous inversion of pre-stack seismic data

Brian Russell, Dan Hampson, and Brad Bankhead CGG / Hampson-Russell Gary Boukall, Harvest Operations Corp.





Thanks to:

- Hampson Russell Software
- Black Gold Business Unit, Harvest Operations Corp.
- Beth Adams for the graphics and design
- Dave Wardlaw, Gary Boukal, Harvest Operations corp.
- Wayne Nowry, CGG



2100, 330-5th Avenue SW Calgary, Alberta, Canada T2P 0L4

Telephone: **403-265-1178** Fax: **403-265-3490** www.harvestenergy.ca

