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THE UNIVERSITY OF CALGARY

**Seismic interpretation of two possible meteorite impact craters: White
Valley, Saskatchewan and Purple Springs, Alberta**

by

Hans-Henrik Westbroek

A THESIS SUBMITTED TO THE FACULTY OF GRADUATE STUDIES IN PARTIAL
FULFILLMENT OF THE REQUIREMENTS FOR THE DEGREE OF
MASTER OF SCIENCE

DEPARTMENT OF GEOLOGY AND GEOPHYSICS

CALGARY, ALBERTA

DECEMBER, 1997

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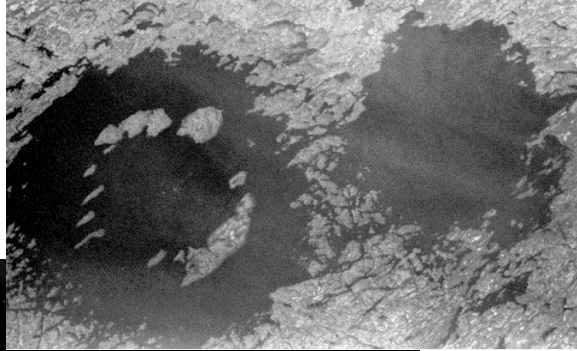
There is something fascinating about science. One gets such wholesale returns of conjecture on such a trifling investment of fact. — Mark Twain

Meteor Crater, U.S.A



D.J. Roddy

Clearwater Lakes Craters, Canada



NASA

END OF THE CRETACEOUS?



D. Davis



NASA

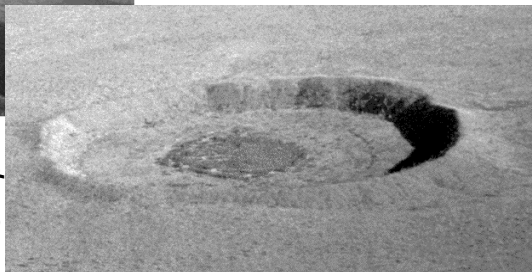
Manicouagan Crater, Canada



B. Robertson

New Quebec Crater, Canada

Wolfe Creek Crater, Australia



V.L. Sharpton

THE UNIVERSITY OF CALGARY

FACULTY OF GRADUATE STUDIES

The undersigned certify that they have read, and recommended to the Faculty of Graduate Studies for acceptance, a thesis entitled “Seismic interpretation of two possible meteorite impact craters: White Valley, Saskatchewan and Purple Springs, Alberta” submitted by Hans-Henrik Westbroek in partial fulfillment of the requirements for the degree of Master of Science.

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Abstract

High-velocity impact events have played a major role in the formation of the Solar System, including the Earth. The terrestrial record of impact structures shows over 150 examples, most of which are on the surface. This work uses the seismic reflection method to analyse sub-surface structures as possible meteorite impacts. I investigate two structures of possible meteorite impact origin: White Valley, Saskatchewan, and Purple Springs, Alberta. The impact hypothesis is evaluated by comparing structure geometry as seen on seismic reflection images with models (i.e., scaling criteria) derived from other known structures, laboratory experiments and numerical modelling.

The White Valley structure is most likely explained as a complex meteorite impact structure. It is some 7.5 km in diameter, with a nearly 2 km central uplift and is characterized by a terraced rim, a downdropped trough, and an uplifted center. The structure extends to a depth of 1300 m but the trough of the crater itself is only 100 to 220 m deep based on seismic data and scaling relationships. Structural uplift is estimated at 620 m, in good agreement with the scaling results. The gravity anomaly over the structure is consistent with the complex impact crater model. The structure is between about 55 and 60 Ma old.

The Purple Springs structure is also reasonably well described by scaling criteria for a complex impact crater. It is elliptical in nature, about 4 km long and 3 km wide. The structure is apparent in some 780 m of rock extending from the Mississippian to the Devonian Elk Point Group and is about 320 Ma old. The Mississippian shows about 180 m of downdrop into the structure in excellent agreement with scaling criteria. The rim of the structure is characterized by listric normal rim faults delineating terraces which drop to a relatively flat central plain. The lack of a prominent central uplift suggests post-impact processes may have substantially altered the structure to its current form.

Acknowledgements

This thesis represents the culmination of work which, as is often the case with such endeavours, could never have been completed without the assistance of many people. I would like to thank my supervisor, Rob Stewart, for his guidance throughout the course of this research and in particular, for giving me encouragement at the times when self motivation failed me. I would also like to thank Don Lawton for his time in discussing these structures and for sharing his work on the Eagle Butte impact crater with me.

For additional insight into the formation and character of these amazing structures, I would like to thank Richard Grieve and Alan Hildebrand, both of the Geological Survey of Canada, for many useful and insightful discussions.

Without appropriate data these projects would not be possible so I would like to thank Mark Resources Inc. and Enron Oil Ltd. of Calgary for their generous donation of the White Valley seismic data. Andy St. Onge was particularly helpful by helping me acquire the data and sharing his knowledge of the structure. Similarly, Norcen Resources Ltd. and Amoco Canada gave me the use of the Purple Springs dataset. I would like to thank Brad Nazar, from Norcen, for bringing the structure to my attention, and Wes Bader, also from Norcen, for his donation of time for many discussions we had about the structure and the geology of the area.

My thanks, also, to Henry Bland and Darren Foltinek of the CREWES Project at The University of Calgary for their technical support and many last minute miracles prior to (i.e., the night before) many important deadlines.

For generous financial support, I would like to thank the CREWES Project sponsors and the National Science and Engineering Research Council of Canada.

To my office mates, Chris Collom (Ph.D. Paleontology), Dave Thomas (M.Sc. Hydrogeology) and Andrew McRae (Ph.D. Paleontology), thanks for putting up with a “squiggle reader” and realizing that geophysics really *is* the more superior of the three disciplines. Finally, to Lynn Gillies, who patiently waited for me to get “that damn thesis” done, and to the many new friends I’ve made over the last few years: thanks so much for the great memories. It’s been one heck of a ride.

Dedication

This thesis is dedicated to the memory of Hendrik Westbroek, my mentor, my teacher, my friend and my father. It is also dedicated to Marijke, Wido, Reinout and Jiska, for their love and support throughout this endeavour.

Table of Contents

Approval Page.....	ii
Abstract.....	iii
Acknowledgements	iv
Dedication.....	vi
Table of Contents	vii
List of Tables.....	x
List of Figures.....	xi
 CHAPTER ONE - INTRODUCTION.....	 1
1.1 BACKGROUND.....	1
1.2 IMPACT MECHANICS.....	3
1.2.1 Contact and Compression Stage.....	4
1.2.2 Excavation Stage	6
1.2.3 Modification Stage	8
1.3 ECONOMIC POTENTIAL	12
1.3.1 Progenetic Deposits	13
1.3.2 Syngenetic Deposits	14
1.3.3 Epigenetic Deposits	15
1.3.3.1 Hydrothermal Ores.....	15
1.3.3.2 Chemical Sediments.....	16
1.3.3.3 Water Resources.....	16
1.3.3.4 Placer Deposits	16
1.3.3.5 Oil Shales.....	16
1.3.3.6 Hydrocarbon Accumulations.....	17
1.4 SEISMIC EXAMPLES OF TERRESTRIAL CRATERS.....	17
1.4.1 The Manson Impact Crater.....	18
1.4.2 The Sudbury Impact Crater	18
1.4.3 The Montagnais Impact Crater.....	19
1.4.4 The Mjølñir Impact Crater.....	19
1.4.5 The Haughton Impact Crater.....	20
1.4.6 The Red Wing Creek Impact Crater.....	20
1.4.7 The Eagle Butte Impact Crater	21
1.4.8 The James River Structure	21

1.4.9 The Viewfield Structure	21
1.4.10 The Hartney Structure	22
CHAPTER TWO - SCALING RELATIONSHIPS AND RESERVOIR	
POTENTIAL	43
2.1 SCALING RELATIONSHIPS	43
2.1.1 Transient Crater Scaling	44
2.1.2 Simple Crater Scaling	46
2.1.3 Complex Crater Scaling	48
2.2 RESERVOIR POTENTIAL	50
2.3 CONCLUSIONS	55
CHAPTER THREE - THE WHITE VALLEY STRUCTURE	62
3.1 GEOLOGICAL SETTING	62
3.1.1 Regional Geology	62
3.1.2 Geological Well Control	63
3.2 GEOPHYSICAL CHARACTERISTICS	64
3.2.1 Well Log Data	65
3.2.2 Well Log to Seismic Data Correlations	66
3.2.3 Seismic Data Interpretation	68
3.2.3.1 <i>Horizon Description</i>	69
3.2.3.2 <i>Time Structure</i>	70
3.2.3.3 <i>Gravity Anomaly</i>	70
3.2.3.4 <i>General Morphology</i>	74
3.3 DISCUSSION	75
3.3.1 Kimberlite Origin	75
3.3.2 Meteorite Impact Origin	78
3.4 CONCLUSIONS	81
CHAPTER FOUR - THE PURPLE SPRINGS STRUCTURE	100
4.1 GEOLOGICAL SETTING	100
4.1.1 Well Control	101
4.2 GEOPHYSICAL CHARACTERISTICS	102
4.2.1 Well Log to Seismic Data Correlations	103

4.2.2	Seismic Data Interpretation.....	104
4.2.2.1	<i>Horizon Description</i>	105
4.2.2.2	<i>Time Structure</i>	107
4.2.2.3	<i>General Morphology</i>	108
4.3	DISCUSSION	110
4.3.1	Meteorite Impact Origin	110
4.3.2	Dissolution Phenomena	113
4.4	CONCLUSIONS	115
CHAPTER FIVE -	CONCLUSIONS	132
5.1	INTRODUCTION	132
5.2	THE WHITE VALLEY STRUCTURE	133
5.3	THE PURPLE SPRINGS STRUCTURE	135
5.4	GENERAL COMMENTS AND FUTURE WORK	137
REFERENCES	139

List of Tables

Table 2.1 - Structural association of hydrocarbon accumulations	52
Table 3.1 - Survey acquisition parameters for White Valley	64
Table 3.2 - Basic processing flow for White Valley	65
Table 3.3 - Summary of measured and scaling equation results.....	81
Table 4.1 - Survey acquisition parameters for Purple Springs.....	103
Table 4.2 - Basic processing flow for Purple Springs.....	104
Table 4.3 - Summary of measured and scaling equation results.....	112

List of Figures

Figure 1.1 - World map of impact structures	24
Figure 1.2 - Contact and compression stage	25
Figure 1.3 - Energy partitioning during an impact event	26
Figure 1.4 - Near surface interference zone at an impact site	27
Figure 1.5 - Excavation flowfield	28
Figure 1.6 - Simple and complex crater morphologies	29
Figure 1.7 - Crater depth vs. rim diameter and the onset of the transition diameter	30
Figure 1.8 - Log-log plot of crater diameter vs. gravitational acceleration	31
Figure 1.9 - The Manson impact crater	32
Figure 1.10 - The Sudbury impact crater	33
Figure 1.11 - The Montagnais impact crater.....	34
Figure 1.12 - The Mjøltnir impact crater.....	35
Figure 1.13 - The Haughton impact crater.....	36
Figure 1.14 - The Red Wing Creek impact crater.....	37
Figure 1.15 - The James River structure.....	38
Figure 1.16 - Dip-azimuth map from the James River structure	39
Figure 1.17 - The Viewfield structure.....	40
Figure 1.18 - The Hartney structure.....	41
Figure 1.19 - Time structure map over the Hartney structure	42
Figure 2.1 - Crater dimensions used in scaling criteria	57
Figure 2.2 - Avak structure map showing gas field locations.....	58
Figure 2.3 - Steen River well map showing exploration targets.....	59
Figure 2.4 - Eagle Butte well map showing exploration targets	60
Figure 2.5 - Viewfield well map showing exploration targets	61
Figure 3.1 - Generalized stratigraphy of SW Saskatchewan.....	83
Figure 3.2 - Aerial photograph over the White Valley structure	84
Figure 3.3 - Base map of the White Valley area	85
Figure 3.4 - Shallow repeated zone in 07-07-010-23W3.....	86
Figure 3.5 - Middle repeated zone in 07-07-010-23W3	87
Figure 3.6 - Deepest repeated section in 07-07-010-23W3	88
Figure 3.7 - Comparison of edited 07-07 velocity log and regional velocity trend.....	89

Figure 3.8 - Correlation of 01-04-010-22W3 to seismic data.....	90
Figure 3.9 - Correlation of 04-01-011-24W3 to seismic data.....	91
Figure 3.10 - Correlation of 07-07-010-23W3 to seismic data	92
Figure 3.11 - Interpretation of seismic line WV-017.....	93
Figure 3.12 - Interpretation of seismic line WV-021.....	94
Figure 3.13 - Interpretation of seismic lines WV-011 and WV-016.....	95
Figure 3.14 - Time structure map of the Belly River reflector	96
Figure 3.15 - Bouguer gravity profile over the White Valley structure	97
Figure 3.16 - Schematic of a kimberlite pipe.....	98
Figure 3.17 - Diatreme emplacement as modelled by fluidization experiments.....	99
Figure 4.1 - Base map of the Purple Springs area.....	117
Figure 4.2 - Generalized stratigraphy of southern Alberta	118
Figure 4.3 - Cross section through the four wells (Datum = Sea Level)	119
Figure 4.4 - Correlation of 01-36-009-13W4 to seismic data.....	120
Figure 4.5 - Correlation of 06-04-011-14W4 to seismic data.....	121
Figure 4.6 - Correlation of 08-31-010-14W4 to seismic data.....	122
Figure 4.7 - Correlation of 04-32-010-14W4 to seismic data.....	123
Figure 4.8 - Seismic line ties.....	124
Figure 4.9 - Seismic line DBRR-1	125
Figure 4.10 - Seismic line DBRR-2.....	126
Figure 4.11 - Seismic line DBRR-3.....	127
Figure 4.12 - Interpretation of seismic line DBRR-1.....	128
Figure 4.13 - Interpretation of seismic line DBRR-2.....	129
Figure 4.14 - Interpretation of seismic line DBRR-3.....	130
Figure 4.15 - Schematic of the Purple Springs structure	131

CHAPTER 1 - INTRODUCTION

1.1 BACKGROUND

Collisions between astronomical bodies have been an integral process in the formation of the Solar System. It is likely that the planets formed through accretionary processes in the early solar nebula when relative bolide velocities were lower, preventing catastrophic collisions and allowing for the formation of the Sun and planets. Separation of components by density in the solar accretionary disk resulted in fractionation of planetary constituents; thus the inner terrestrial planets (Mercury, Venus, Earth and Mars) formed largely by the accretion of solid bodies while the outer planets (Jupiter, Saturn, Uranus and Neptune) have a greater gaseous component, although solid inner cores are believed to exist (Ruzmaikina et al., 1989; Wetherill, 1989).

In Earth's early history, bombardment of its surface was a major geological process. Evidence of this bombardment actually stems from observations of the Moon where a lack of geological and atmospheric processes have lessened erosion of impact craters. It seems highly unlikely that while the Moon was being impacted by objects, the Earth was left immune, especially when one considers Earth's larger mass and cross-section and thus its greater capacity to attract bolides. Over the course of Earth's history, however, more interplanetary debris has been effectively removed by the gravitational attraction of the planets, reducing current rates of impact for Earth to approximately 10^{-5}yr^{-1} for 0.5 km diameter Earth-crossing objects (Wetherill and Shoemaker, 1982).

Meteorites are thought to originate mainly from the asteroid belt, the ring of debris between the orbits of Jupiter and Mars, which marks the transition from the inner terrestrial planets to the giant planets beyond. The belt might have been the location where another planet formed had it not been for the prior formation of Jupiter and its resulting tidal effects in the region which prevent the asteroids from accreting into a planet (Wetherill, 1989). These perturbations, as well as interbelt collisions, can cause asteroids to be redirected along new trajectories which take them toward the Sun. In doing so, these asteroids have the potential for crossing Earth's orbit and colliding with it at high velocity.

Comets also pose a potential threat to Earth. Comets are thought to originate from two regions: the Oort cloud far outside the Solar System (possibly some 20000 to 100000 astronomical units (AU) from the Sun - one AU is the average distance between Earth and the Sun, or approximately 150 million kilometres), and the Kuiper Belt just beyond the orbit of Neptune (Levy, 1994). About 10% of comets which enter the Solar System have the potential to collide with Earth. Of these, 2% are long-period comets - those with parabolic orbits - and thus show large orbital velocities. Some investigators believe that cometary impacts may account for a substantial portion of terrestrial craters and that they may have brought water to the Earth's surface, critical to the development of life (Weissman, 1982). Some asteroids are believed to be the degassed remnants of comets. The recent collision of Shoemaker-Levy 9 with Jupiter in 1994, its fragments only some 1.5 km in diameter, demonstrates that the potential for collisions is real and that the damage done by such a collision would be catastrophic on Earth.

Over 150 craters have been discovered on Earth (Figure 1.1) composed largely of two basic forms: the relatively small simple crater (<2-4 km diameter) and the larger complex craters (Grieve, 1991; Pilkington and Grieve, 1992; Hodge, 1994). Some, such as the structures found at Vredefort, South Africa; Manicouagan, Quebec; Chicxulub, Mexico;

and Sudbury, Ontario may even be of the still larger multi-ring form. Impacts of this size are thought to disrupt surface processes enough to cause mass extinctions although this topic remains controversial (Tappan, 1982; Hildebrand et al., 1991). Regardless of their final morphology, these craters are the result of immense impact energy and the interactions between the projectile, the resulting shock wave and the target rocks. These interactions may have been instrumental in extinction events (Hildebrand et al., 1991) and can lead to the redistribution, formation and/or the concentration of various economically important mineral and hydrocarbon deposits (Masaitis, 1989). Historically, about 23% of known impacts are associated with economic deposits (Grieve and Masaitis, 1994).

1.2 IMPACT MECHANICS

Impact craters are the result of highly energetic collisions between meteoroids and Earth. The energy is due to the immense approach velocity of the meteoroid. The minimum approach velocity for an object striking Earth is Earth's escape velocity or 11.2 km/s (this corresponds to the velocity attained by an object which is at rest with respect to Earth at large distances from the Earth), while the maximum approach velocity of some 83 km/s results from a combination of Earth's escape velocity, heliocentric orbital velocity, and the object's velocity when it is just bound to the Sun at a distance of one AU from the Sun. However, an average impact velocity of about 20 km/s is reasonable. Thus a 500 m wide spherical asteroid is, in terms of energy, roughly equivalent to some 3.1×10^{20} J. By comparison, the atomic bomb dropped on Hiroshima was equivalent to some 6.3×10^{13} J. However, the analogy that a hypervelocity impact is equivalent to an explosion is not entirely correct. Instead, I will summarize this phenomenon from the point of view of three formative stages: the contact and compression stage, the excavation stage and the modification stage and how they impinge on the final crater form. These stages are discussed separately but may occur simultaneously with one stage beginning before the previous stage ends. They generally form a continuous process of crater formation. The

stages as they are presented here are largely a simplification of the work in Melosh (1989).

1.2.1 Contact and Compression Stage

Although the most likely incident angle for a meteorite striking the Earth's surface is 45° (Shoemaker, 1962), a vertically incident projectile is considered here for simplicity. Obliquity of the impact has the result of decreasing the energy coupling to the target and reducing the vertical component of the projectile's velocity. These types of impacts are important because they can lead to asymmetry in the final crater form. For example, the Manson impact structure in Iowa, U.S.A., shows a central uplift which is offset from the structure's geometric centre. This is thought to be due to the low incident angle of impact, estimated at 20-30° from the horizontal (Shultz and Anderson, 1996). Impacts below 10° will leave highly elliptical craters such as the structures associated with the Rio Cuarto crater field in north-central Argentina (Hodge, 1994; Melosh, 1989). Obliquity also plays an important role in the distribution of ejecta deposits. These phenomena have been seen with regard to Venusian craters where ejecta deposit patterns are linked to the incident angle and direction of impact (Schaber et al., 1992; Schultz, 1992). Nonetheless, most laboratory and numerical modelling experiments focus on vertical impacts and, for this stage, most of the basic characteristics are adequately represented by this model.

This stage begins when the leading edge of the projectile first strikes the surface of the target. The initial contact immediately forms a shock wave which propagates into the target as well as back into the projectile. The trailing edge of the projectile continues at its initial velocity. This stage is characterized by its short duration which is on the order of

$$\tau \approx \frac{D_p}{v_p \sin \theta}, \quad (1-1)$$

where τ is the time for this stage, D_p is the projectile diameter, v_p is the projectile velocity

and θ is the incident angle measured from the horizontal. Shock pressures may reach 50-100 GPa causing mineralogical phase changes and overcoming the material strength of the projectile causing it to flow hydrodynamically (Melosh, 1989; Grieve, 1991). The geometry at the contact between the projectile and the target surface is essentially a sphere striking a flat plate. Oblique convergence of the spherical surface results as the projectile continues to penetrate into the target. This creates a torus of extreme high pressure at the interface which leads to jetting of melted and vaporized material (Figure 1.2). Jet velocities can exceed the initial velocity of the projectile and thus jetted material may be ejected permanently from the planet. Jetting has been observed in laboratory experiments at velocities as low as 6 km/s.

The shock wave reaches the rear of the projectile and is reflected back towards the target as a strong rarefaction event. It is this rapid unloading that leads to surface spalling, melting and vaporization if the initial shock pressure is high enough. This rarefaction event travels faster than the shock wave because the projectile and target rocks through which it propagates are still under compression. It eventually overtakes and weakens the shock front. By the time of projectile unloading, the shock wave is propagating into the target as a hemisphere, isolated from the impact site by the rarefaction event. The projectile and some target rock have been largely vaporized by the unloading of the rarefaction event and the vapor plume expands back into the cavity. Contact, compression and final unloading of the projectile is largely completed within one projectile volume. At this point, the projectile's kinetic energy has been converted to internal energy of the projectile, the vapor cloud and target rocks (Melosh, 1989). For most impacts, the projectile is completely vaporized and melted during this stage, although this varies depending on the dynamics of the impact and the physical properties of the projectile.

1.2.2 Excavation Stage

The excavation stage is dominated by two processes: 1) the attenuation of the shock wave to a plastic wave and then an elastic wave and 2) the development of the excavation flow field and large scale movement of material (Melosh, 1989). The rate at which the shock wave weakens to an elastic wave determines the amount of melted or vaporized target material created. This rate decreases quickly such that melting and vaporization of target material usually occurs within 3-4 projectile diameters of the impact site with the mass of melt roughly equal to ten times the mass of vapor (Melosh, 1989). The projectile's kinetic energy is converted largely into internal energy of the projectile, the target and the vapor via the shock wave. Figure 1.3 summarizes the energy partitioning which takes place between the projectile and the target rocks. After the contact and compression stage, most of the projectile's kinetic energy manifests itself as internal energy of the target rocks.

Vapor expansion continues during the excavation stage. In a vacuum, the vapor cloud reduces to an expanding hemisphere traveling at tremendous velocities. A mean gas velocity of 10 km/s is possible for a 20 to 30 km/s impact (Melosh, 1989). The expanding gas can overcome solid ejecta and even crush or melt ejecta due to aerodynamic stress. In the presence of an atmosphere, the vapor plume rises, forming an expanding torus similar to the classic mushroom cloud effect produced by nuclear detonations. If the vapor cloud never equilibrates with the ambient atmosphere (in terms of vapor cloud pressure and temperature) then atmospheric blow-out is possible whereby the plume continues through the top of the atmosphere and into the relative vacuum beyond. This process has the potential to deposit fine solid and liquid material into the upper atmosphere and likely explains the deposition of tektites hundreds or even thousands of kilometres from the impact site.

The near surface adjacent to the expanding cavity is often termed the interference zone for it is here that the shock wave and rarefaction wave interact to produce reduced maximum pressures (Figure 1.4). The rarefaction event causes spalling along the surface, ejecting material at velocities which can exceed the escape velocity and are usually on the order of half the projectile velocity. These large spall velocities are essentially the result of the particle velocity doubling rule at a free surface. The particle velocity at the free surface is the sum of the particle velocity for the shock wave and the particle velocity of the rarefaction wave. Tensile fragmentation can continue to great depths resulting in a great deal of target rock brecciation (Melosh, 1989).

Perhaps the most important aspect of cratering mechanics, in terms of final gross morphology, is the initiation of the excavation flow field. The flow field itself is a result of the difference in particle velocities of the shock wave and rarefaction wave. It stems from the thermodynamics of the shock and rarefaction events. Shock is an irreversible process; it conserves mass, energy, and momentum but not entropy. Rarefaction is reversible in that it conserves mass, energy, momentum and entropy; it is also adiabatic (i.e. it conserves heat). The difference in entropy manifests itself as heat and a residual particle velocity. Anything which enhances the irreversibility of the shock process, such as porosity crushing, phase changes and plastic deformation, increases the residual particle velocity (Melosh, 1989).

The geometry of the flow field is much like that in the case of groundwater flow under a head gradient (Figure 1.5). Material flows through streamtubes defined by isobars. The velocity of this material slows as it moves through the divergent streamtubes until it leaves the surface at the same velocity as the material which preceded it in the same tube. Drag on the material from adjacent streamtubes, gravity and internal deformation all conspire to decrease the ejection velocity from deeper streamtubes, further from the impact site.

Eventually, the ejection velocity in a streamtube falls to zero thus defining the rim of the transient crater (Melosh, 1989). Material in still deeper streamtubes plastically deform and may raise the surface around the transient crater rim. The maximum depth obtained by the transient crater occurs when material in the axial streamtube stops moving. The diameter of the crater continues to grow resulting in the paraboloid shape of the transient crater. Depth-to-diameter ratios for the transient crater approximate 1/3. The ejected material generally comes from a depth only 1/3 to 1/2 the transient crater depth while the rest is displaced (Melosh, 1989). The excavation stage is essentially complete when subsurface motion ceases. It takes considerably longer than the contact and compression stage and is on the order of:

$$\tau \approx \left(\frac{D_{at}}{g} \right)^{\frac{1}{2}}, \quad (1-2)$$

where τ is the time for excavating a transient crater of diameter D_{at} , and g is the acceleration due to gravity.

1.2.3 Modification Stage

As its name implies, the transient crater is short-lived and modification begins to reshape it to a more gravitationally stable form. Ejecta set in motion during excavation and spalling may still be in motion during this stage. The result of the modification stage are two morphological forms of craters: simple and complex (Figure 1.6).

Simple craters are bowl-shaped, likened to a parabola of rotation (Melosh, 1989). Slumping of the transient crater walls leaves a lens of brecciated rock in the bottom of the crater also with a paraboloid shape. The final rims are left standing at near the angle of repose which is usually around 30° and also gravity independent (Melosh, 1989). Because of the slumping, the transient crater diameter widens to the final, post-modification

diameter, resulting in lower depth-to-diameter ratios. The breccia lens itself tends toward a particular stratification. The bottom is lined by melt rocks which are not displaced from the transient crater bottom by the excavation flow field. Melt rock on the walls of the transient crater are subject to shear as the transient crater grows. This results in some mixing of the melt rock with the brecciated material. Thus, immediately above the melt rock, primarily brecciated rock slides from the walls followed by the mixed melt rock and brecciated rock nearest the transient crater walls (Grieve et al., 1977). Slumping can occur at relatively high speeds (several 10s of m/s) and may cause mounding of slumped material near the center of the crater. This has been found at terrestrial craters such as Meteor Crater in Arizona. This phenomenon should not be confused with actual structural uplift that is observed in complex craters where material from beneath the transient crater is brought to surface.

Complex craters form after a specific transition diameter is reached by the transient crater (Figure 1.7). The onset of this transition diameter is often abrupt but varies under different gravitational fields and target rock types. In general, the transition diameter follows an inverse gravity dependence (Figure 1.8). For Earth, the simple to complex crater transitional diameter is about 2-4 km and is dependent on target rock properties (Pilkington and Grieve, 1992; Grieve and Pilkington, 1996). Nonetheless, transient craters which go on to become complex craters have similar aspect ratios as those which become simple craters. The final depth-to-diameter ratios for complex craters, after the modification stage is complete, is much smaller than that for simple craters (see Chapter 2). Central peaks demonstrate stratigraphic uplift comparable to transient crater depth. Study of complex craters has revealed that collapse of the transient crater incorporates a particular volume of material beyond the actual transient crater in which the strength of the target rocks range from zero at the transient crater to nominal. Croft (1981) names this volume the strength crater. The rim of the complex crater represents the point where the materials within the

strength crater have reached the tensile strength of the target rocks. The actual mechanics of central peak formation remains controversial and is the subject of ongoing research. Some postulated reasons for its occurrence, some of which have been successfully argued against, include layering, elastic rebound, vapor scouring, and gravitational slumping accompanied by pseudo-hydrodynamic flow (Melosh, 1989).

Layering in target rocks likely affects crater morphology, although there is currently a lack of understanding on this aspect of cratering mechanics. Laboratory experiments of impacts into a weak layer overlying a strong one suggests that morphology is sensitive to thickness of the weak layer and the relative strength differences between the layers. These morphological differences in simple lunar craters, which ranged from central mounds of unexcavated material, to flat floors when excavation is not powerful enough to remove the strong layer, to benches in the sides of the crater when the strong layer begins to be excavated, were used to successfully predict the regolith (unlithified material on the lunar surface) thickness (Melosh, 1989). However, these effects are restricted to transient crater diameters less than that required for complex craters.

Elastic rebound of the rocks at the bottom of the transient crater might produce some uplift, however, this fails to answer why uplifts do not form in simple craters where presumably elastic rebound should also occur. Deformation of rocks beneath the transient crater is plastic and is unlikely to result in a great deal of rebound in any event. Nonetheless, current evidence is inconclusive on the role elastic rebound might play in generating a central uplift.

Gas scouring occurs in explosive events when expanding gases leave an erosional remnant in the center of the crater. Such craters show no evidence of structural uplift and hence can not explain the central peak in complex craters.

It is therefore suspected that uplift is primarily a result of gravitational collapse, plastic deformation, and possibly the pseudo-hydrodynamic response of target rocks beneath the center of the transient crater. Melosh (1989) proposes that the debris beneath and adjacent to transient craters behaves much like a fluid due to their being subject to violent shaking and alternating, localized compression and rarefaction events. This allows for localized failure throughout the debris mass, where the rarefaction event overcomes the overburden stress, resulting in a net motion (Melosh, 1989). The driving force of these pressure fluctuations might be long-lived, random noise which is present after the main shock event. The dynamics of this process is beyond the scope of this paper, but the reader is referred to Melosh (1989) and references therein for further discussion on this topic. In short, regardless of the true mechanics, the transient crater collapses while its bottom is uplifted - this is known from direct study of impact craters. A secondary collapse of the central peak likely occurs before the final complex morphology is reached (Grieve and Pesonen, 1992).

Thus, the final result of transient crater modification is, in general, two crater morphologies. The simple crater is characterized by a brecciated lens of material in the bottom of the true crater caused by slumping of the transient crater walls. It is generally composed of highly brecciated and melted rocks with most of the shocked rock (~90%) remaining in the autochthonous zone beneath the breccia lens (Grieve and Pesonen, 1992). In contrast, the complex crater contains a central area where rocks from great depth have been structurally uplifted primarily by gravitational collapse of the transient crater. There is little melted debris in the central uplift and large scale fracturing dominates over brecciation. Listric, normal rim faults develop during collapse and terraces often form along the crater perimeter. Between the rim and central uplift, an annular moat is filled with brecciated debris which has a similar composition to the brecciated lens of simple craters.

1.3 ECONOMIC POTENTIAL

Impact craters on Earth have been linked to economic deposits of various materials due to a variety of impact-related processes. While materials in the vicinity of impact craters have been exploited for many decades, only recently has an inventory been made on the revenues generated by this exploitation. Historically, about 35 of the 150 known terrestrial impact craters, have been associated with economic deposits. Currently 17 (about 11%) are being actively exploited. The estimated annual revenues from these deposits are over \$12 billion (Grieve and Masaitis, 1994). This estimate is based largely on North American deposits (annual revenues \approx \$5 billion) and the gold and uranium ores of the Vredefort structure in South Africa, (annual revenues \approx \$7 billion) and does not include revenues generated from the extraction of building materials (e.g., cement and lime products at Ries, Germany \approx \$70 million per year) or from the generation of hydroelectric power (e.g. 4000 GWh/a from the reservoir at Manicouagan, Quebec \approx \$200 million per year).

In general, the economic potential for an impact crater relies on intensive and extensive factors (Masaitis, 1989). Intensive factors include the energy of the impact, the paleogeography at the time of impact and any endogenic processes which are triggered by the impact itself. Extensive factors include the composition of the target rocks, impactite and breccia, as well as the structure of geological formations at the impact site. However, deposits of materials formed in or around impact craters are divided among three categories: progenetic, syngenetic and epigenetic deposits (Masaitis, 1989). Progenetic deposits are those which originated strictly by endogenic, geological processes. In these cases, the impact has had the effect of redistributing the deposit allowing it to be more economically exploited. Syngenetic deposits are those which originate during or shortly after an impact event. These types of deposits are generally attributed to the direct deposition of energy into the target rocks causing mineralogical and physical phase changes. Epigenetic deposits

are formed after the impact and are generally attributed to hydrothermal alteration, formation of enclosed basins with isolated sedimentation, or the flow of fluids into structural traps associated with the crater. Grieve and Masaitis (1994) outline these types of deposits in detail and give specific examples of the more economically significant, a summary of which follows.

1.3.1 Progenetic Deposits

Deposits of this type include ores of iron, uranium and gold, and to a lesser extent, silica, ilmenite and bauxite. There are currently 7 craters associated with progenetic deposits of which the Vredefort structure in South Africa is the most spectacular. While many shock metamorphic features have been found at the site, its genesis remains controversial (Nicolaysen and Reimold, 1990; Grieve and Masaitis, 1994). Some 100 km southwest of Johannesburg, the 2 Ga old feature is estimated at 140 km wide with an original diameter of 300 km (Hodge, 1994). It is the site of the most extensive gold deposits in the world, having produced half the world's total gold output (40500 metric tons) worth some \$50 billion (Grieve and Masaitis, 1994). Associated with the gold ore are 136500 metric tons of uranium with an estimated value of \$4 billion. Mining of these two ores currently results in annual revenues of \$7 billion. Preservation of these deposits is attributed to structural lowering of the deposits within the annular ring adjacent to the central uplift, protecting them from the estimated 8 km of erosion which has taken place in the area (Grieve and Masaitis, 1994). The gold fields occur on the proximal and distal edges of the annular ring with respect to the central uplift and occur largely in the northwestern quadrant of the structure (Myers et al., 1990). Both the gold (found in fluvial fans or fan deltas structurally controlled by faults) and uranium (in the form of detrital uraninite) are derived from Archean granites and are thought to have been partially redistributed or remobilized by the impact event.

Carswell, Saskatchewan, is about 130 km south of Uranium City, and is the site of another progenetic deposit of uranium ore. The structure has a post-erosional diameter of 39 km and is about 115 Ma old (Hodge, 1994). The ores are thought to be a result of hydrothermal activity about 1.1 Ga ago. Two kilometres of structural uplift associated with the center of the structure, brought these deposits nearer to the surface allowing for easier exploitation. An estimated 46500 metric tons of uranium ore (perhaps a billion dollars worth) reside in the deposit (Grieve and Masaitis, 1994).

1.3.2 Syngenetic deposits

Copper-nickel ores, Platinum group metals (PGMs), impact diamonds and glass are associated with deposits formed during or shortly after an impact event. While impact diamonds are not currently exploited, they are mentioned here because of their interesting physical characteristics. Impact diamonds, formed from the phase transformation of graphite or crystallized from coal, are harder and more physically resistive than normal diamonds formed at depth, possibly making them useful for industrial applications (Grieve and Masaitis, 1994). They are irregularly distributed in minor amounts, usually associated with melt dikes and suevite. Shock pressures over 30 GPa are required for impact diamonds to form, a value easily reached during meteorite impact events (Melosh, 1989). They have been found at several impact craters including Ries (Germany), Kara (Russia), Puchezh-Katunki (Russia), Ternovka (Russia), Zapadnaya (Ukraine) and others (Grieve and Masaitis, 1994; Hodge, 1994).

The most important syngenetic deposits occur at the Sudbury structure in Ontario. The Sudbury structure, of which the ore-bearing Sudbury Igneous Complex (SIC) is but one part, is an elliptical structure some 15000 km² in area with major axis trending NE-SW. It is estimated to have had an original diameter of 200-250 km with NW-SE shortening

caused by the Penokean orogeny shortly after the impact event (1.85 Ga). Inside the structure, the SIC contains rich Cu-Ni and PGM deposits. Extraction of the 15 million tons of nickel and copper has resulted in annual average revenues of \$2 billion over the last five years (Grieve and Masaitis, 1994; Hodge, 1994). The ore bodies are generally located along the basal edge or below the SIC, which represents the impact melt sheet in a current interpretation (Grieve and Masaitis, 1994). This interpretation deviates from previous ones in that it suggests that the metals were crustal in origin and that the variable composition of the impact melt was due to the variety of lithologies that were incorporated into the melt. Thus the SIC did not require magmatic sources (either triggered by the impact or purely endogenic) to reach a composition conducive to the formation of the ore bodies.

1.3.3 Epigenetic Deposit

Epigenetic deposits are the most common form associated with impact craters and include hydrothermal ores, chemical sediments, fresh water, oil shales and hydrocarbons.

1.3.3.1 Hydrothermal Ores

Hydrothermal ores are partially syngenetic in nature as they usually require a thermal driving force which can be attributed directly to the impact itself. Because of the immense deposition of heat into the target rocks by the impacting bolide and low thermal diffusivity of the rocks ($\kappa \approx 10^{-6} \text{ m}^2/\text{s}$), deeply buried melt in the breccia lens may take thousands of years to cool (on the order of H^2/κ for apparent crater depth H), forming a long-term thermal reservoir. It is possible that early bombardment of Earth may have contributed significantly to the surface's thermal budget as well as contributed significantly to hydrothermal systems (Melosh, 1989). Pb, Zn and Ag are common ores of this type found at the Siljan (Sweden), Crooked Creek (U.S.A.), Serpent Mound (U.S.A.) and Decaturville (U.S.A.) structures which have been mined. At Sudbury, the basal Vermillion member of the Onwatin formation lies above the suevite layer (Onaping formation) and is

estimated to contain 6 million tons of 4.4% Zn, 1.4% Cu, 1.2% Pb as well as some gold and arsenic. Unfortunately, the fine-grained texture of the deposit makes current attempts at recovery impossible (Grieve and Masaitis, 1994).

1.3.3.2 Chemical Sediments

Chemical sediments and evaporites form in the isolated basins created by water-filled impact craters occurring in warmer climates. Anhydrite, gypsum, lignite, bentonite, various carbonates, bicarbonates and chlorides are currently being exploited at Lonar, India and Saltpan, South Africa although it is unclear what revenues this activity generates (Grieve and Masaitis, 1994).

1.3.3.3 Water Resources

As well as providing a surface catchment basin, structural and lithologic changes in the subsurface caused by the processes of impact cratering can affect groundwater quality and enhance aquifer characteristics. Such a case exists at the 35 km wide Manson crater in the U.S.A. where unusually soft groundwater was discovered when the Manson city well was drilled. This later was found to be because of crystalline rocks that had been structurally raised in the central uplift (Hodge, 1994).

1.3.3.4 Placer Deposits

A particular deposit associated with terrestrial craters are placers formed by Earth's erosional processes. Moldavite tektite placers (used for jewelry) as well as placer diamonds have been found. Placer deposits are often distal to the impact site such as the placer diamonds from Popigay, Russia which are found 150 km distant (Grieve and Masaitis, 1994).

1.3.3.5 Oil Shales

The impact craters at Boltysh (25 km wide, 88 Ma), Obolon (15 km wide, 215 Ma) and Rotmistrovka (2.7 km wide, 140 Ma), all in the Ukraine, contain oil shales equal to some 90 million barrels of unmaturred oil. Boltysh alone contains 4.5 billion metric tons of oil shale in a 400-500 m thick productive sequence which lies over the trough and central

uplift (Grieve and Masaitis, 1994). Evidently, these impact craters formed isolated basins in which algae and plant activity thrived, providing the biogenic mass for development of the oil shales.

1.3.3.6 Hydrocarbon Accumulations

The structural facies associated with impact craters makes them potential traps for migrating hydrocarbons. Analogous to the development of oil shales, impact craters can result in the formation of source rocks as well (Castaño et al., 1995). Thus, hydrocarbon reservoirs of this nature do not necessarily have to develop in traditional basin-type regions. The Ames structure in Oklahoma is one of the most prolific hydrocarbon producers of all impact craters and an example of a crater providing both the isolated basin in which the source rocks formed as well as the structural traps in which the hydrocarbons accumulated. The simple Newporte crater in North Dakota is a similar case where source oil shales are localized in the crater. In general meteorite impact craters can provide unique, localized, structural traps and enhanced reservoir rock characteristics due to brecciation and fracturing of target rocks as well as displacement of large, competent blocks of rock during the modification stage of crater formation. The structures become prospective when they lie in the path of migrating hydrocarbons. The estimated total reserves of hydrocarbon deposits, largely from four impact structures (Ames, Red Wing Creek, Avak, and Viewfield) include some 140 million barrels of oil and nearly 200 billion cubic feet of gas. The structural association of these deposits are discussed in more detail in Chapter 2.

1.4 SEISMIC EXAMPLES OF TERRESTRIAL CRATERS

The primary goal of this work is to investigate the usefulness of seismic reflection data as a tool for recognizing buried meteorite impact craters. Specifically, two seismic interpretation case studies (the structures at White Valley, Saskatchewan and Purple Springs, Alberta) are studied in detail in Chapters 3 and 4. However, it is useful to review other structures in the literature, both proven and possible impact craters, which have been

studied using seismic methods. The following is a brief summary of the seismic interpretations of a few of these structures.

1.4.1 The Manson Impact Crater

The Manson structure is located in northwest Iowa and is the largest known impact crater in the U.S.A. It has been extensively studied (e.g., Koeberl and Anderson, 1996 and references therein). Investigation of the site by seismic reflection methods does not appear extensive; the bulk of the work is petrologic and geochemical in nature. Nonetheless, some seismic work has been recently completed in the last few years with the acquisition of high-resolution vibrator data (Kieswetter et al., 1996 and references therein). High-resolution vibrator seismic data were acquired along a radial line which primarily images the terraced rim on the eastern portion of the structure (Figure 1.9). The final interpretation based on seismic data and deep well data shows terracing of the rim towards the crater center with a distinct thickening of sediments in the center of the terraces, an area also characterized by an overturned sequence (Figure 1.9). Only a short portion of the annular trough is imaged in the western extremity of the seismic line.

1.4.2 The Sudbury Impact Crater

The Sudbury structure has already been described as the site of the world's richest copper-nickel deposits. Although its history is complex, the discovery of several shock metamorphic effects leave little doubt that a large meteorite impact was involved in its genesis (Grieve et al., 1991). In fact, some interpretations suggest that no endogenic processes are required at all to produce the structure and resulting ore bodies (Grieve and Masaitis, 1994). Despite apparent post-impact deformation, the main crater basin, thought to have contained much of the impact melt, can still be seismically imaged (Figure 1.10). While details of the crater structure are not imaged, and may no longer be present, the high-resolution Lithoprobe seismic line does show the main crater basin and its relation to

structural elements associated with the Penokean orogeny (Wu et al., 1994).

1.4.3 The Montagnais Impact Crater

The Montagnais structure, also a proven impact crater, is unique in that it was the first submarine impact crater found (Jansa et al., 1989). Approximately 200 km south of Halifax, Nova Scotia, it lies on the edge of the Scotian shelf in about 110 m of water. Melt rocks, breccia and shock-induced features all point to an impact origin. The structure itself is 45 km wide and extends to a depth of 2.7 km beneath 500 m of Tertiary and Quaternary marine sediments (Jansa et al., 1989). The central uplift region is extensive; its diameter is 11.5 km wide with a central basin 3.5 km wide composed largely of basement rocks. Such “peak-ring” structures are common on other planetary surfaces (Melosh, 1989) and are thought to be a normal progression from the smaller central peak structures to the enormous multi-ring structures (e.g. Vredefort, South Africa, Chicxulub, Mexico, and Manicouagan, Quebec are suspected of being terrestrial multi-ring craters). The interpreted seismic data (Figure 1.11) shows some 1250 m of structural uplift. Another 552 m of breccia overlies the central uplift. This draping of breccia over the central uplift is an unusual feature of Montagnais; Jansa et al. (1989) suggest it may be a particular result of marine impact processes.

1.4.4 The Mjølner Impact Crater

The Mjølner structure is located in the central Barents Sea to the north of Scandinavia and Russia in 350-400 m of water. It has only recently been identified as a meteorite impact crater by the discovery of shock metamorphic features and an iridium anomaly (Dypvik et al., 1996). Disrupting some 3.6 km of Mesozoic sediment, the structure is 40 km in diameter showing many of the morphological features of a complex crater including an annular moat and central uplift (Figure 1.12). Study of what is interpreted to be the ejecta deposits suggests an age of impact in the late Jurassic to Early Cretaceous (Dypvik et al.,

1996). This feature is also somewhat unique as it represents only the fourth proven submarine impact crater (Montagnais, Nova Scotia; Chicxulub, Mexico; and Chesapeake Bay, Virginia are the other three structures).

1.4.5 The Haughton Impact Crater

Seismic reflection imaging was used to delineate the western flank of the Haughton impact crater (Hajnal et al., 1988). The structure is located in the Canadian Arctic on Devon Island just north of Baffin Island (75°22'N, 89°41'W). The structure is 20 km in diameter and relatively young at 21 Ma., but it disrupts the entire 1700 m sequence of gently westward dipping Paleozoic rocks plus some crystalline basement (Hajnal et al., 1988; Hodge, 1994). The radial seismic line (Figure 1.13) shows many of the terraces delineated by normal faults along the rim. These faults appear to be listric - slowly curving towards the center of the structure - and transecting most of the Paleozoic. Listric rim faults are characteristic of many complex impact craters.

1.4.6 The Red Wing Creek Impact Crater

The Red Wing Creek structure is another important buried structure in terms of hydrocarbon accumulation (see Chapter 2). It is located in west-central North Dakota (47°36'N, 103°33'W) is 9 km in diameter and about 200 Ma old (Hodge, 1994). The unmigrated seismic data (Figure 1.14) clearly shows a raised rim, followed by a syncline, before the 3 km wide central uplift is reached (Brenan et al., 1975). The syncline and rim are again encountered further along the line past the uplift. The large “bowtie” features seen beneath the troughs are classic artifacts seen on stacked seismic data from the scattering of energy off the dipping sides of synclines. Migrating the seismic data with the correct velocities would minimize this effect and help to image the structure more clearly. Note also the pull-up seen along the Ow horizon. This is characteristic of many complex craters in sedimentary settings where the maximum depth of the structure does not reach

basement (see the White Valley structure in Chapter 3).

1.4.7 The Eagle Butte Impact Crater

The Eagle Butte impact crater is located in southeastern Alberta. It is a complex crater about 18 km in diameter with structural uplift at its core of some 250-300 m (Sawatzky, 1976). Its impact origin has been proved by the discovery of shatter cones at the surface (Lawton et al., 1993; Hodge, 1994). An area of active hydrocarbon exploration, it has been extensively covered by seismic acquisition lines and the structure has been drilled in a number of localities. To date, a few gas accumulations have been found associated with the structure.

1.4.8 The James River Structure

James River is a structural anomaly consistent with complex crater morphology seen on 3-D seismic data (Figure 1.15). Buried nearly 4 km deep and truncated by an erosional unconformity at the top of the Cambrian, it is imaged clearly along the Cambrian A reflector as a nearly 5 km wide circular structure with an annular moat and central uplift (Isaac and Stewart, 1993). Figure 1.16 illustrates a dip-azimuth map of the structure which highlights the annular trough and terracing along the crater walls. Of particular exploration interest, these terraces that occur along the walls of complex craters result in large blocks of competent rock being displaced and forming structural traps. Such a case exists at the gas fields of the Avak structure mentioned earlier.

1.4.9 The Viewfield Structure

This structure is located in southeastern Saskatchewan and is important for its structural influence on hydrocarbon deposits in the area (see Chapter 2). Hydrocarbon accumulations are predominantly from the rim of the structure (Isaac and Stewart, 1993). The circular structure is about 2.4 km wide and appears to have the morphology of a simple crater

(Figure 1.17). The structural history is a complex one with interpretations invoking both a meteorite impact as well as salt dissolution (Sawatzky, 1972). Sawatzky (1972) suggests, though, that the structural deformation created initially by an impact controlled subsequent dissolution events. The seismic data for the Jurassic or Triassic aged structure shows the typical synclinal cross-section of simple craters including a raised rim (Figure 1.17). The Jurassic horizon may even show infill at the center of the structure perhaps due to post-impact sedimentation. Nonetheless, the lack of evidence for shock metamorphism has prevented this structure from being accepted as being the result of a meteorite impact.

1.4.10 The Hartney Structure

The Hartney structure is located in southwest Manitoba (approx. 49°N, 100°30'W) and was discovered as a result of hydrocarbon exploration (Anderson, 1980). The structure is about 8 km in diameter. Seismic data acquired over the anomaly shows structural disruption from the Winnipeg shales (Ordovician in age) to the Lower Cretaceous Blairmore formation (Figure 1.18). Although the diameter of the structure falls within the regime for complex morphology, it appears that the center of the structure is a structural low surrounded by a ring anticline and subsequent syncline (see Winnipeg shale horizon, Figure 1.19). While “peak-ring” morphologies are possible, this structure is probably too small for such development. On the other hand, near the center of the anomaly, drilling results have shown structurally uplifted Devonian strata and a complete absence of Mississippian strata (Anderson, 1980). Conversion to depth was accomplished by a velocity model based on interval velocities from well data. This resulted in the Winnipeg shale structure map showing a central uplifted high (Figure 1.19). Perhaps the apparent low in the Winnipeg shale was due to a velocity anomaly. The structure apparently fits some of the morphological constraints of a complex meteorite impact crater, (e.g. a central uplift region) although they may not be as obvious as in many of the previous examples. This structure is a good example of how difficult it can be to make suppositions on genesis

based on morphology alone. Furthermore, a lack of shock metamorphism leaves this structure classified as a possible impact crater only.

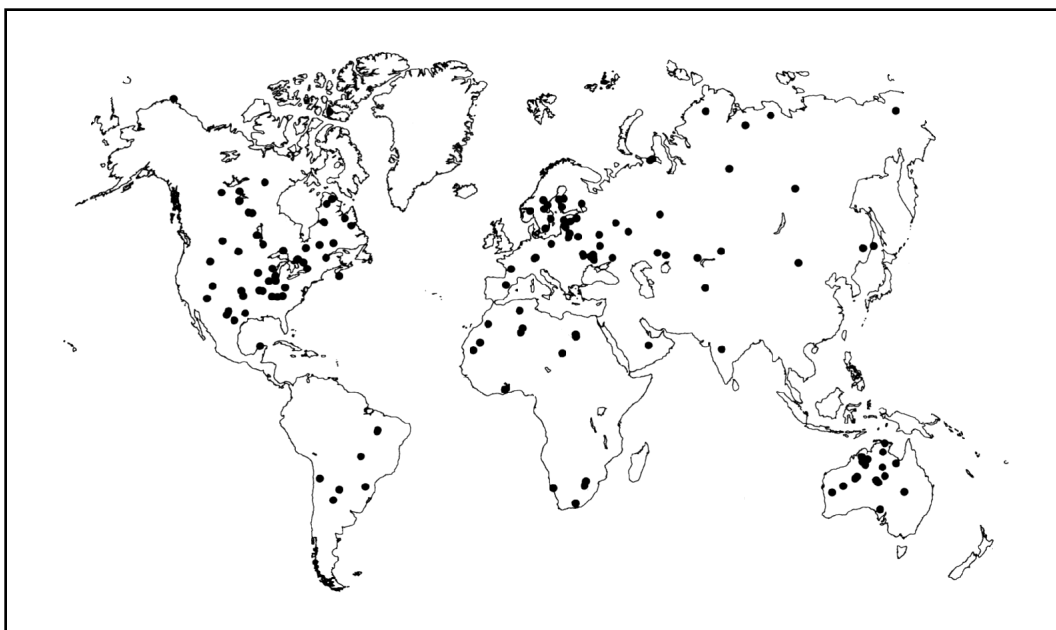


Fig. 1.1 World map showing the distribution of currently known meteorite impact craters. Data courtesy of the Geological Survey of Canada.

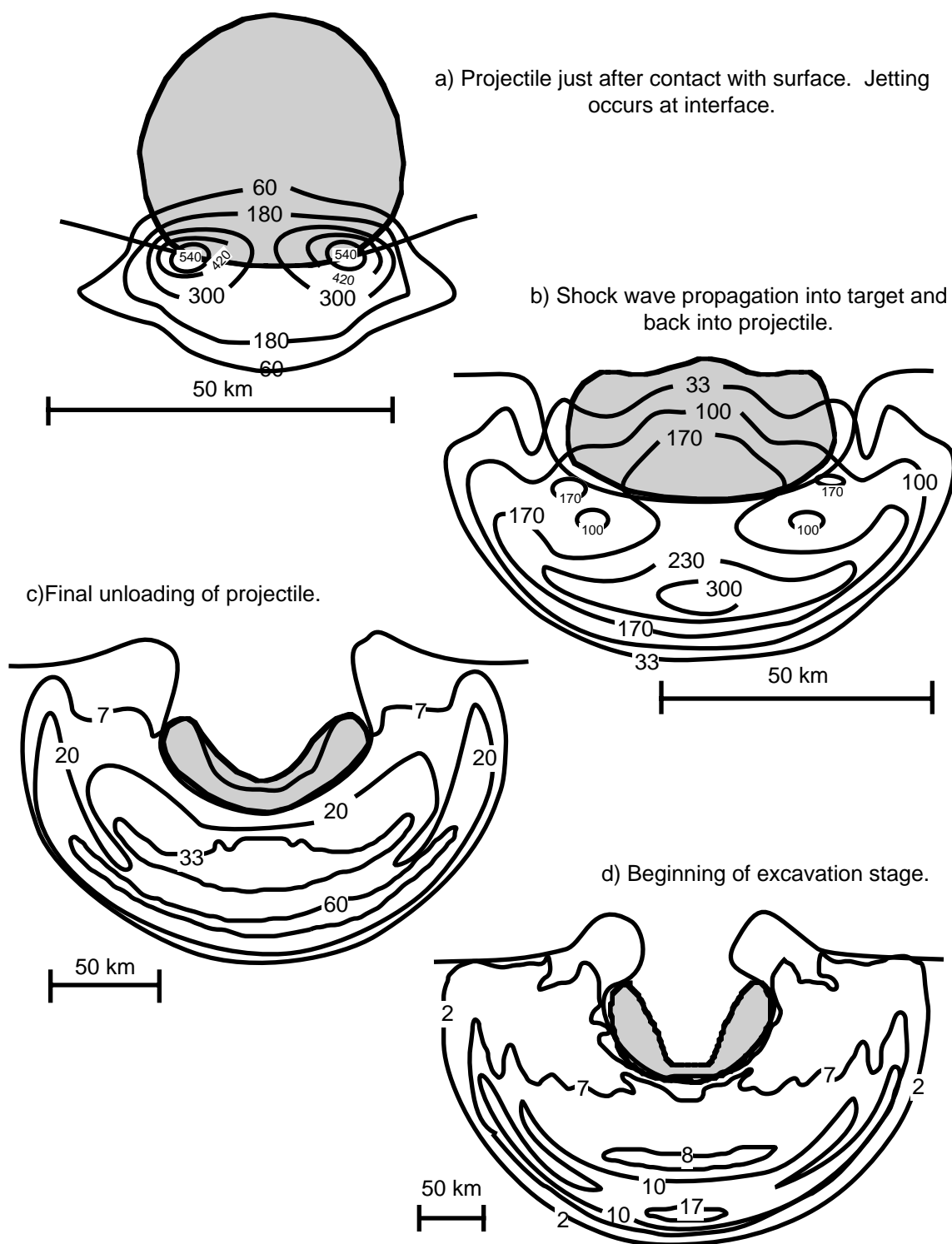


Fig. 1.2. Schematic representation of the contact and compression stage based on numerical modelling. Depicted are the deformation of the projectile and the resulting pressure field in GPa. Note the changing scale in each diagram (from O'Keefe and Ahrens, 1975; Melosh, 1989).

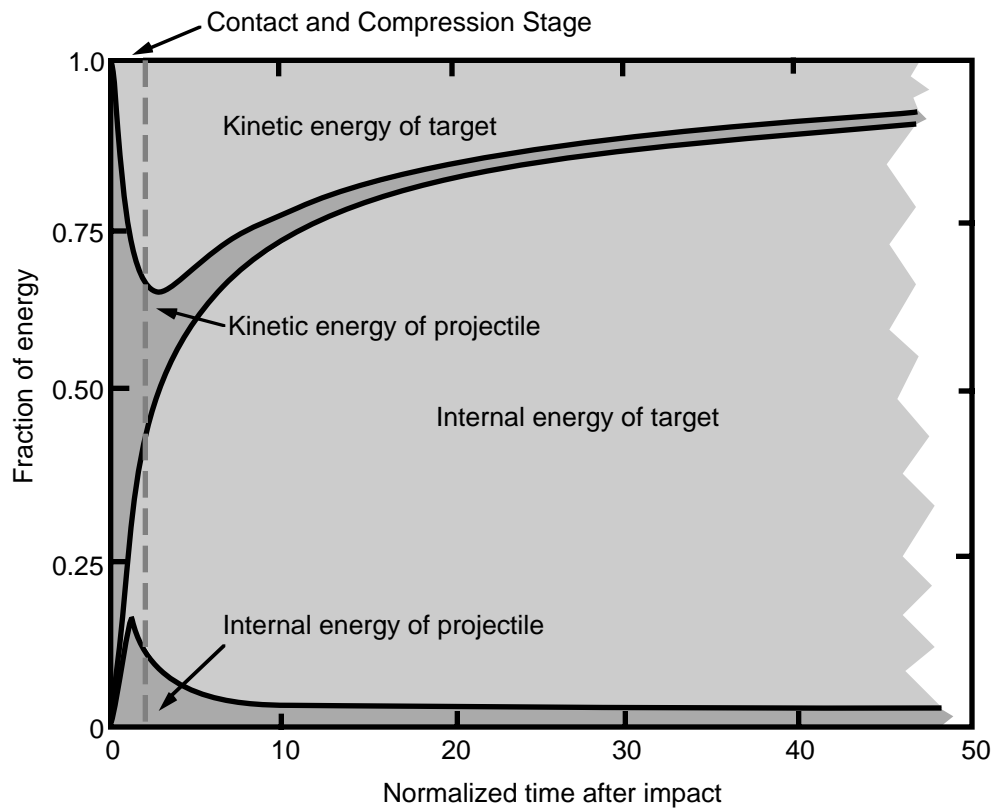


Fig. 1.3 Graph of energy versus time for an impact event. Initially, the projectile contains 100% of the available energy as kinetic energy (at $t=0$). This is then quickly partitioned between the kinetic and internal energy of the target rocks (light grey) and residual kinetic and internal energy of the projectile (dark grey) in the event any of the projectile survives the impact (from Melosh, 1989).

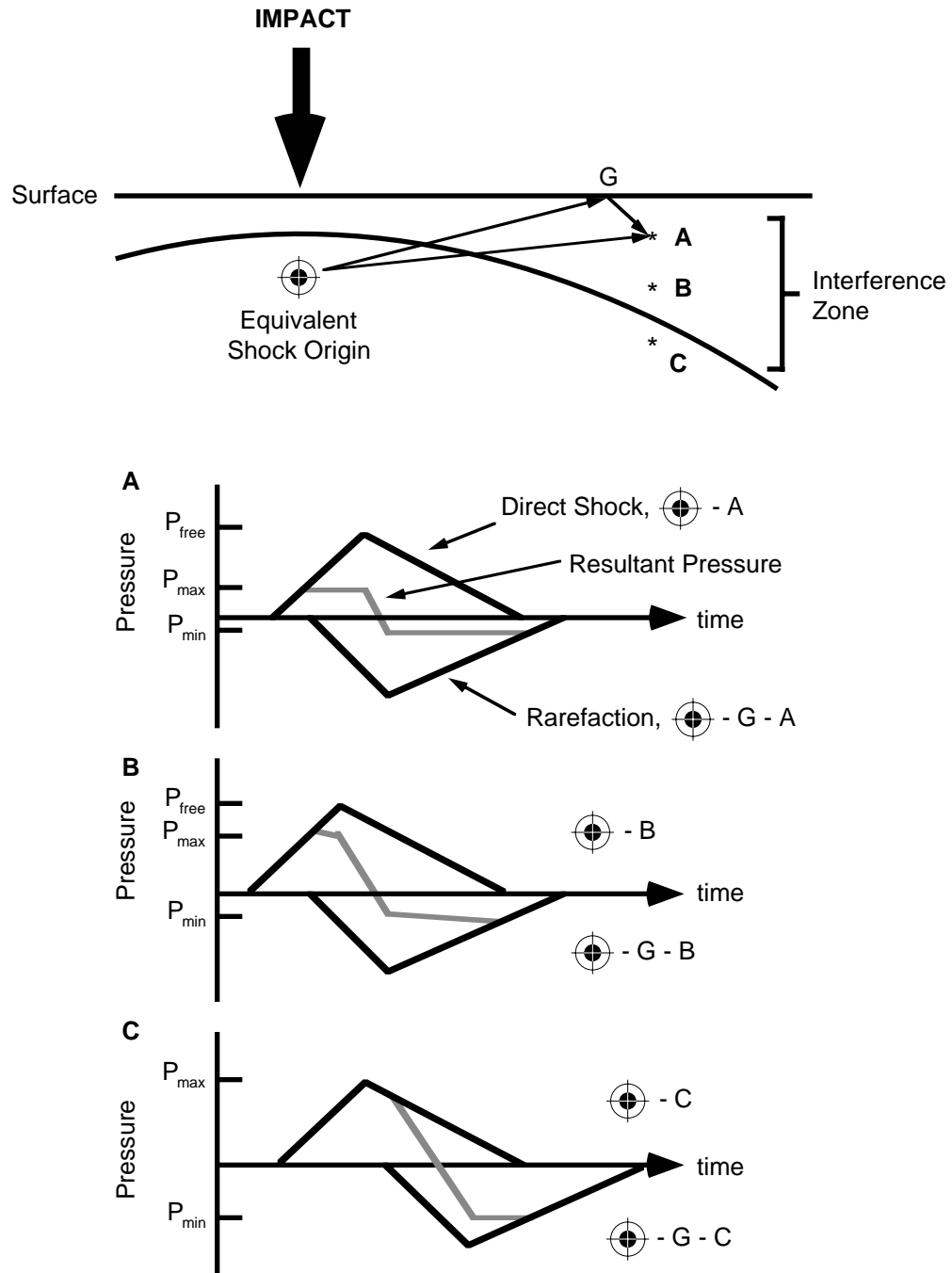


Fig. 1.4 Schematic depiction of the near surface interference zone at an impact site. The pressure-vs.-time graphs show the shock pressure and rarefaction pressure at subsurface points A,B, and C, respectively. Note that the rarefaction event is a result of the reflection of the shock wave off of the surface at G. The resultant pressure is shown in the graphs by the grey line (from Melosh, 1989).

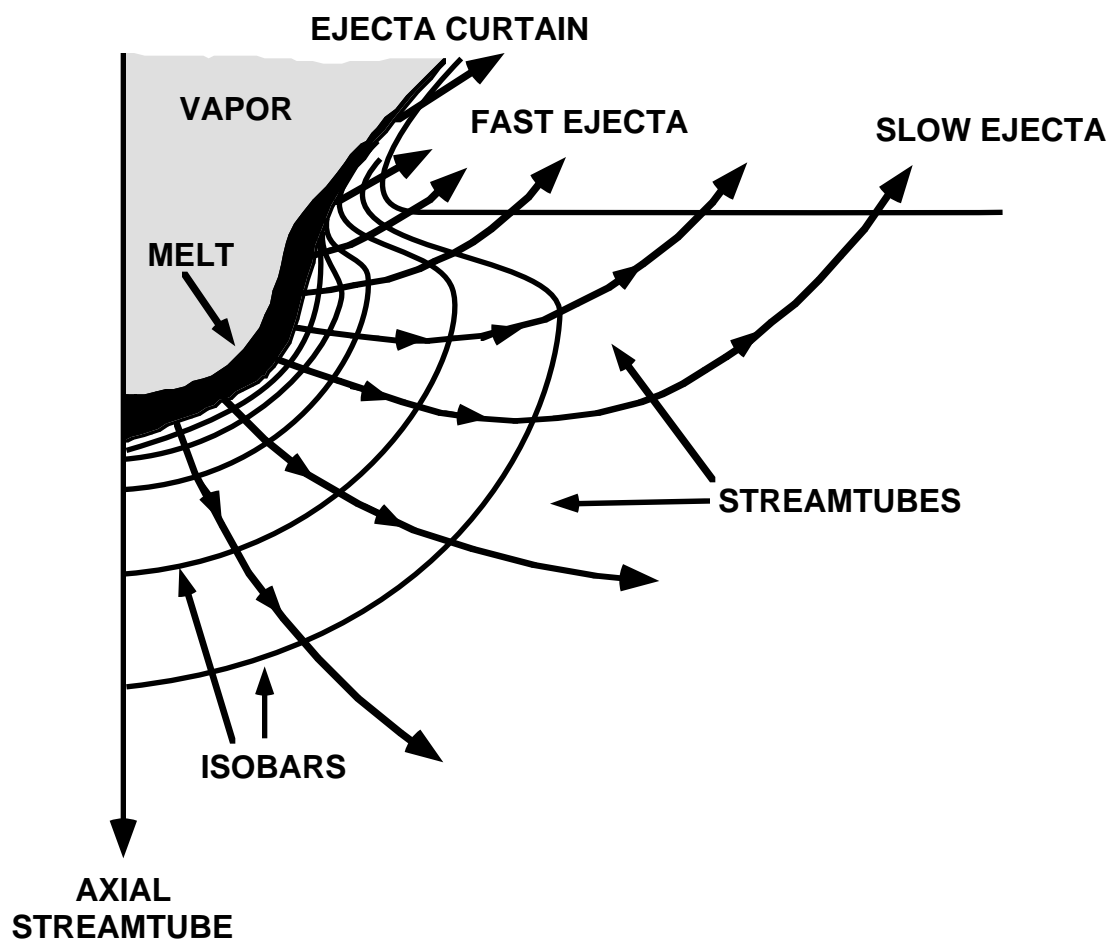


Fig. 1.5 Depiction of the excavation flowfield as a series of isobars intersected at right-angles to the streamtubes. It is through the streamtubes that the target material flows. Where this material breaks the surface, ejecta is ballistically thrown from the impact site (from Melosh, 1989).

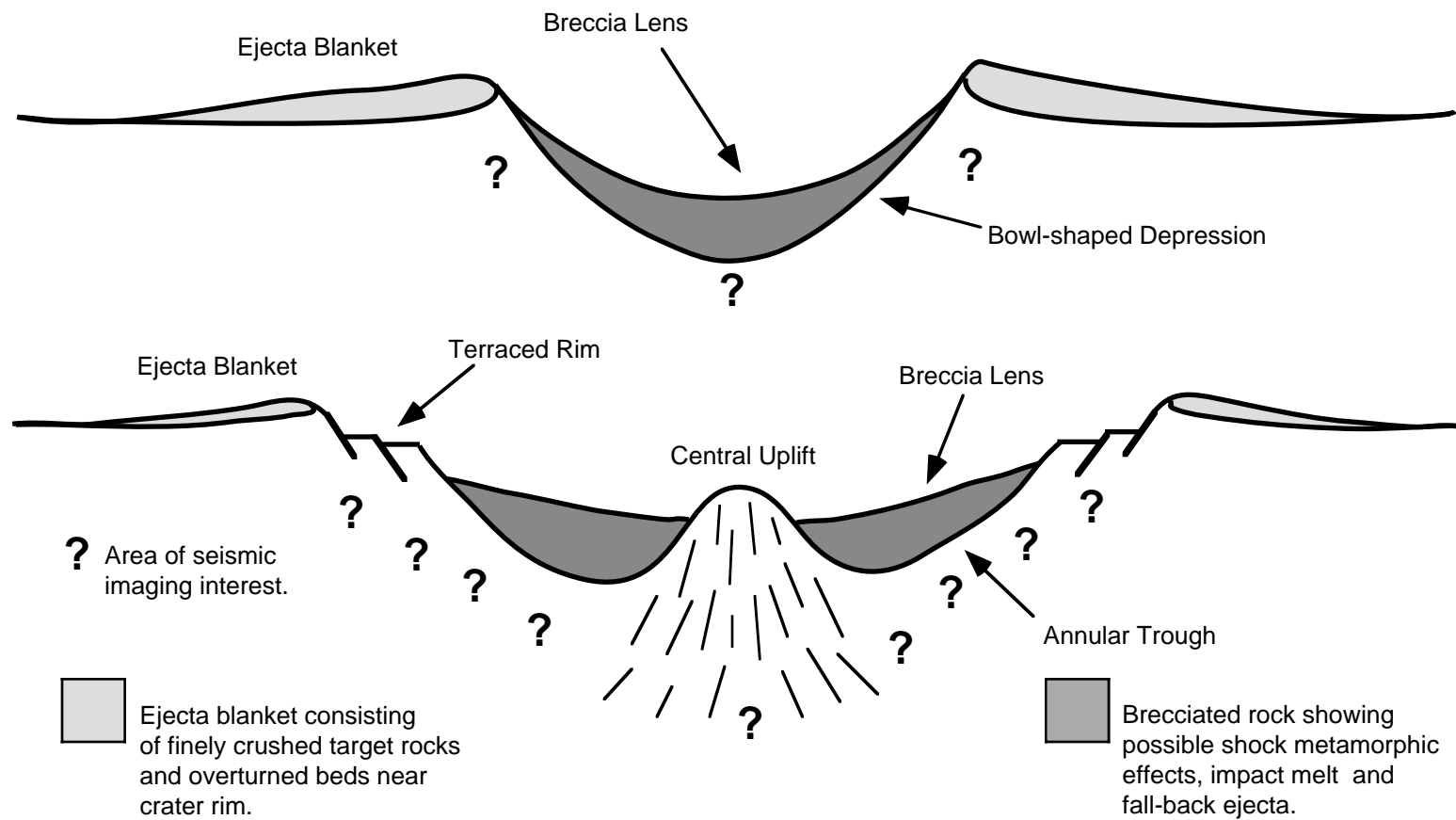


Fig. 1.6 Schematic diagrams of simple (top) and complex (bottom) crater morphologies.

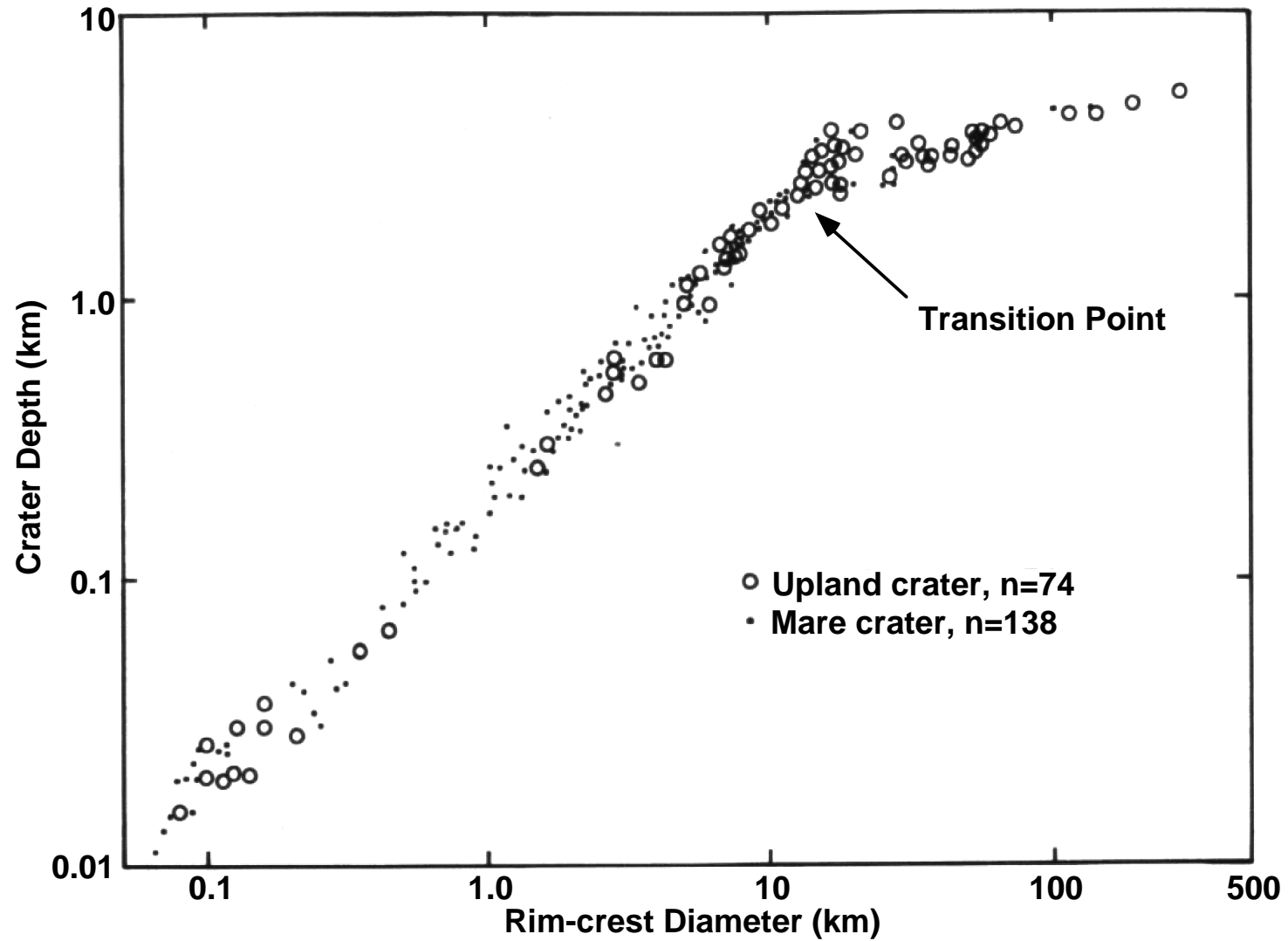


Fig. 1.7 Log-log plot of crater depth versus rim-crest diameter for lunar craters. A transition diameter of approximately 15 km is given by the inflection in the linear trend of the graph (from Melosh, 1989).

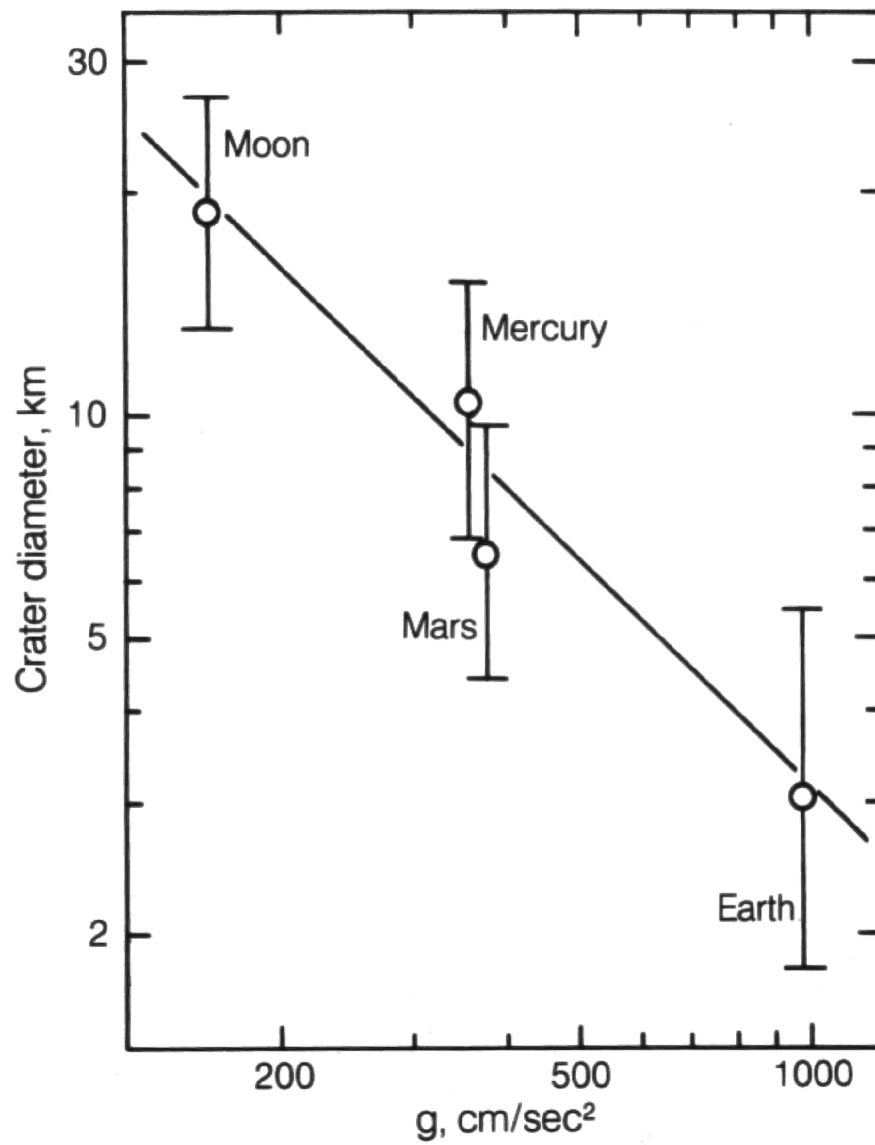


Fig. 1.8 Log-log plot of transition crater diameter versus gravitational acceleration for three of the terrestrial planets and the Moon. As the gravitational field increases, the transition diameter decreases, displaying an inverse relationship between the two variables (from Melosh, 1989).

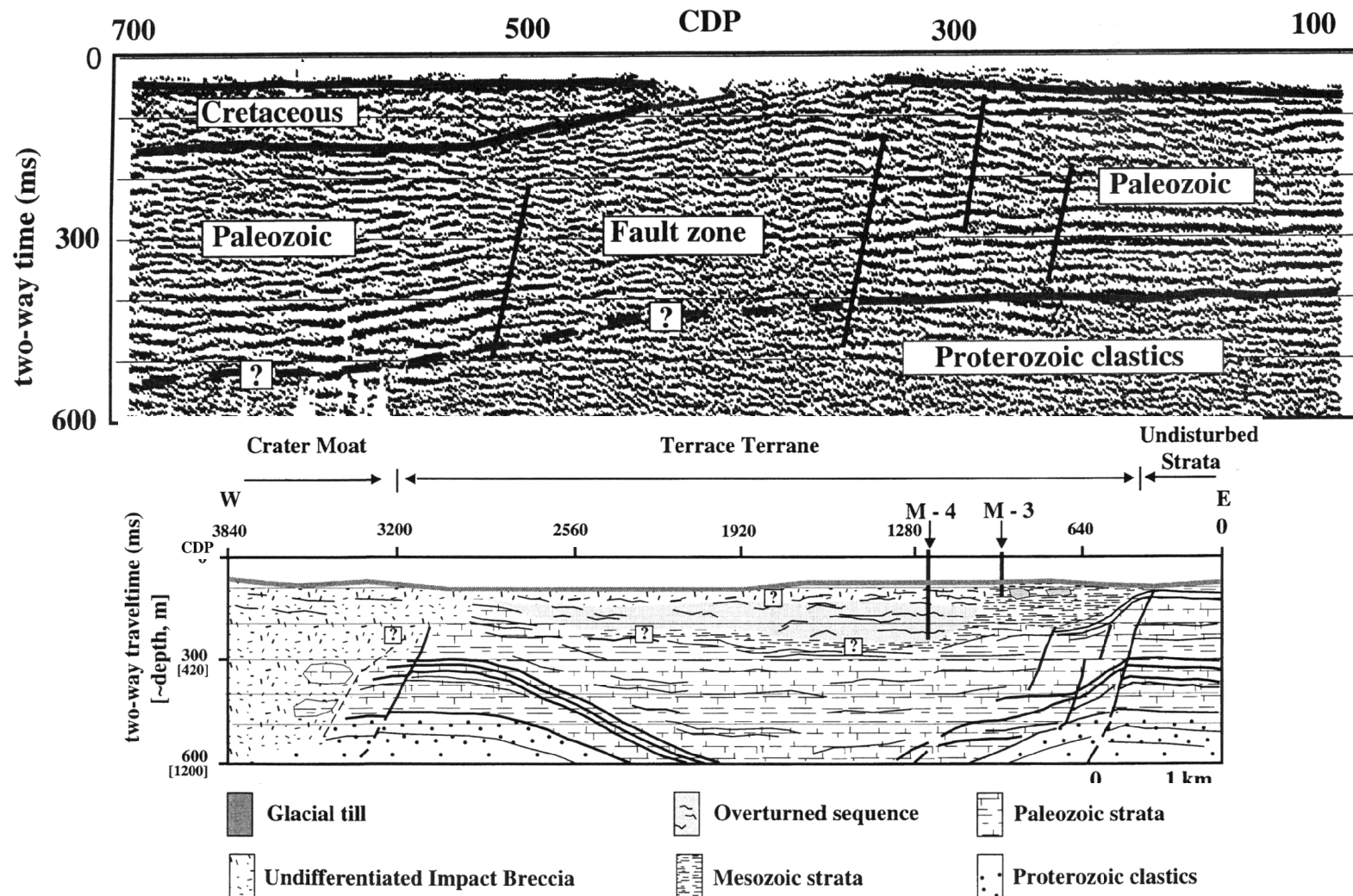


Fig. 1.9 The seismic data (top) and interpretation (bottom) over the eastern rim of the Manson impact structure in Iowa, U.S.A. Note that the seismic data extends only from CDPs 100 to 700 while the interpretation includes the full line (from Kieswetter et al., 1996).

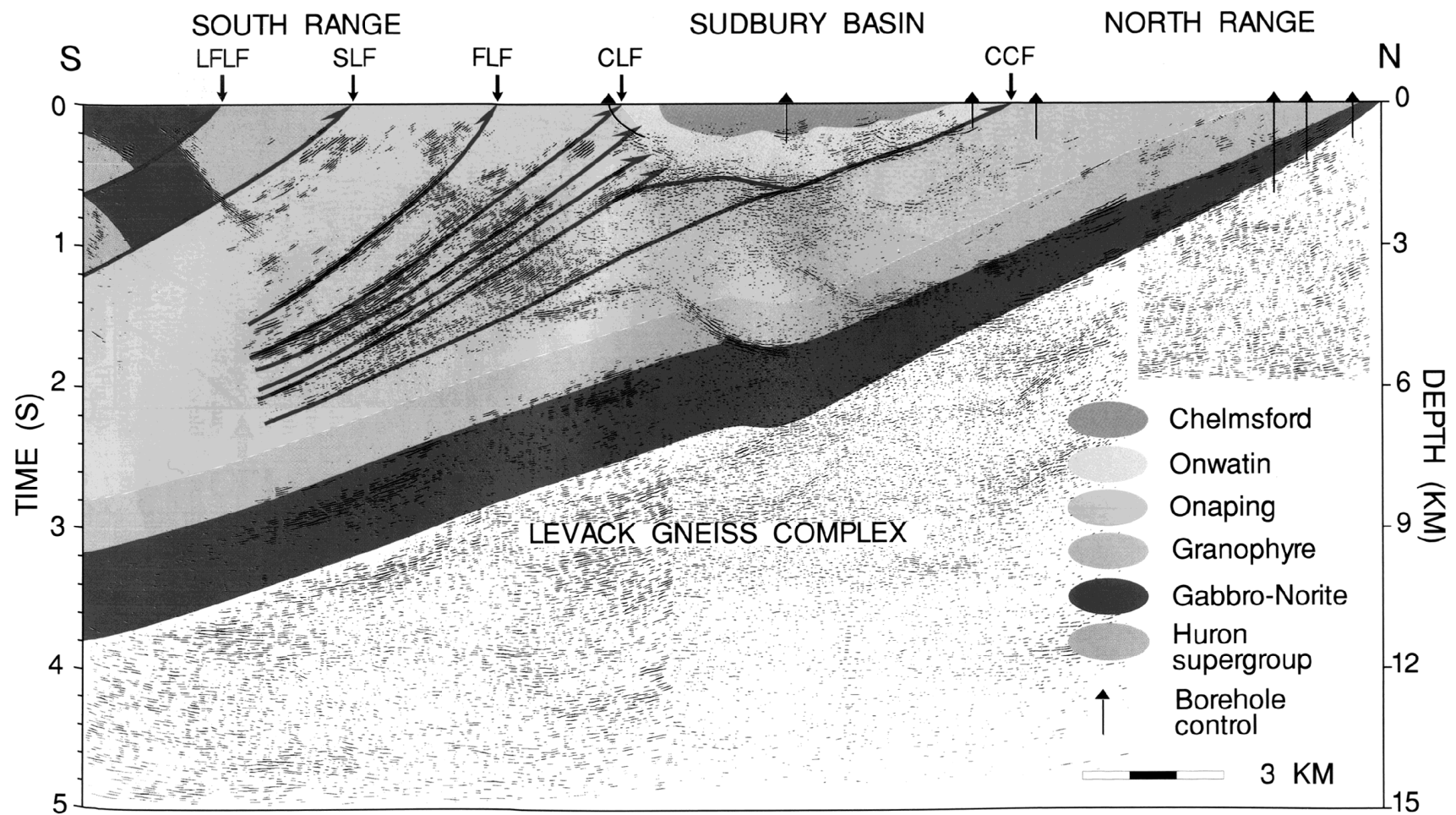


Fig. 1.10 The interpreted Lithoprobe seismic line over the Sudbury impact structure showing its relationship to geological formations and structures associated with the Penokean orogeny (from Wu et al., 1994).

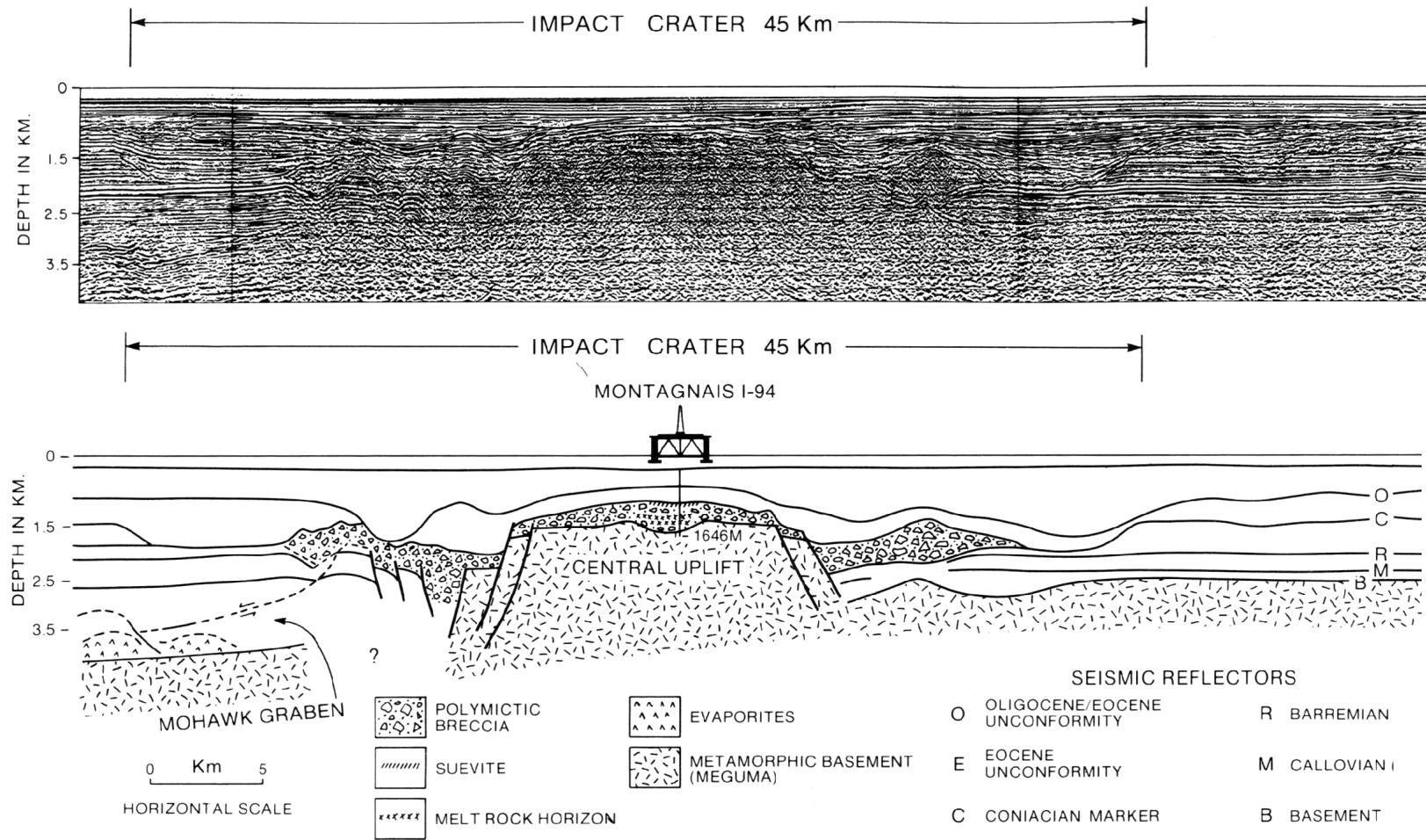


Fig. 1.11 The seismic data (top) and interpretation (bottom) from the Montagnais structure. It was the first submarine impact discovered (from Jansa et al., 1989).

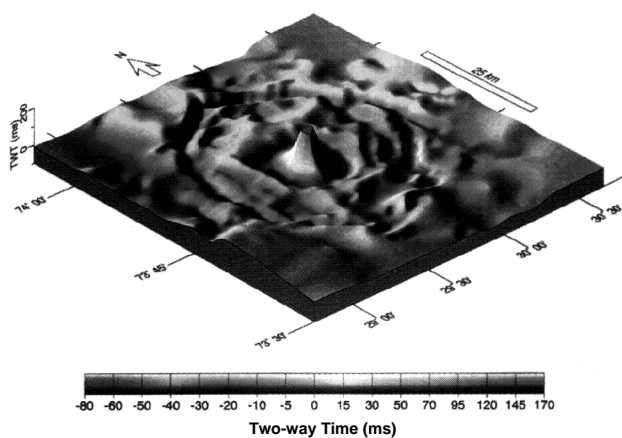
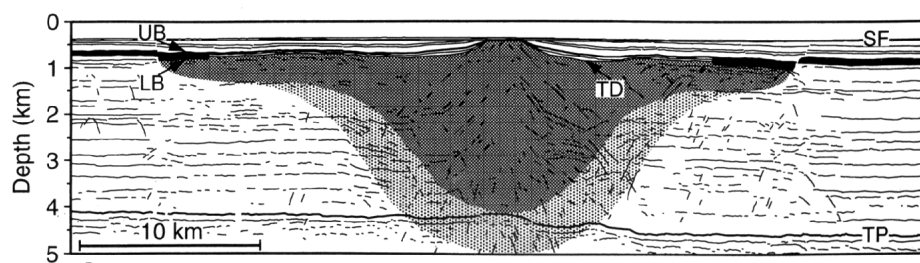


Fig. 1.12 The Mjølner impact crater interpreted from the seismic data (top) and on a time structure map (bottom) of the UB reflector (from Dypvik et al., 1996).

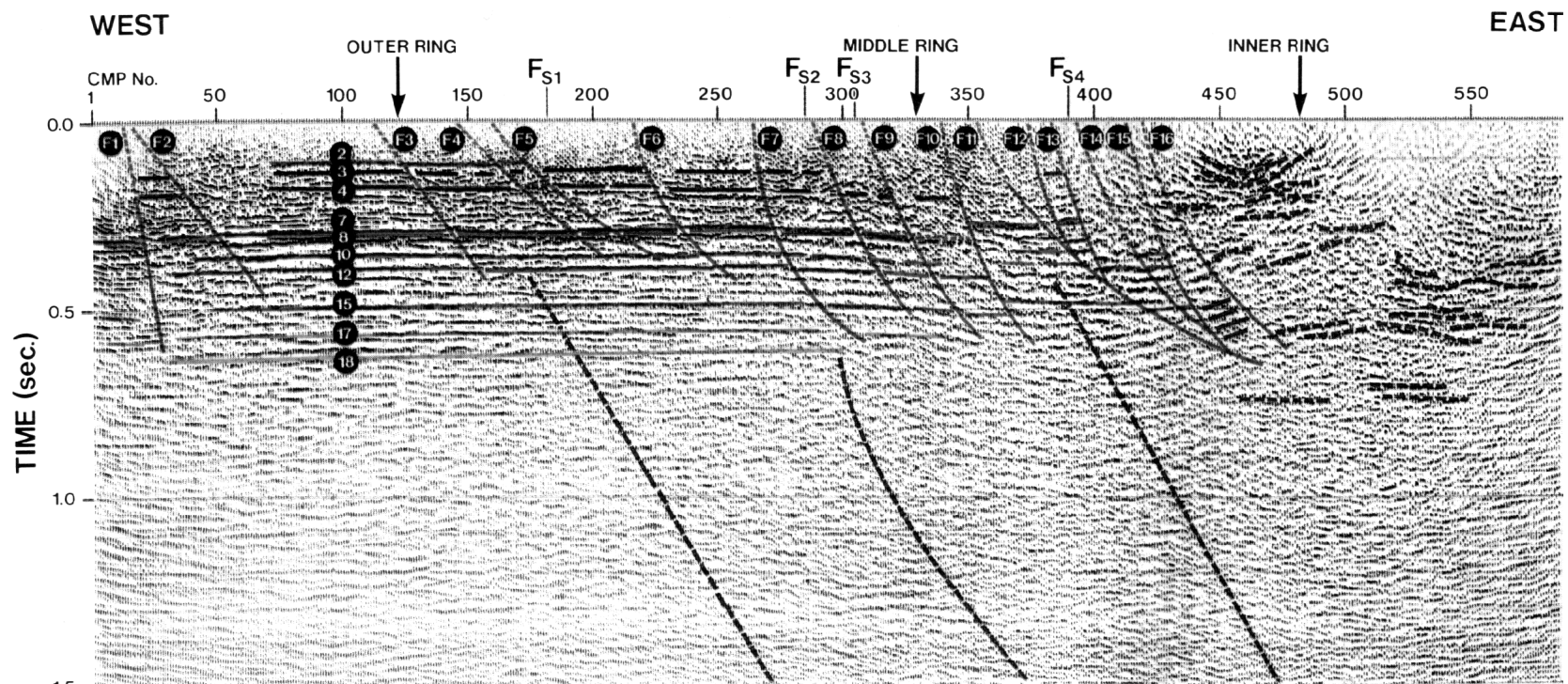


Fig. 1.13 The Haughton impact structure from the Canadian Arctic. The interpretation from the western portion of the structure shows numerous listric rim faults characteristic of complex impact craters (from Hajnal et al., 1988).

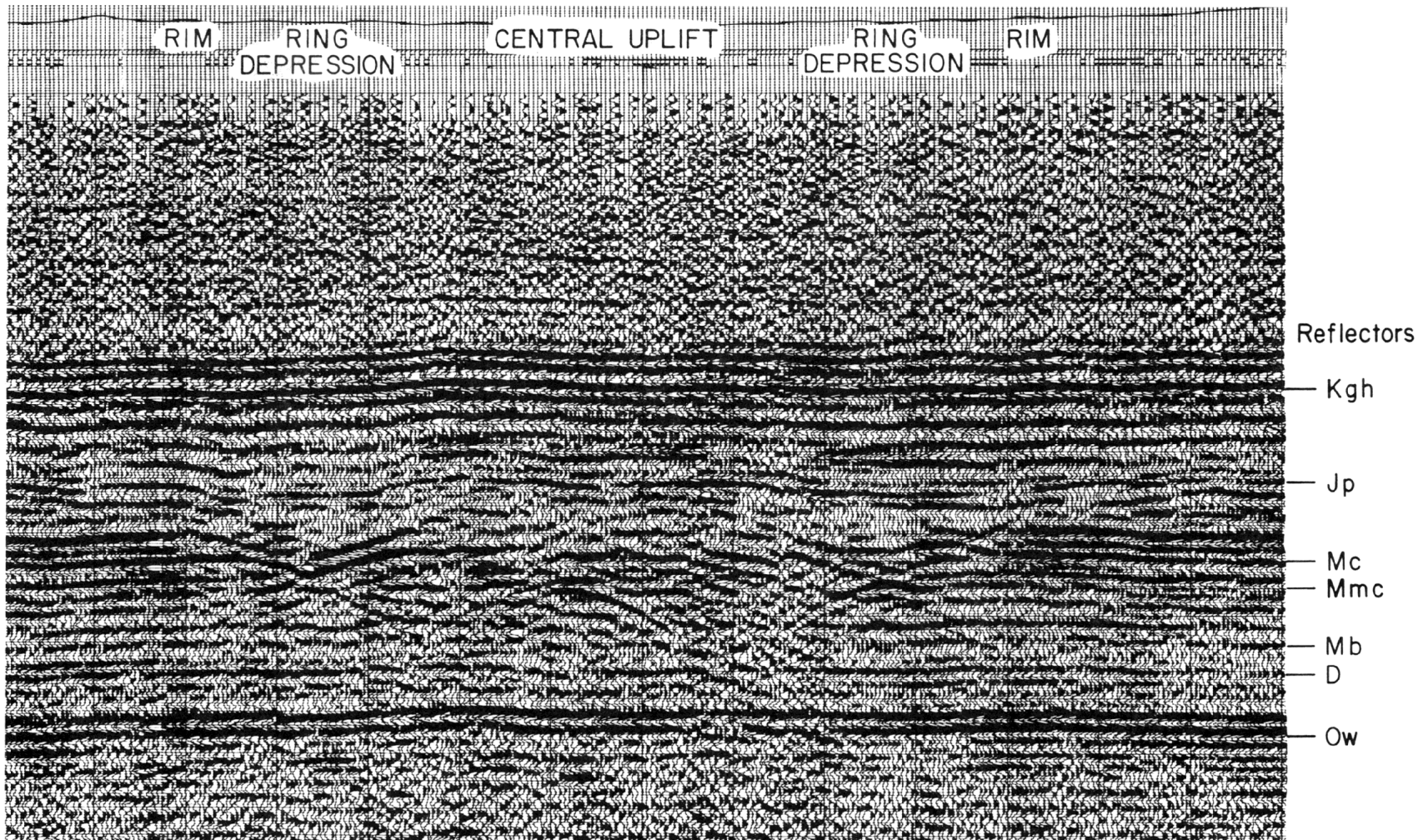


Fig. 1.14 A seismic structure stack over the 9 km wide Red Wing Creek impact structure. The morphology of the structure is apparent at the Jp reflector level (from Brenen et al., 1975).

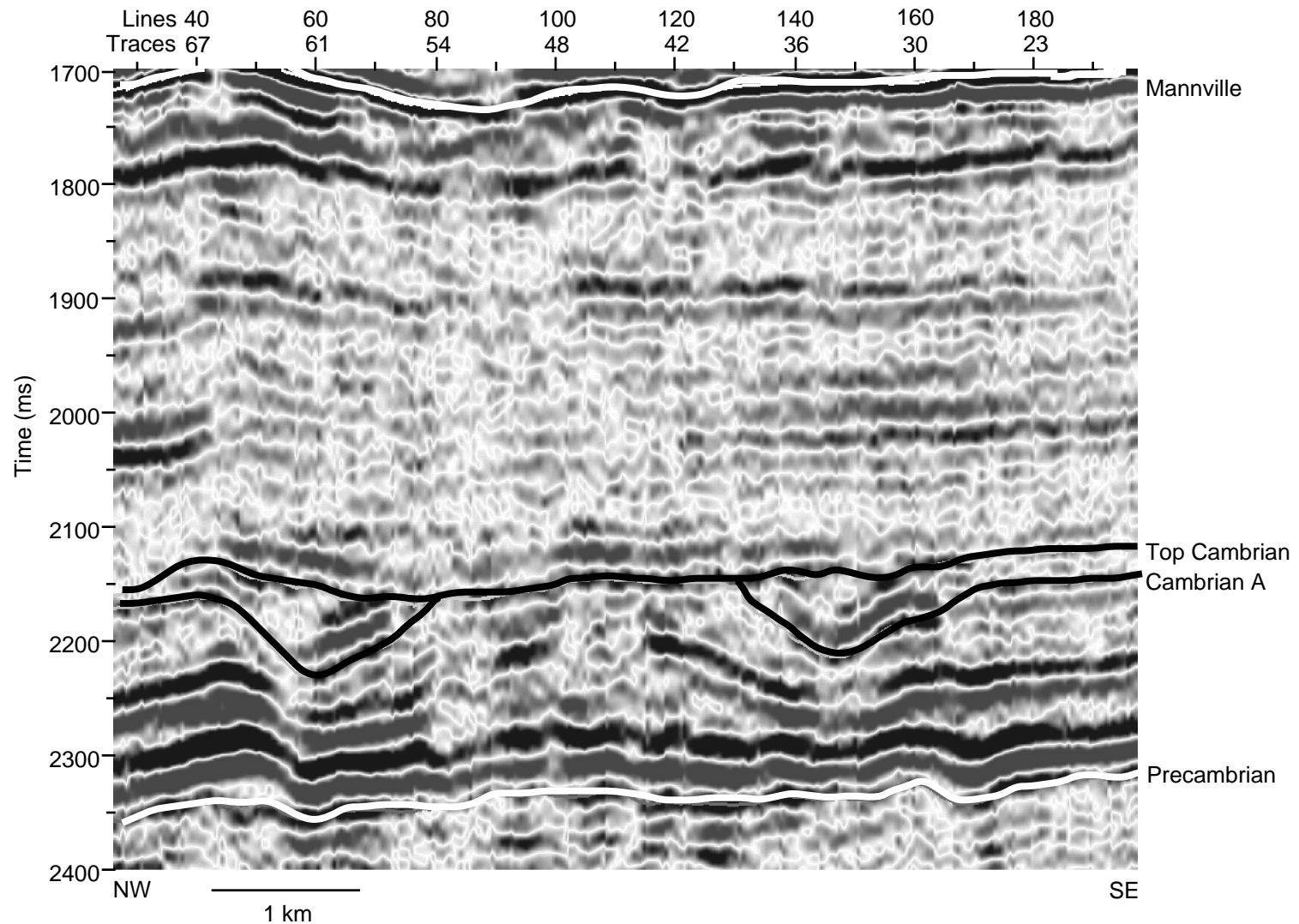


Fig. 1.15 A radial seismic section from the James River 3-D dataset. Note that the Top Cambrian reflector represents an erosional unconformity. The original diameter of the crater may have been 7 km (from Isaac and Stewart, 1993).

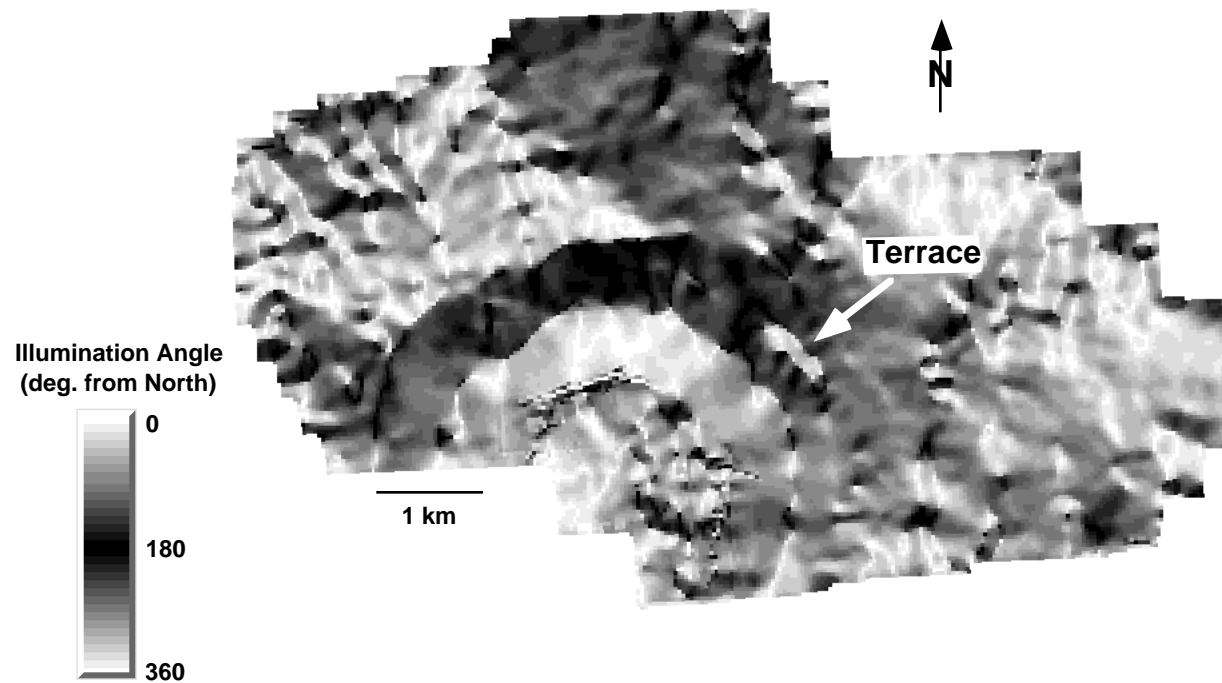


Fig. 1.16 The dip-azimuth map from the James River structure at the Cambrian A reflector. The large terraced blocks which make up the rim, can lead to structural traps (from Isaac and Stewart, 1993).

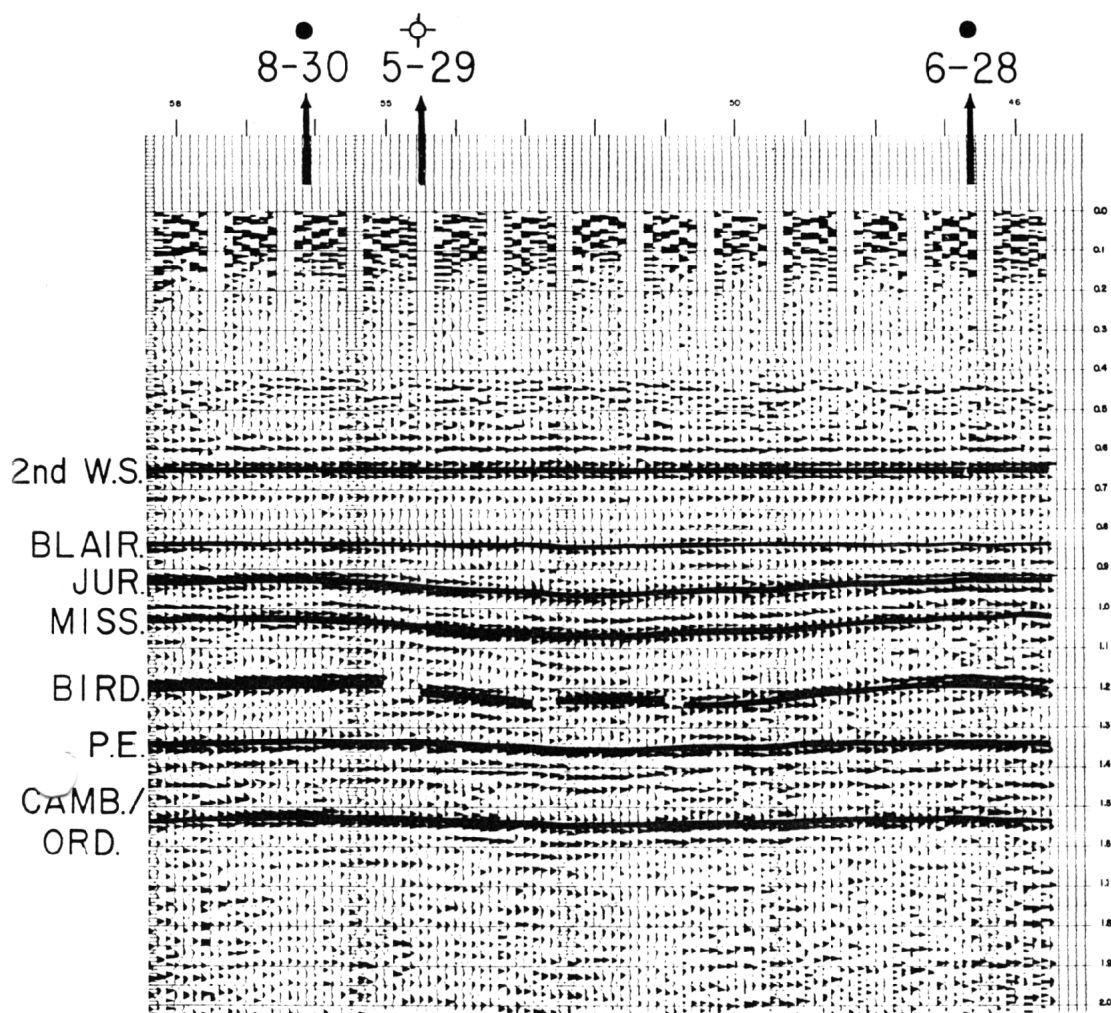


Fig. 1.17 Interpretation of the seismic data over the simple Viewfield structure in southeastern Saskatchewan. Within the structure, at the JUR reflector, the seismic data appears to show possible infill of the crater (from Sawatsky, 1972).

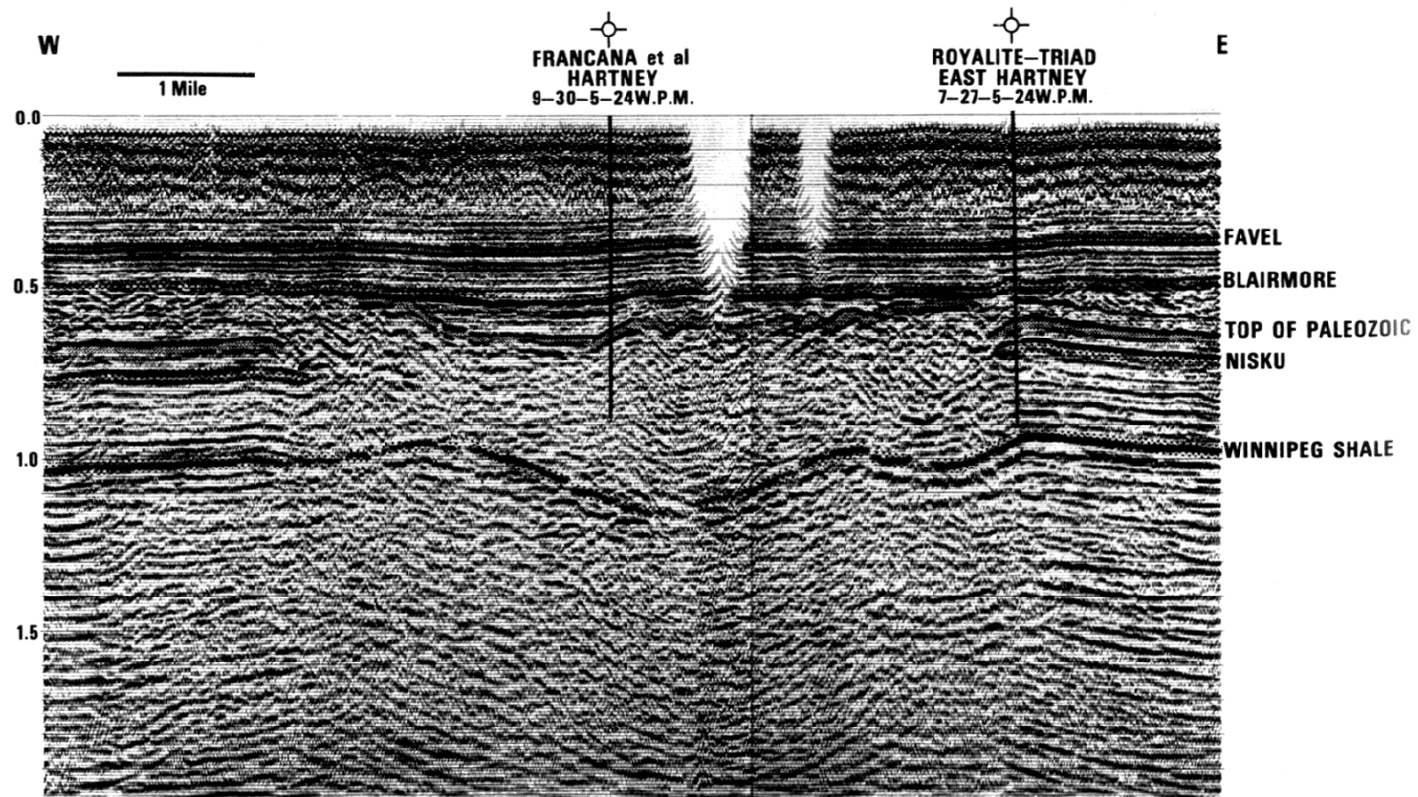


Fig. 1.18 A migrated seismic line over the Hartney structure. The apparent low in the center of the structure at the Winnipeg Shale is apparently due to a velocity anomaly above the central peak (from Anderson, 1980).

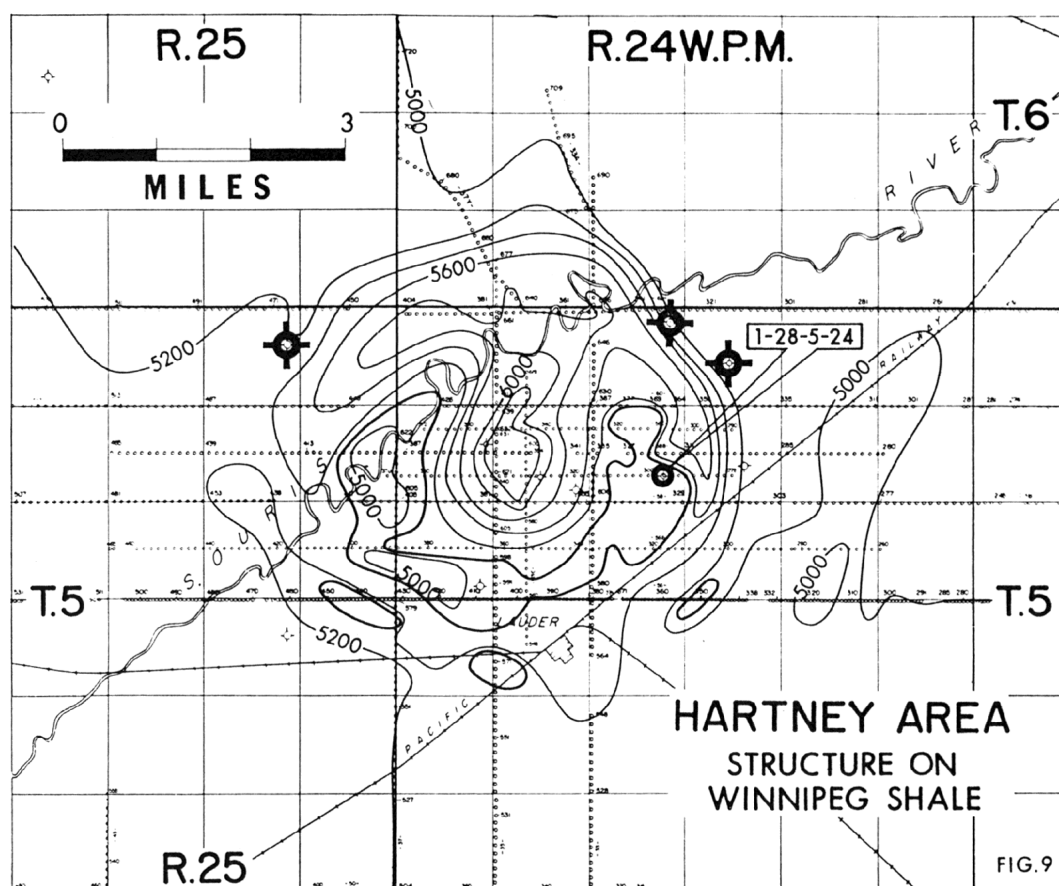


Fig. 1.19 The structure map of the Winnipeg Shale horizon after conversion of the seismic data to depth. The map shows a central peak within the structure after depth conversion. The contour interval is 100 feet (from Anderson, 1980).

CHAPTER 2 - SCALING RELATIONSHIPS AND RESERVOIR POTENTIAL

2.1 SCALING RELATIONSHIPS

Morphometry, the analysis of crater form based on laboratory experimentation, numerical modeling and actual impact structures, provides quantitative relationships between crater geometry and the nature of the impacting bolide (Grieve and Pilkington, 1996; Melosh, 1989). These relationships include estimates of the melt rock volume produced by high-velocity impact (Grieve and Cintala, 1992) as well as expressions for crater depth-to-diameter ratios. In the case of buried impact craters on Earth, which can only be examined remotely by geophysical means, these criteria are useful in examining the dimensions of the structure under investigation. Presumably, if the structural dimensions adhere to those which are predicted by scaling, then the structure itself is more likely to be an impact crater. On the other hand, if the structure does not exhibit dimensions which are predicted by scaling criteria then the impact hypothesis for its origin is less likely. This is a particularly useful exercise in the event that the structure has been imaged by seismic data which has the greatest potential to show the best structural detail.

It is my intention here to introduce and summarize scaling criteria in a manner such that they become useful when used in interpreting seismic data over structures suspected of having an impact origin. Thus I will focus on those scaling criteria relating to the size and shape of the crater and related phenomena. I've attempted to emphasize recent formulations of these criteria assuming that these are based on the latest available data, both experimental and observed without delving into theoretical implications. Note also that these

relationships are based on fresh, or reconstructed craters and therefore do not take erosion or other post-impact deformation into account.

2.1.1 Transient Crater Scaling

The transient crater is completely formed at the end of the excavation stage of crater development (see Chapter 1, section 1.2.2). As its name implies, it quickly changes in size and shape, largely under the influence of gravity, until it finds a more long-lived, relatively stable form - either the final simple morphology or the complex morphology (see Chapter 1, Figure 1.6). It has been postulated that the shape of the transient crater may be represented by a parabola of revolution such that:

$$z = 4 \frac{H_t}{D_t^2} r^2, \quad (2-1)$$

where z is the vertical distance from a point on the crater wall, to the crater floor, H_t is the depth of crater, D_t is the rim diameter and r is the distance from the center of the crater to the point at which z is measured (Melosh, 1989). Thus, $0 \leq z \leq H_t$ and $0 \leq r \leq D_t/2$ for any given transient crater (Figure 2.1). The volume of such a crater can then be calculated to be

$$V_t = \frac{\pi D_t^2 H_t}{8}, \quad (2-2)$$

where V_t is the transient crater volume, D_t is the transient crater rim diameter, and H_t is the transient crater depth. Melosh (1989) also suggests that the transient crater's rim height can be determined from

$$\delta = \frac{H_t}{40} \left(\frac{D_t}{r} \right)^3, \quad (2-3)$$

where δ is the rim height of the transient crater, H_t is the depth of the transient crater, D_t is the diameter of the transient crater and r is the rim radius from the vertical axis of symmetry (i.e., $r \geq D_t/2$). This equation is based on the equivalence of the rim's volume above the

pre-impact surface with the crater's volume beneath the pre-impact surface and thus does not allow for bulking and mixing of ejecta due to its own impact with surface material (Figure 2.1).

Work by Schmidt and Housen (1987) showed that the transient crater diameter is a function of the projectile characteristics. For saturated sand targets, they found empirically that

$$\pi_r = 0.8\pi_2^{-0.22}, \quad (2-4)$$

where $\pi_r \equiv r_{tc}(\rho_t/m)^{0.33}$ (where r_{tc} , ρ_t , and m are the radius of the crater, the density of the target and the mass of the projectile, respectively), a dimensionless ratio essentially equal to the ratio of transient crater radius to projectile radius (Melosh, 1989), and $\pi_2 \equiv 3.22gr_p/v_p^2$ (where g , r_p and v_p are the acceleration due to gravity, the radius of the projectile and the velocity of the projectile, respectively), a dimensionless ratio, sometimes referred to as the gravity-scaled size of the crater, which is approximately equal to the inverse of the Froude number ($F = v^2/2gr$), which itself relates inertial stresses to gravitational stresses (Melosh, 1989). All the above values are expressed in cgs units. π_r and π_2 are results of a form of dimensional analysis known as pi-group scaling. Note that the use of π here does not relate to the common use of π as the ratio between a circle's circumference and radius. The details of this scaling method are beyond the scope of this work and are formally treated in Schmidt and Housen (1987) and references therein. However, the essential idea is that the physically relevant variables are grouped into dimensionless parameters (the π -parameters such as π_r and π_2 mentioned above). The relationship between one π -parameter on another is tested experimentally holding all but the variable of interest constant. This in turn, results in relationships as expressed in Equation 2-4. As noted, the above result stems from the work by Schmidt and Housen (1987), who also tentatively suggest that Equation 2-4 is a best-estimate for impact into rock.

Taking the values for π_r and π_2 and substituting them into Equation 2-4, we get

$$r_{tc}(\rho_t/m)^{0.33} = 0.8(3.22gr_p/v_p^2)^{-0.22}$$

$$r_{tc} = 0.62(\rho_t/m)^{-0.33}(gr_p/v_p^2)^{-0.22}. \quad (2-5a)$$

Assuming the projectile can be estimated as a sphere with density, ρ_p , and mass, $m = 4/3\pi r_p^3 \rho_p$, and noting that $r_{tc} = 1/2 D_{tc}$ where D_{tc} is the transient crater diameter and $r_p = 1/2 D_p$, where D_p is the projectile diameter, then Equation 2-5a can be simplified to

$$D_{tc} = 1.16(\rho_p/\rho_{tr})^{0.33} D_p^{0.78} v_p^{0.44} g^{-0.22}, \quad (2-5b)$$

where D_{tc} is the diameter of the transient crater, ρ_p is the density of the projectile, ρ_{tr} is the density of the target rocks, D_p is the diameter of the projectile, v_p is the velocity of the projectile and g is the acceleration due to gravity, all in cgs units (Grieve and Cintala 1992). Grieve and Cintala (1992) use this formulation of Schmidt and Housen's (1987) result to calculate transient crater dimensions in their study of impact melt volumes with some success. In the sections to follow, relationships between transient crater dimensions and those for simple and complex craters are introduced. By using Equation 2-5b, it will be possible to relate final crater diameters to the size of the projectile that made them.

By conservation of volume, it has been estimated that for transient craters which undergo modification to the simple final morphology, depth-to-diameter ratios are about 1/3. A similar ratio is found for transient craters which evolve into the complex final form when the total depth of excavation is examined (Melosh, 1989). Thus,

$$\frac{H_t}{D_t} = \frac{1}{3}, \quad (2-6)$$

where H_t = the depth of the transient crater and D_t = diameter of the transient crater, regardless of final crater form. However, depth-to-diameter ratios for simple and complex craters, after modification of the transient crater, are quite different.

2.1.2 Simple Crater Scaling

Modification of small transient craters is dominated by simple gravity slumping of the transient crater's walls into the depression, forming a breccia lens. Study of these types of craters has resulted in a series of scaling criteria between various dimensions of the crater (Figure 2.2), some of which follow.

The velocity with which the slumping occurs can be approximated as a free-fall along a frictionless slope. Thus

$$v_s \approx (2gH_t)^{0.5}, \quad (2-7)$$

where v_s = velocity of the slide along the transient crater, g = acceleration due to gravity and H_t = depth of the transient crater in metres (Melosh, 1989). The result of the sliding is to widen the diameter of the final crater such that

$$D = 1.19D_t, \quad (2-8)$$

where D = the rim diameter of the simple crater and D_t = the transient crater diameter (Melosh, 1989). As the transient crater fills with the slumped material, the relative depth of the crater decreases as the diameter increases. This reduces the depth-to-diameter ratio such that

$$\frac{H}{D} = \frac{1}{5}, \quad (2-9)$$

where H = the depth of the crater and D = rim diameter (Melosh, 1989). The depth of the crater and the thickness of the breccia lens are approximately related by

$$H \approx 2H_b, \quad (2-10)$$

where H = the depth of the crater and H_b = thickness of the breccia lens as defined in Figure 2.2 (Melosh, 1989). This is perhaps overly simplified as Grieve and Pilkington (1996) found that

$$H_{gs} = 0.13D^{1.06} \quad (2-11)$$

and

$$H_{gs} + H_b = 0.28D^{1.02}, \quad (2-12)$$

where H_{gs} is the depth of the crater measured from the original ground surface (see Figure 2.2), H_b is thickness of the breccia lens and D is the rim diameter, all in kilometres. However, these equations are only based on seven good terrestrial examples and, in any case, approximate Equation 2-10. Slumping also incorporates part of the rim of the transient crater into the breccia lens. Pike (1977) found that the final rim height is related to the crater diameter for simple lunar craters such that

$$h_r = 0.036D^{1.014}, \quad (2-13)$$

where h_r is the height of the rim from the pre-impact surface and D is the rim diameter both in metres. This result is in remarkable agreement with the estimate of Equation 2-3.

2.1.3 Complex Crater Scaling

Larger transient craters undergo greater modification to form the complex morphology. Study of these types of craters has also attempted to relate the geometric dimensions of these craters into a series of scaling criteria.

Experimental and observational data obtained with regards to the maximum excavation within complex craters suggests that

$$D_t \approx 0.6D, \quad (2-14)$$

where D = rim diameter and D_t = transient crater diameter (Melosh, 1989). However, work by Croft (1985) showed that a power law relation seemed to fit the spectrum of

available data better. Using several transient crater reconstruction techniques, the diameter can be expressed as

$$D_t = D_{tr}^{0.15 \pm 0.04} D^{0.85 \pm 0.04}, \quad (2-15)$$

where D_t = diameter of the transient crater, D_{tr} = transition diameter for simple to complex craters and D = rim diameter, all in kilometres. This is an improvement over Equation 2-14 in that it attempts to incorporate differences in target rock type as reflected by the transition diameter variable.

Grieve and Pesonen (1992) evaluated five terrestrial structures and found that

$$H = 0.12D^{0.30}, \quad (2-16)$$

where H is the apparent crater depth, D is the rim diameter, in kilometres, for sedimentary target rocks and

$$H = 0.15D^{0.43}, \quad (2-17)$$

where H = apparent crater depth, D = rim diameter, in kilometres, for crystalline target rocks. However, being based on only a few examples, there is a great deal of uncertainty associated with these relationships. Nonetheless, they follow the same form as the relationship on the Moon which Pike (1977a) showed was of the form $H \propto D^{0.3}$. They also indicate that complex craters in sedimentary target rocks are shallower than those for in crystalline target rocks (Grieve and Pesonen, 1992).

Similarly, Grieve and Pilkington (1996) evaluated 24 complex craters and found that the structural uplift showed a power law relationship to rim diameter such that

$$SU = 0.086D^{1.03}, \quad (2-18)$$

where SU is the structural uplift, defined here to mean the vertical displacement of lowermost strata now exposed at surface, D is the rim diameter, all in kilometres. Thus complex craters should show structural uplifts, to a first approximation, of about 1/10 their

rim diameter. There is no indication whether or not there is a dependence on target rock type.

Almost before the transient crater has formed completely, structural uplift of its bottom begins, ultimately rising and then settling to form the central peak (Melosh, 1989; Grieve and Pesonen, 1992). The size of the central peak can be determined by

$$D_{cp} = (0.22 \pm 0.03)D, \quad (2-19)$$

where D_{cp} is the diameter of central peak and D is the rim diameter (Pike, 1985; Melosh, 1989) although there is a great deal of scatter in this relationship. This calculation also sets a basic lower bound on the size of the transient crater.

The above relationships form a framework with which buried structures, imaged only on seismic data, and suspected of an impact origin, can be studied. They are meant as an interpretive guide rather than a quick yes-or-no answer to the impact origin hypothesis. This process is attempted for the two case studies presented in Chapters 3 and 4.

2.2 RESERVOIR POTENTIAL

Before presenting the details of the above mentioned case studies, it seems prudent to demonstrate that meteorite impact structures have exploration potential in terms of hydrocarbon resources. Since impact craters apparently appear randomly over the Earth's surface, a fortuitous encounter during general exploration activity usually precedes any kind of detailed investigation. Since the impact event itself does not induce the formation of hydrocarbons (i.e., hydrocarbon accumulations are epigenetic deposits), the value of these structures becomes apparent only if they lie across hydrocarbon migration pathways or form basins in which post-impact sedimentation gives rise to hydrocarbon generation (e.g., the Ames structure). Thus, as is the case with all hydrocarbon exploration activity,

an understanding of the regional geological setting is important in establishing the likelihood of an impact crater having hydrocarbons trapped within it. As there are few examples of impact craters which are associated with hydrocarbons, this analysis is largely qualitative in terms of locating prospective parts of an impact crater. Because of the number of variables involved in determining whether or not a particular structure is prospective, and the uniqueness of each structure on a small scale, a strict exploration strategy of these features is likely impossible to implement except in the most general of terms. We can investigate this potential by first looking at current relationships between a few of these structures and the associated hydrocarbon exploration or exploitation activity. Table 2-1 describes nine structures and their associated hydrocarbon accumulations as well as the basic structural facies in which the discoveries were made.

As mentioned in Chapter 1, the Ames structure, one of the most prolific hydrocarbon producers, is a case in which the structure provided both the isolated basin in which source rock formed, as well as the structural trapping mechanisms for hydrocarbon accumulations. Total reserves at Ames are estimated at 50 million barrels of oil and some 60 billion cubic feet of gas (Isaac and Stewart, 1993; Grieve and Masaitis, 1994; Kuykendall and Johnson, 1995). While the first discovery came from karsted rim dolomites, the largest deposits are found in the granite-dolomite breccia of the central uplift and brecciated granite in the floor of the crater, the transient crater having excavated to basement. Over 100 wells have been drilled on the structure of which 52 produce oil and 1 produces gas. The original discovery well rated at 3440 MCF of gas and 300 bbl of oil per day. However, the Gregory 1-20 well, drilled on the flank of the central uplift, is the most productive oil well with 80 m of granite-dolomite pay, a drill stem test of 1300 barrels of oil per day and a primary recovery of more than 10 million barrels.

Structure	Diameter and Morphology	Age	Hydrocarbon Accumulation	Structural Association
Ames, Ok	14 km - C	450 Ma	<ul style="list-style-type: none"> • 50 MMbbl oil • 20-60 BCFG • source rock controlled by structure 	<ul style="list-style-type: none"> • karsted rim dolomites • brecciated granite-dolomites of the central uplift and crater floor
Red Wing Creek, N.D.	9 km - C	200 Ma	<ul style="list-style-type: none"> • 40-70 MMbbl oil recoverable • 100 BCFG recoverable • 12.7 MMbbl oil and 16.2 BCFG total production • provided trap to migrating hydrocarbons 	<ul style="list-style-type: none"> • faulted Mississippian reservoir in central uplift
Avak, Al	12 km - C	3-100 Ma	<ul style="list-style-type: none"> • 37 BCFG reserves • provided trap to migrating hydrocarbons 	<ul style="list-style-type: none"> • listric rim faults which form structural traps in competent blocks
Marquez, Tx	22 km - C	58 Ma	<ul style="list-style-type: none"> • some gas production 	?
Newporte, N.D.	3.2 - S	500 Ma	<ul style="list-style-type: none"> • oil shows in Cambrian-Ordovician sands 	<ul style="list-style-type: none"> • highly fractured basement
Calvin, Mi.	6.2 km - C	Late Ordovician	<ul style="list-style-type: none"> • 600 MMbbl oil reserves • 500,000 bbl oil since 1978 	?
Steen, AB	22 km - C	95 Ma	<ul style="list-style-type: none"> • 600 bbl per day 	<ul style="list-style-type: none"> • rim complex
Viewfield, SK	2.4 km - S	Triassic-Jurassic	<ul style="list-style-type: none"> • 400 bbl per day • 20 MMbbl recoverable oil • formed trap to migrating hydrocarbons 	<ul style="list-style-type: none"> • Mississippian carbonate breccia • Mississippian in the rim
Tookoonooka, Australia	55 km - C	?	<ul style="list-style-type: none"> • forms shadow zone to migrating hydrocarbons from Eromanga Basin 	<ul style="list-style-type: none"> • potential for rim traps

Table 2.1 Structures associated with hydrocarbon accumulation. Simple and complex crater morphology is denoted by an “S” and “C” respectively. (Sources: Isaac and Stewart, 1993; Grieve and Masaitis, 1994; Hodge, 1994; Buthman, 1995; Milstein, 1995).

The 9 km wide, 200 Ma old Red Wing Creek structure in North Dakota is another complex crater in which production is primarily from brecciated Mississippian rocks in the central uplift. The petroleum source rocks in this case are not local to the structure. There is nearly 500 m of net pay from Mississippian strata which have been repeated by thrusting in the central uplift region. Higher porosity and permeability values are a result of impact induced fracturing and brecciation resulting in flow rates of 1000 barrels per day for a single well (Pickard, 1994). Cumulative production is more than 12.7 million barrels of oil

and 16.2 billion cubic feet of gas while recoverable reserves are estimated at 70 million barrels of oil and 100 billion cubic feet of gas (Grieve and Masaitis, 1994; Pickard, 1994).

The Avak structure, located on the north coast of Alaska, shows three associated gas fields (Figure 2.2). These fields are primarily contained between the outer rim structure and the inner trough of the crater. In this particular case, it is believed that the structure may have disrupted already existing gas accumulations within the Barrow High, a west-east trending anticline (Kirschner et al., 1992). Whether or not the current accumulations are less than those which were already in place prior to the impact is unknown, nonetheless, the reservoirs are now structurally controlled by the shallower, listric, normal faults along the rim which juxtapose Jurassic reservoir rock against a Cretaceous seal updip. Currently the South and East Barrow fields are in production with estimated reserves of some 37 BCF of gas (Grieve and Masaitis, 1994).

Figure 2.3 shows a recent well map over the Steen River structure in northern Alberta. Currently an active area of exploration, the terraced rim and central uplift of the structure have been the major targets. Drilling has been more successful on the rim of the structure with four oil wells producing over 600 bbl per day (Isaac and Stewart, 1993) from the Keg River and Muskeg formations of the Lower Devonian. The land position also gives clues to the strategy for exploration of the structure as land currently held by exploration companies and land currently for sale is shown in grey, and covers most of the rim and central uplift of the structure. Similarly, Figures 2.4 and 2.5 show current well maps over the Eagle Butte structure, in southern Alberta, and the Viewfield structure, in southeastern Saskatchewan, respectively. Drilling over the Eagle Butte structure is largely confined to the flanks of the central uplift and the 18 km diameter rim (particularly the southeastern edge), where some gas accumulations are apparent. The structure itself disrupts most of

the 1200 m thick clastic part of the section as well as the carbonates of the Mississippian making it a likely exploration target (Lawton et al., 1993). Current accumulations are from the Cretaceous Second White Speckled Shale and Bow Island formations. The Viewfield structure (Figure 2.5) at only 2.4 km in diameter is thought to be a simple impact crater. The structure is Triassic to Jurassic in age but disrupts prospective Mississippian carbonates (see Figure 1.17). The infill of the structure effectively forms a stratigraphic seal against which oil has migrated and been trapped within the Mississippian. No hydrocarbons have been discovered within the center of the structure. Current reserves are estimated at 20 MMbbl of oil (Isaac and Stewart, 1993).

These examples provide a general frame work from which exploration may be more effective. Impact craters have the potential to be associated with hydrocarbons only when they lie in the path of migrating hydrocarbons. In particular, their geometric relationship with regional dip will indicate how migrating hydrocarbons will encounter the structure and their morphology will determine the type of trapping mechanism. In settings where the impact structure crosscuts the regional strata in such a fashion that the crater lies parallel to the regional geology, migrating hydrocarbons will encounter the structure laterally, and will likely be trapped along the listric rim faults of the structure. For complex craters, this scenario usually results in the central uplift being somewhat isolated from the regional setting by the trough and the rim faults. The rim faults can effectively prevent fluids from migrating to the interior of the structure. However, in the event that the impact occurs in dipping strata, the migrating fluids may reach the central peak directly from beneath the structure. In this case, faulting is usually directed up towards the uplift allowing for migration into the center of the structure. Similarly for simple craters, a normal setting with respect to regional geology will likely result in trapping along the rim of the structure, provided it is infilled with relatively less permeable material. There is no direct evidence

whether the breccia lens might be suitable as a reservoir. It likely has enhanced porosity and permeability and may become prospective if a suitably impermeable cap rock is present. The exception to these generalizations occurs in the case where the source rock is internal to the structure, as in the Ames crater. In this case, both the rim and the central uplift are within range for migrating fluids, depending on the infill geology of the structure and regional influences are less important.

Impact structures may be indirectly involved in the trapping of hydrocarbons by controlling the formation of subsequent structures shallower in the stratigraphic section. The impact site may experience long-lived hydrothermal activity enhanced by the high temperature and fracturing imparted to the target rocks during the impact. Such an environment may be conducive to hydrothermal alteration of rocks or dissolution. The fractures associated with the structure may provide conduits for dissolving brines long after the impact has been buried at depth.

2.3 CONCLUSIONS

The scaling criteria introduced in Section 2.1 are meant to provide a framework in which to help interpret suspected meteorite impact craters which are imaged on seismic data. Rather than a definitive answer to the impact origin hypothesis for a structure, the equations represent a means of testing the hypothesis either to help lend credence to it or to help dismiss it from possibility. Such analysis is limited by the quality of the seismic image, as well as the inherent assumptions behind the scaling criteria used. This analysis is attempted for the two case studies in Chapters 3 and 4.

The concepts introduced in Section 2.2 oversimplifies the situation of exploring for hydrocarbons in and around meteorite impact craters. Each structure will probably have its

own particular set of unique reservoir properties depending on size of the crater, regional geological setting, post-impact infill, depth of burial, level of erosion, the hydrogeological regime within and surrounding the crater, and post-impact deformation. Nonetheless, current exploration activity around these structures suggests that the rim is likely to hold promise for structural trapping of hydrocarbons, regardless of crater morphology. The central portion of the crater is generally more isolated from the regional geological setting but may become prospective in the event the impact occurs in dipping strata. In the case of complex craters, the flanks of the central uplift are more prospective as they often demonstrate repeated stratigraphy due to thrusting of rock units during the modification stage of crater formation. In some instances, when the hydrocarbon source rock resides internally to the structure itself, accumulations can occur in both the rim and central uplift of the structure. In the case of simple craters in dipping strata, the breccia lens may become prospective if a suitably impermeable infill is present, however, as simple craters are, by definition, smaller than complex craters, they are more likely to be removed by erosion, thus making them poorly represented in the total crater population.

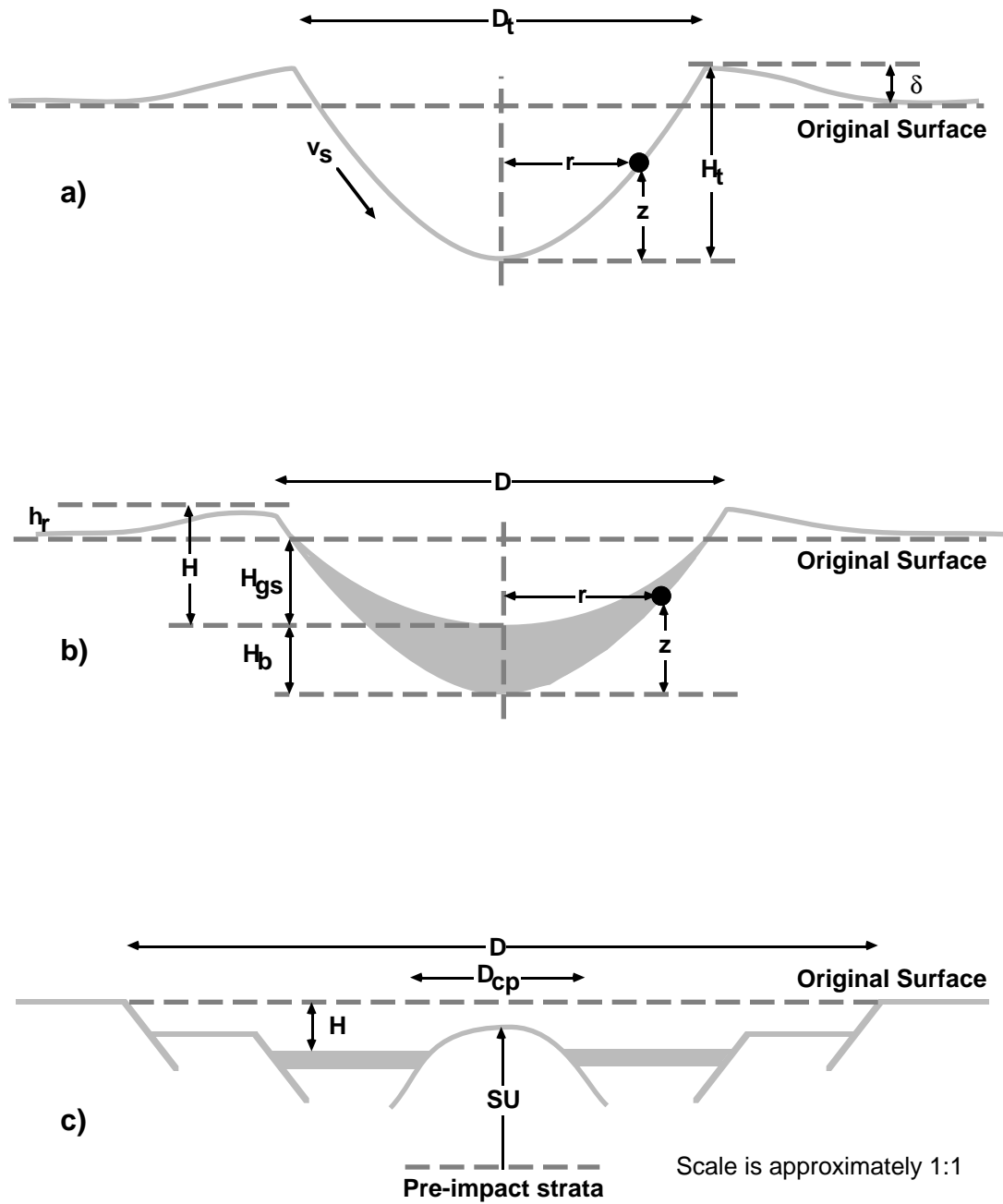


Fig. 2.1 Schematic diagram of a) the transient crater, b) a simple crater and c) a complex crater with the dimensions used in scaling criteria annotated.

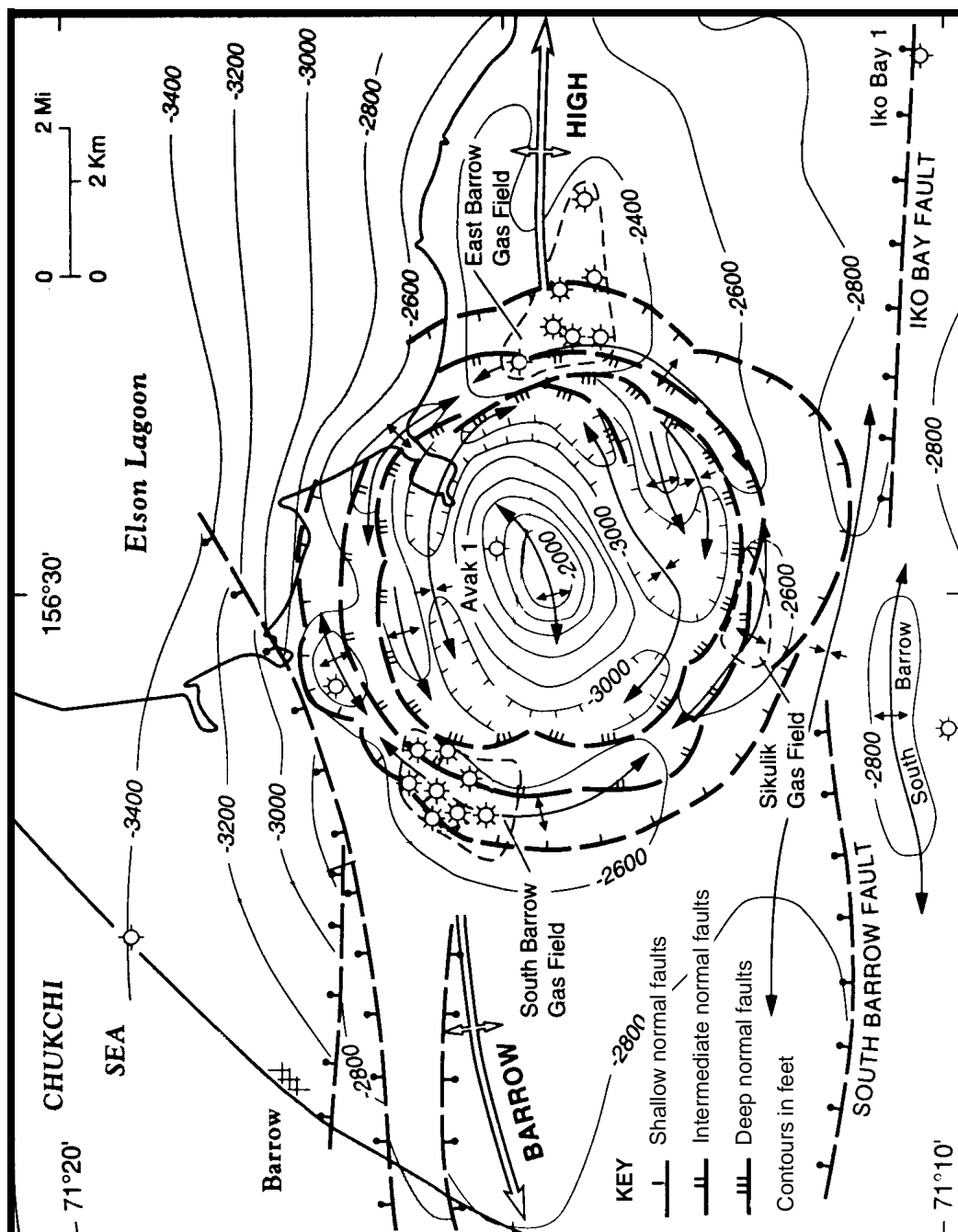


Fig. 2.2 Structure map over the Avak crater showing the three associated gas fields located between the shallowest rim faults and those at intermediate depth (from Kirschner et al., 1992).

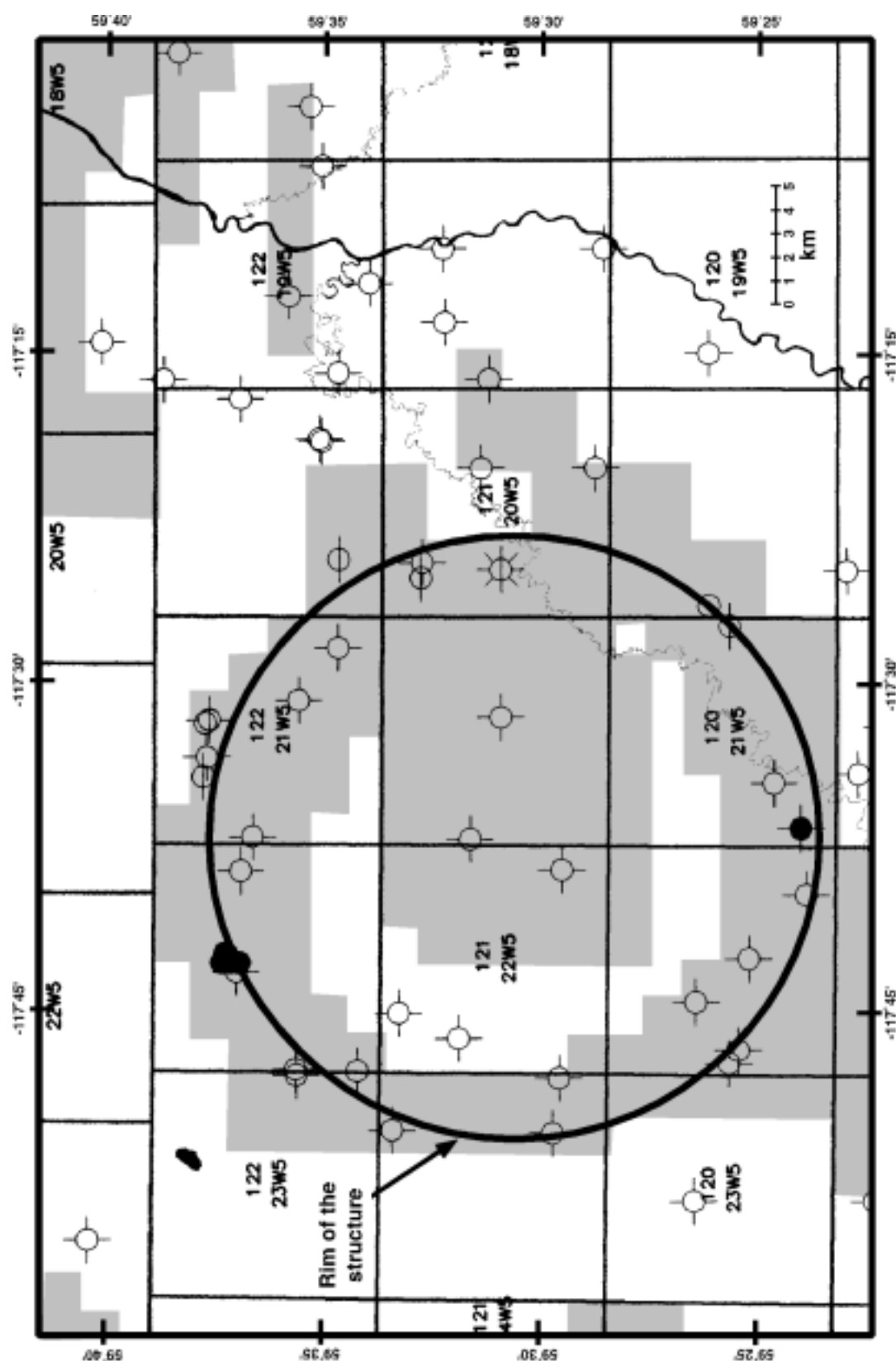


Fig. 2.3 Well map over the Steen River structure. Exploration has so far been limited to the rim of the structure with some wells also drilled on the central uplift. The shaded area represents land currently held or for sale.

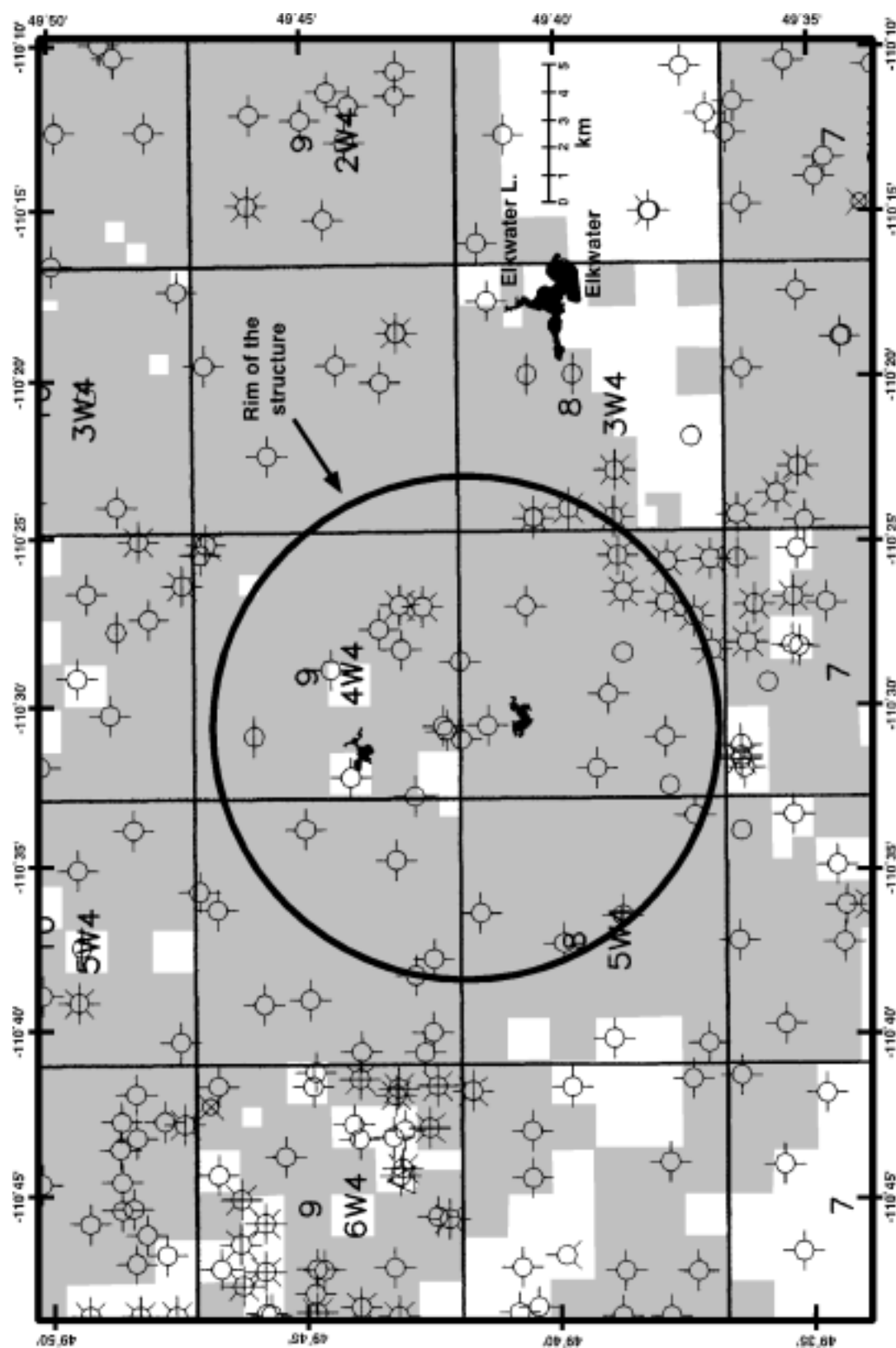


Fig. 2.4 Well map over the Eagle Butte structure. Drilling on the structure was primarily related to the rim of the structure and the flanks of the central uplift.

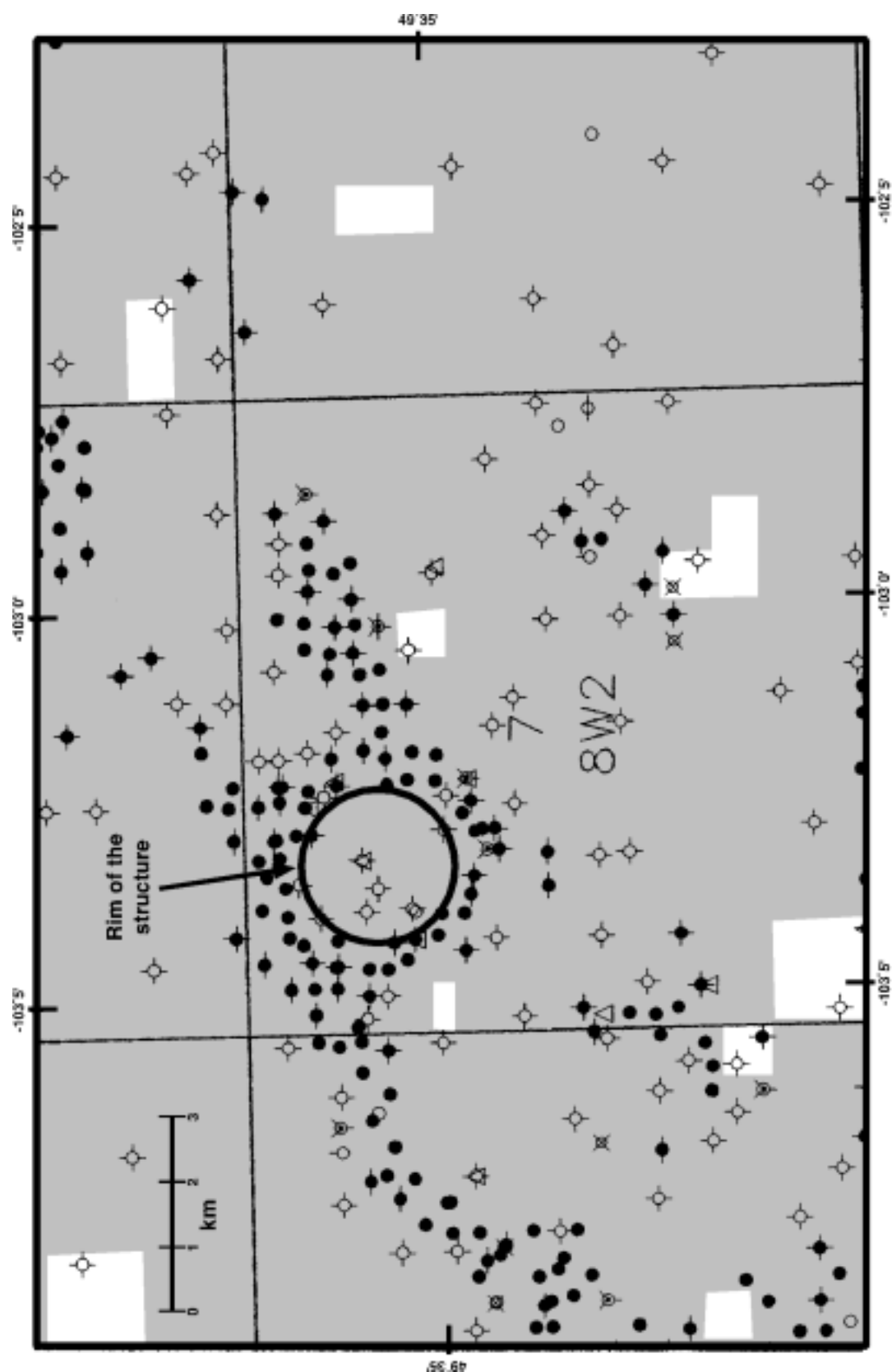


Fig. 2.5 Well map over the Viewfield structure. The rim of the structure at the Mississippian level and the impermeable infill of the structure has allowed for trapping of hydrocarbons along the structure's periphery.

CHAPTER 3 - THE WHITE VALLEY STRUCTURE

3.1 GEOLOGICAL SETTING

3.1.1 Regional Geology

The White Valley structure, also known as the Maple Creek structure, is located in the Cypress Hills area of southwestern Saskatchewan ($49^{\circ}48'00''\text{N}$, $109^{\circ}06'30''\text{W}$). The structure lies within a valley on the north side of the Cypress Hills which rise about 1200m above the regional plains and surround the structure to the west, east, and south (Furnival, 1946, Gent et al., 1992). The generalized stratigraphic chart of this region is shown in Figure 3.1. Initial geological mapping in this area showed that the regional stratigraphy of the Cypress Hills consisted mostly of gently southeast dipping strata composed of Tertiary and Upper Cretaceous sediments from the uppermost Cypress Hills formation to the Bearpaw formation. The plains north of the Cypress Hills are covered by glacial drift of varying thickness which is underlain by the Bearpaw Formation (Furnival, 1946, Gent et al., 1992). However, near the White Valley structure Furnival (1946) described these near-surface strata as having high dip angles, slickensides, and complex folds that indicated much more intense deformation than is typical of the area. Furnival (1946a) also concluded that the strikes and dips indicated that the structure was much more irregular than other structures in the area and that the available outcrops were insufficient to permit any definite conclusions regarding the character or origin of the deformation. Well-preserved repeated sections of the Eastend and Bearpaw formations about 1 km west of the test-holes, are tilted toward the structure and become younger to the east (Gent et al., 1992).

Field work conducted by Dr. Art Sweet of the Geological Survey of Canada uncovered evidence for deformation in the Ravenscrag Formation within a fresh road cut near the rim of the structure (Sweet, pers. comm., 1997). Shallower formations are largely unconsolidated gravels and no structure within these could be seen (Sweet, pers. comm., 1997). This suggests the structure formed after early Ravenscrag time (< 60 Ma ago). It should be noted, however, that such shallow deformation has been observed elsewhere in the Cypress Hills and has been attributed to the thrusting action of ice during the Pleistocene (Christiansen and Whitaker, 1976; Sweet, pers. comm., 1997). The amount of erosion is unknown so it is possible that the structure occurred at a paleo-surface higher in elevation, resulting in an even younger age for the structure. Aerial photography of the area shows an arcuate ridge which projects to a circle approximately 7.5 km in diameter closely matching the projected diameter of the structure from seismic data (Section 3.2.3) and also suggests that the structure is quite recently formed (Figure 3.2).

3.1.2 Geological Well Control

Geological well control comes primarily from the 07-07-010-23W3 well, drilled near the center of the structure, and two shallow test wells (01-07-010-23W3 and 16-06-010-23W3) also drilled near the apparent center of the structure. Disruption of the stratigraphic column occurs to a depth of about 1300 m as indicated from drilling. The oldest strata involved appear to be Mississippian in age. The target of the 07-07-010-23W3 well, drilled near the center of the structure, was the oil-bearing carbonate Birdbear Formation of the Late Devonian. It was dry and abandoned, but indicated that the Mississippian and Birdbear formations occurred at regional depths. Structures found in core samples from the two shallow test-holes include boudinage-like and ball structures along surfaces, as well as intense brecciation, microfaults and slickensides giving evidence for shearing and plastic deformation (Gent et al., 1992). Gent et al. (1992) also noted that the Bearpaw

Formation is entirely absent from 16-06 with older sediments from the Belly River and Lea Park formations in its position.

3.2 GEOPHYSICAL CHARACTERISTICS

The structure was discovered during hydrocarbon exploration in the area and is evident on four 2-D seismic lines, a base map of which is shown in Figure 3.3. Lines WV-017 and WV-021 best demonstrate the overall morphology of the structure as they pass close to its center. WV-011 and WV-016, being non-radial to the feature show the complexity of the rim and the likely problem of out-of-plane effects. Tables 3.1 and 3.2 briefly summarize the acquisition and processing of the data to final migrated stack. A gravity profile, acquired by Saskatchewan Energy and Mines and the University of Saskatchewan, trends N-S over the center of the structure along seismic line WV-017 (Gent et al., 1992) and is discussed in Section 3.2.3.3.

In addition to the seismic and gravity data, data from three wells in the area were used to aid in correlation of horizons to reflectors and to identify evidence for structural deformation via differences in well log signature. These included 07-07-010-23W3 which was drilled near the structure's core, and 01-04-010-22W3 and 04-01-011-24W3 which

ACQUISITION PARAMETERS	
Source	<ul style="list-style-type: none"> • Vibroseis: 4 vibrs over 50 m • Frequency: 8 sweeps, 10-90 Hz • Interval: 125 m
Receiver	<ul style="list-style-type: none"> • Interval: 25 m • Geometry: 9 inline per group
Shot-Receiver Geometry	<ul style="list-style-type: none"> • 2D split spread • offset range of 100 m to 1575 m • 3 W-E lines, 1 N-S line
Sample Rate	<ul style="list-style-type: none"> • 2 ms

Table 3.1 Survey acquisition parameters.

represented more regional trends (Figure 3.3).

3.2.1 Well Log Data

Both velocity and electrical logs are available for the 07-07-010-23W3 well. The electrical logs indicate repeated zones while the velocity log, when compared to the velocity logs from 01-04-010-22W3 and 04-01-011-24W3, indicates a velocity anomaly at this location as well as further evidence for the repeated zones.

Figures 3.4, 3.5 and 3.6 show various sections of the electrical log from 07-07. The

PROCESSING FLOW	
Demultiplex	
Amplitude Recovery	
Deconvolution	<ul style="list-style-type: none"> • spiking • 80 ms operator length
Statics	<ul style="list-style-type: none"> • elevation, refraction • datum = 1100 m
Velocity Analysis	
Normal Moveout Correction	
Mute	
Stack	
Migration	<ul style="list-style-type: none"> • Stolt fk • 100% stacking velocities
Filter	<ul style="list-style-type: none"> • bandpass: 10/15-70/80 Hz

Table 3.2 Basic processing flow.

anomalous regions are labelled Zones A and A', B and B', and C and C' with increasing depth. Based on the log character, the repeated zones indicate thrust faulting and in both the shallower zones (Figures 2.4 and 2.5 respectively), thickening occurs in the zone above the thrust fault (Zone A and B respectively). Thickening is not evident for Zone C (Figure 3.6).

These zones, with the thrust faults added into their overall thickness, were translated to the velocity log from 07-07. Removal of the repetitions (Zone B and Zone C) as well as the

removal of Zone A and A', results in an edited 07-07 well which closely matches the regional wells (Figure 3.7). This suggests that Zones B and C are indeed repetitions caused by thrusting. Zones A and A' are more of an enigma as their complete removal is apparently required to reduce the 07-07 log signature to that of the regional wells.

Comparison of the velocity logs also indicates that there is a velocity increase over the structure. This anomaly measures approximately 150 m/s greater than regional values down to the Mississippian level. This manifests itself as velocity pull-up in the seismic data as will be seen later (Section 3.2.3).

Drilling depths to identifiable horizons in both the 07-07 well and the regional wells indicates that the Mississippian is the first horizon that is not structurally deformed and so it defines the lowermost reaches of the structure. Thus the structure reaches to a depth of about 1300 m below the surface. In addition, the three wells were also used for correlation of horizons to the seismic data.

3.2.2 Well Log to Seismic Data Correlations

As mentioned previously, four seismic lines were available for interpretation over the structure: WV-011, WV-016, WV-017, and WV-021. Using the velocity logs from wells 01-04, 04-01, and 07-07 various geological horizons were correlated to reflectors on the seismic data. The 01-04 log, representing the regional velocity trend, was correlated to line WV-016 and WV-021. The projection distance to WV-021 was approximately 9 km but the well was located directly on line WV-016. The 04-01 log, also representing a regional well, was projected a distance of nearly 5 km to line WV-017 and correlated there. The 07-07 log, drilled on the structure, was projected approximately 700 m along strike around the estimated center of the structure to lines WV-017 and WV-021. Despite some long projection distances, the horizontal nature of the regional stratigraphy, with only a

very slight regional dip to the southeast, allowed for reasonable correlations of seven horizons including the Belly River (BLYRIV), the Milk River (MILKR), an A-horizon (HOR-A), bottom of the Second White Speckled Shale (BSWSPK), the Mannville (MANN), the Mississippian (MISS) and the Birdbear Formation (BRDBR). Also shown on the well correlations are a B-horizon (HOR-B) and the Viking Formation (VIK). These latter two were used to help in the comparison of the regional well logs to the 07-07 well log as discussed in the previous section but were not correlated to the seismic data as they did not prove to be very coherent reflectors.

Data from wells 01-04, 04-01 and 07-07 are shown in Figures 3.8, 3.9 and 3.10 respectively, which display each of the velocity logs, the corresponding zero-offset synthetic seismograms (based on a 30 Hz zero-phase Ricker wavelet) and the tie to the seismic data. Note that a velocity increase is represented by a trough (reverse polarity). The horizon lines (gray) mark the tops of the formations and are shown in dashes where the correlation is less clear.

The 07-07 well correlation was a particularly difficult one (Figure 3.10). Note that the 07-07 well was used to correlate reflectors deeper than MILKR since shallower reflections could not be seen clearly on the seismic data. Also labelled on the 07-07 well correlation are the repeated zones mentioned previously. However, none of the repeated zones were evidenced in the seismic data from lines WV-017 and WV-021 to which the well was correlated. Apparently, the structure is complex enough, and perhaps asymmetric enough, that even the relatively small 700 m projection distance for the well log is too far for reliable correlation of these thrust structures. The strength of the correlations for events shallower than VIK actually hinges on the character and continuity of these reflectors from the regional correlations to within the structure itself. The continuity of these reflectors is quite good and their character fairly definitive in making these correlations.

3.2.3 Seismic Data Interpretation

Once the basic correlations from the wells to the seismic was performed it was possible to concentrate on the seismic lines themselves. Comparison of lines WV-017 and WV-021 demonstrated a static time shift of 60 ms at their tie point. The time shift is probably due to different processing flows used by the two processing contractors involved. Nonetheless, it was not difficult to correlate horizons between the two lines.

Figures 3.11 and 3.12 show the uninterpreted and interpreted migrated sections of lines WV-017 and WV-021 respectively. Figure 3.13 shows the portions of lines WV-011 and WV-016 used in the interpretation. Using an average velocity value of 2500 m/s to the MISS based on well data, the sections were scaled and plotted such that there is nearly a one-to-one correspondence between the time axis in seconds and depth in kilometres resulting in nearly no vertical exaggeration. Horizon markers are shown in solid dark lines while faults are indicated by dashed lines with arrows depicting relative movement. The projected well locations, line ties and major morphological features are also labeled. All four lines, being 2-D, likely suffer from side scatter interference off of structures outside the plane of the lines. This is likely a greater problem with lines WV-011 and WV-016 as they lie tangential to the core of the structure. These areas probably experienced more rock movement across the plane of the seismic sections complicating their interpretation. Labelled on the interpretations of WV-017 and WV-021 are some morphological characteristics based on the hypothesis that the structure was formed by a meteorite impact. These include the rim, the trough of the structure, and the central uplift which is depicted as the region with no coherent reflectors, all of which are indicative of a complex crater. The validity of this model will be discussed in Section 3.3 along with other possibilities.

3.2.3.1 Horizon Description

The BLYRIV horizon is the shallowest correlateable reflector in the sequence. There is also some suggestion of coherent reflectors shallower in the sections but the data quality is poor here. Disruption of the BLYRIV horizon by listric normal faults is apparent as the rim of the structure is encountered. These faults form terraces from the outer rim to the trough which is located at about CDP 641 and 941 on line WV-017 (Figure 3.11) and CDP 271 and 571 on line WV-021 (Figure 3.12). The trough appears on both sides of the structure's core on both WV-017 and WV-021 suggesting that it surrounds the entire core. At depth, and closer to the center of the structure, these listric faults delineate large competent blocks of rocks which have been thrust and rotated upwards toward the surface and into the structure's core. The flanks of the central, disrupted zone shows evidence of further normal faulting away from the core. The formation then becomes uncorrelateable across the structure's center where complete disruption of the subsurface has resulted in chaotic, scattered reflections.

The MILKR, HOR-A, BSWSPK and the MANN horizons represent good regional markers which, by their deformation in the structured area, help to delineate the trajectory of the major faults seen in the Belly River horizon mentioned above. As can be seen on lines WV-017 and WV-021 (Figures 3.11 and 3.12), the listric rim faults penetrate to substantial depth and delineate the outer-most extent of the structure. The MANN horizon is disrupted by rim faults on all four lines and shows evidence of being thrust on line WV-017 (CDP 770, 1.2s; Figure 3.11) as well as normally faulted in graben-type structures (e.g., line WV-016, CDP 1350, 1.2s; Figure 3.13). As with the BLYRIV, these horizons also become uncorrelateable through the most disrupted portion of the structure's core.

The MISS and BRDBR horizons also represent regional reflectors which underlie the deepest portion of the central uplift. Both of these horizons occur at shale-carbonate interfaces with a corresponding velocity contrast of about 3000 m/s. On line WV-017 (Figure 3.11) the Mannville is also more continuous beneath the central uplift indicating that structural deformation becomes shallower further from the center of the structure giving it a bowl shape in three dimensions. Both the MISS and BRDBR reflectors are coherent except for some slight normal faulting of the MISS apparent on line WV-021 (Figure 3.12).

3.2.3.2 Time Structure

Both the Mississippian and Birdbear horizons show about 55 ms of two-way time structure relative to their regional positions (Figures 3.11 and 3.12). In both cases, and for both formations, the time structure takes the form of pull-up beneath the central uplift region. The 150 m/s velocity anomaly over the structure that was mentioned previously in Section 3.2.1 is enough to account for this velocity pull-up in the lower horizons. Reasons for this velocity increase over the structure will be examined in Section 3.3.

The circular nature of the structure becomes clearer once the 2-D lines are combined to create a 3-D time-surface map. This was accomplished for the Belly River horizon by digitizing it on each line, assigning a surface location from the base map and then gridding the data. The resulting interpolated time structure map is shown in Figure 3.14. This diagram would have been aided by a denser dataset but the circular shape and general morphology of the crater can still be seen.

3.2.3.3 Gravity Anomaly

A gravity profile was acquired over the White Valley structure by Saskatchewan Energy and Mines and the University of Saskatchewan primarily over the central part of the

structure (see Figure 3.3 for its location). The resulting Bouguer gravity profile is illustrated in Figure 3.15. The profile indicates a 2.75 mgal anomaly over the center of the structure and is bilaterally symmetric. The profile can be modelled as the result of a density anomaly beneath the surface which I assume here to be a sphere or vertical cylinder for simplicity. The gravity anomaly associated with a spherical anomaly stems from the gravity anomaly of a point mass which, in general, is expressed by

$$\Delta g_r = \frac{Gm}{r^2}, \quad (3-1)$$

where Δg_r is the gravitational attraction in the direction of the mass at a distance r from the mass. G is the gravitational constant defined to be $6.67 \times 10^{-11} \text{ m}^3 \text{ kg}^{-1} \text{ s}^{-2}$. However, when gravity measurements are being taken at the surface, only the vertical component of the gravity is measured. Thus the measured gravity anomaly is

$$\Delta g = \frac{Gm}{r^2} \cos \theta, \quad (3-2)$$

where θ is the angle between the vertical component and total gravity vector. If we let z be the vertical distance to the point mass and x be the horizontal distance to the point mass, then $\cos \theta = z/r$ and $r^2 = (x^2 + z^2)^{1/2}$ which by substitution into Equation 3-2 gives

$$\Delta g = Gmz(x^2 + z^2)^{-\frac{3}{2}}. \quad (3-3)$$

However, we are primarily interested in the maximum gravity anomaly which occurs directly over the anomaly where $x = 0$. Thus the maximum gravity anomaly is given by

$$\Delta g_{\max} = \frac{Gm}{z^2}, \quad (3-4)$$

in agreement with Equation 3-1. Equation 3-4 is the maximum gravity anomaly of a spherical mass beneath the surface where z represents the vertical distance to the center of the *excess* mass, m . This excess mass (which is negative for a mass deficiency), can be calculated from

$$m = \frac{4}{3}\pi r_m^3 \Delta\rho, \quad (3-5)$$

for a spherical anomaly. Substituting Equation 3-5 into Equation 3-4 and solving for $\Delta\rho$ gives

$$\Delta\rho_{\text{sph}} = \frac{3\Delta g_{\text{max}} z^2}{4G\pi r_m^3}, \quad (3-6)$$

where $\Delta\rho_{\text{sph}}$ is the required density anomaly to produce a maximum gravity anomaly, Δg_{max} , for a spherical body with its center at a depth, z , and radius, r_m .

Similarly, Dobrin (1976) gives a maximum gravity anomaly of

$$\Delta g_{\text{max}} = 2\pi G \Delta\rho \left(h - r_m + \sqrt{h^2 + r_m^2} \right), \quad (3-7)$$

for a vertical cylinder of height, h , and radius, r_m . Rearranging Equation 3-7 to solve for $\Delta\rho$ gives

$$\Delta\rho_{\text{cyl}} = \frac{\Delta g_{\text{max}}}{2\pi G \left(h - r_m + \sqrt{h^2 + r_m^2} \right)}, \quad (3-8)$$

where $\Delta\rho_{\text{cyl}}$ is the vertical cylinder density anomaly which gives rise to Δg_{max} . We see from Equations 3-6 and 3-8 that only Δg_{max} is a known quantity from the actual gravity survey. However, the values for z , r_m and h can be estimated by the following.

For the spherical model, the seismic data show that the chaotic portion of the structure over which the gravity survey was performed has a radius of approximately 1000 m (Figure 3.11). The vertical distance to the center of the anomalous zone, z , can be estimated from the gravity anomaly half-width, $x_{1/2}$. The half-width is defined as the horizontal displacement from the point at which the maximum gravity anomaly occurs to the point at

which the gravity anomaly reaches half its maximum value (Kearey and Brooks, 1991).

Thus at $x = x_{1/2}$, $\Delta g = \Delta g_{\max}/2$ (Figure 3.15). Substituting these values into Equations 3-3 and 3-4 and solving for z gives

$$z = 1.3048x_{1/2}. \quad (3-9)$$

From the gravity survey (Figure 3.15), the half-width is estimated to be 750 m giving an estimated depth to the anomaly's center of nearly 980 m using Equation 3-9. Therefore, using $z = 980$ m, $r_m = 1000$ m, and $\Delta g_{\max} = 2.75 \times 10^{-5}$ m/s² in Equation 3-6 gives a density anomaly of 94.5 kg/m³ for a spherical anomaly.

In the case of the vertical cylinder model, I take the depth of the structure, 1300 m, to be the height, h . As with the spherical model, the seismic data show the radius of the chaotic portion of the structure to be about 1000 m which I use as an estimate for the radius of the vertical cylinder. Similarly, the gravity anomaly is taken from the gravity survey giving $\Delta g_{\max} = 2.75 \times 10^{-5}$ m/s². Using these values in Equation 3-8 gives a density anomaly of 33.8 kg/m³ for a vertical cylinder which outcrops at surface.

The measured density logs in the 07-07 and 04-01 wells give an average difference in the density of about -50 kg/m³ representative of an overall decrease in density over the structure. The disparity between the modelled results and the well data is probably because the gravity survey does not extend beyond the rim of the structure. The positive anomaly is the result of density differences between the trough and the central chaotic portion of the structure whereas the wells sample the regional geology and the central portion of the structure. Combining these two datasets suggests that while there is a density decrease over the structure compared to regionally, the greatest density decrease occurs within the trough zone of the structure which shows a negative anomaly as compared to the center of

the structure. The fact that the estimated depth to the center of the anomalous zone is deeper than half the total depth of the White Valley structure suggests that more of the excess mass lies near the bottom of the structure or that the structure is buried by post-impact sediments which do not contribute to the gravity anomaly.

3.2.3.4 General Morphology

From the interpreted seismic lines, some general morphological characteristics can be identified. The question of structural symmetry is one which must be viewed carefully as the degree of symmetry may give clues to the structure's origin. Recall from the time-structure map (Figure 3.15) that the gross morphology appears to be largely circular with a raised central core. These features are consistent with the seismic data in Figures 3.11 and 3.12. The circular shape of the structure is, to some extent, also suggested by the erosional remnant ridge which leaves an arcuate imprint on local drainage patterns seen on the air photo (Figure 3.2). Thus we might feel that the structure is quite symmetric. However, on a smaller scale, we see on the seismic data that the expected symmetry (bilateral in the case of seismic lines which lie diametrically over the structure) breaks down. For example, a unique feature seen on line WV-021 is the portion of heavily rotated beds near the central core approximately located from CDPs 241-301 at about 0.8-1.1 s (Figure 3.12). This region of the subsurface appears to have suffered greater rotational deformation than corresponding areas on the other side of the central uplift and on line WV-017 (Figure 3.11). While the structure might be considered bilaterally symmetric in that the rim and trough of the structure occurs on either side of its core, which in itself can be divided symmetrically in the middle, some internal structures like these rotated beds occur on one side of the structure only. Recall also that the repeated zones of the 07-07 well log do not correlate to the seismic data of lines WV-017 and WV-021 again indicating a degree of asymmetry even over relatively small projection distances. So the structure, while

symmetric on a large scale in terms of very general morphology, appears to be asymmetric when looked at on a smaller scale.

More quantitatively, we can obtain structural dimensions from the seismic data. At the BLYRIV horizon, the rim of the structure measures about 6.3 km in diameter. Projecting the most distal rim faults to the surface suggests a greater rim diameter of some 7.5 km, more in line with that which is estimated from the aerial photograph (Figure 3.2). At the BLYRIV horizon, the annular trough measures about 4 km in diameter and the central uplift is about 2.6 km wide. Projecting these features to surface leaves the trough at about 4 km in diameter but decreases the diameter of the core of the structure to about 2 km. The maximum depth of the chaotic portion of the structure appears to be about 1.3 km as this is the depth to the Mississippian, which was penetrated by drilling in the 07-07 well at regional levels.

3.3 DISCUSSION

After compiling the various geophysical and geological data, we must try to combine these into a coherent whole in order to explain the possible origin of the structure. When first investigated, the structure was thought to be the result of glacial thrusting (Christiansen and Whitaker, 1976). However, subsequent work by Gent (1992) dismisses this concept and instead suggests that a kimberlite model is more likely. Explorationsists from Mark Resources Inc. and Enron Oil Ltd. suggested a meteorite impact model for the structure to which Gent et al. (1992) allude. I will look again at these two models in detail and argue that the kimberlite concept is less likely and generally inconsistent with the seismic data.

3.3.1 Kimberlite Origin

Kimberlites form by the rapid rise of lithospheric or asthenospheric magma to the surface with ascent rates on the order of 10-30 km/hr (Eggler, 1989). Explosive release of gases

and fluids sometimes accompanies this magma rise resulting in the so-called explosion pipe (Milashev, 1988). For my purposes here, I will only consider those pipes that break the surface, leaving an identifiable surface structure. I also consider the gross morphology of such a pipe as these features are more likely to be identifiable on seismic data.

The general morphology of explosion pipes is that of an inverted cone, tapering with depth. In detail, several morphological subclasses have been identified based largely on surface expression (e.g., oval, elliptical, etc.) although these haven't been generally excepted (Hawthorne, 1975; Milashev, 1988). Figure 3.16 depicts a general model for a typical kimberlite. Major structural features include a simple crater at surface surrounded by a raised rim of tuff material, while at depth, field studies have indicated that the sides of the pipe dip steeply at angles of 80-85° regardless of country rock type (Hawthorne, 1975; Milashev, 1988). The pipe tends to be filled with tuffs near the surface, followed by explosion breccias and then massive kimberlite at depth. Included in this general matrix are large blocks of wall rock although they are usually restricted to the tuffs and breccias closer to surface (Hawthorne, 1975; Milashev, 1988). Milashev (1988) also suggests that for most pipes, their roots penetrate to about 2 km of depth.

Most of the major structural features associated with explosion pipes have been modelled in fluidization experiments. Woolsey et al. (1975) describe a series of such experiments and the resulting surface and subsurface structural components associated with the "pipes" they create. Along with the major features noted above, their experiments indicate that formerly horizontal strata are tilted toward the main pipe (Figure 3.17). However, field measurements have shown that some of the country rocks very close to large pipes (usually within a few 10s of meters) may be tilted away from the pipe (Milahev, 1988). Fracturing around the pipe is common close to the pipe except for radial fracturing which may extend

for several pipe radii. Total vertical displacements caused by the fracturing is usually less than a few tens of meters and is usually downward from regional levels (Milashev, 1988).

It is possible to contrast many of these features with the morphology of the White Valley structure. First and foremost, the large size of the structure, with a projected diameter of 7.5 km, is much greater than expected for kimberlite pipes which usually reach a maximum diameter of about one kilometre (Milashev, 1988). The general form of the White Valley structure is that of the rim-trough-uplift configuration which is bilaterally symmetric in cross section about the central vertical axis - typical of a complex crater configuration. Explosion pipes demonstrate a bowl-shaped crater at surface - typical of the simple crater configuration. This is even largely true of multiple generation kimberlites which exhibit more than one occurrence of volcanic activity (Milashev, 1988). The cone shape of explosion pipes have flanks which dip at 80-85° whereas the core of the White Valley structure is more bowl-shaped with flanks dipping at perhaps 50-60°. At White Valley, vertical displacements of horizons within the central core are approximately 450-620 m above regional levels and the well data shows evidence of major thrust faulting episodes during the formation of the structure. These displacements are difficult to explain within the context of the kimberlite model where regional stratigraphy is usually tilted toward the pipe. It is also difficult to reconcile thrust faulting with the explosion pipe model. Beds along the flanks of the White Valley structure's core throughout the depth of the structure, are all dipping away from the core to a distance of some 500 m. This attitude reverses itself through the trough. For kimberlites, this phenomenon, when it does occur, is thought to be a near surface effect that occurs within a few tens of meters from the pipe.

These differences in gross morphology make it difficult to reconcile the seismic data over the White Valley structure to the kimberlite model. The lack of any kimberlitic material in any of the wells makes this concept even less likely.

3.3.2 Meteorite Impact Origin

The overall morphology of the structure appears to fit that of a complex impact crater with all the major features imaged in the seismic profiles including normal rim faults stepping down to an annular trough and a central, seismically incoherent zone of uplift (Westbroek et al., 1996). In detail, the repeated sections identified in the log signatures of the 07-07 well as Zones B and C are interpreted as thrust sections of rock - evidence of the structural deformation taking place during the modification stage of the cratering process. Slumping of the transient crater's walls and uplift of the transient crater's bottom may result in a compressional stress regime at the center of the structure, causing rock units to be thrust on top of one another. This phenomenon has been identified at proven meteorite impact structures such as Eagle Butte (Sawatzky, 1972; Lawton et al., 1993) and Avak (Kirshner et al., 1992). This compression may also be responsible for the velocity increase seen in the 07-07 log as it reduced impact-induced porosity. However, the rotation of higher velocity rock units into the region of uplift and perhaps later cementation of fractures contributed to the overall average velocity increase in the central uplift region.

As noted in Section 3.2.1, the complete removal of Zone A and A' is necessary to reduce the 07-07 log signature to the regional wells. This may simply be representative of the chaotic nature of the crater's structure so close to the central uplift or perhaps again indicative of post-uplift slumping and interfingering of material along the sides of the uplift. This is illustrated in the interpretation by normal faulting along the flanks of the central peak at the BLYRIV level.

Asymmetry seen in the seismic data with respect to the fault patterns and structural deformation of rocks is not easily explained as little experimental work has been done regarding high-velocity impact in layered media. However, heterogeneities and anisotropic

rock properties in target rocks cause them to react uniquely, particularly to the modification stage of crater formation, and likely contribute to asymmetry in the final crater morphology. The direction and angle of impact also affects crater symmetry with the central uplift becoming skewed in the direction from which the impacting bolide came. Even atmospheric effects can lead to alterations in surface crater symmetry although deeper crater structures are unlikely to be affected. Such atmospheric phenomena are apparent in the asymmetric surface morphologies and ejecta deposits of Venusian craters (Schaber et al., 1992, Schultz, 1992) and can give clues to the incident direction of the meteorite. Steeper, more numerous rim faults toward the north may be indicative of the downrange edge of the structure. However, the current quantity of seismic and well data and a lack of observable ejecta deposits make it difficult to ascertain the direction of the impacting bolide in the case of White Valley.

Although not studied in detail, the gravity survey indicates a 2.75 mgal positive anomaly above the structure. The gravity profile itself shows symmetry similar to the overall morphology of the structure. Grieve and Pilkington (1992) site several examples of impact structures which indicate a residual negative gravity anomaly followed by a more positive anomaly over the central uplift. For example, Gosses Bluff, Australia has a -5.5 mgal anomaly with a central peak anomaly of -3.5 mgal, a difference of 2 mgal. Similarly, Upheaval Dome, U.S.A., has a 3 mgal anomaly over the central peak (Grieve and Pilkington, 1992). The survey performed at White Valley covers only a portion of the trough and the central peak of the structure. When modelled as a spherical or vertical cylinder anomaly, the data suggest a density increase through the center of the structure of some 30 to 100 kg/m³. Combined with the density comparison between the regional 04-01 and the 07-07 well which shows a 50 kg/m³ decrease between the regional terrane and the central uplift, a profile becomes evident for which the structure demonstrates an overall density decrease compared to regional values with a density increase through the central

peak. This gives rise to a similar gravity profile as described in Pilkington and Grieve (1992). It is not known what the regional gravity was at the survey site, nonetheless, a 2.75 mgal anomaly over the central peak of an impact structure is not unusual. This may be due to the rotation of deeper, relatively competent blocks of rock (and hence of somewhat greater density) into the central peak, compression of rocks through the central uplift as compared to extension of rocks through the trough during transient crater modification, and possibly post-impact alteration of the rock making up the central uplift. More detailed modelling of the gravity data would be required in order to better constrain the interpretation of this dataset.

Using morphometric measurements from the White Valley structure and the scaling criteria introduced in Chapter 2, it is possible to see how well this particular structure scales to known impact craters. From Equation 2-16 and using the 7.5 km projected diameter, the depth of the crater should be some 220 m. Due to the poor quality of the shallow portion of the seismic sections as well as possible erosion of the structure, the true crater surface is unknown, and thus its depth can not be determined. However, downdrop within the trough at the BLYRIV horizon indicates that the depth of the crater should be greater than 100 m. Structural uplift is calculated from Equation 2-18 to be 685 m. Since the BLYRIV horizon is no longer imaged across the central peak, and is no longer present in the 16-06 well, the data indicate a structural uplift of more than 450 m. If the MILKR is projected to the surface, then some 620 m of structural uplift occurred, closer to the value predicted by scaling. The most controversial calculation is that pertaining to the transient crater diameter. Equations 2-14 and 2-15 give a range of 4.5 km and 6.85 km, respectively, for the diameter of the transient crater. This gives a corresponding range in the transient crater depth (using Equation 2-6) of about 1500 to 2300 m. Considering that the seismic data indicate a total depth of 1300 m for the structure, an even deeper transient crater must either indicate some 200 to 1000 m of erosion to accommodate the transient crater size, or

alternatively, the scaling criteria are not suitable for this calculation. The central peak diameter can be estimated from Equation 2-19 and gives a range of 1.6 to 1.9 km. As measured from seismic data, the central peak appears to be about 2 km when the structure is projected to the surface, in reasonable agreement with the calculated estimate. Erosion and post uplift slumping of the central core might account for the measured value being at the high end of the calculated range. These measurements and scaling calculations are summarized in Table 3.3.

3.4 CONCLUSIONS

The structure at White Valley in southeastern Saskatchewan, does not appear to conform to the morphology expected for a kimberlite pipe. It's large size, complex crater morphology, structurally uplifted core, and extensive terraced rim are all difficult to reconcile with the kimberlite pipe model.

Without petrological evidence of shock metamorphic features in the target rocks, the impact origin of this feature can not be proven. Nonetheless, the structural anomaly seen on the 2-D White Valley seismic data shows many of the morphological characteristics of a complex impact crater. It has a circular rim, an annular ring synform and a raised central uplift which in turn, shows evidence of possible slumping along its flanks. The structure's profile is evidenced in the topography of the area and indicates a rim crest diameter of about 7.5 km. The ring synform has an outer diameter of about 4 km while the central uplift is

Dimension	Measured Result	Scaling Equations
Depth	>100 m	220 m
Structural Uplift	620 m	685 m
Central Peak Diameter	2 km	1.6-1.9 km
Transient Crater Diameter	N/A	4.5-6.85 km
Transient Crater Depth	≤ 1300 m	1500-2300 m

Table 3.3 Comparison of measured dimensions and results from the scaling equations for the White Valley structure. Values are based on a rim diameter of 7.5 km.

about 2 km wide when projected to the surface. The amount of structure decreases with increasing depth to a maximum of about 1300 m. Pull-up of the predominantly coherent horizons beneath the central uplift appears to be partially due to a 150 m/s velocity anomaly between regional values and the central uplift. Most of the disturbed zone involves the clastic portion of the sedimentary column. The best age determination from the current data indicates the impact occurred less than about 60 Ma ago. Although most of the scaling criteria pertaining to the final geometry of the structure fit the available data well, the greatest discrepancy occurs when scaling criteria are applied to estimate the size of the transient crater. The calculated transient crater, based on the rim diameter of the structure projected to the surface, does not fit the seismic data well unless a great deal of post-impact erosion is invoked. This discrepancy may reflect an actual erosional component to the post-impact history of the structure or an inherent inadequacy with the chosen scaling criteria. It seems more likely that the transient crater had a depth less than the total depth of the structure, perhaps some 600 to 700 m. The scaling equations were based on laboratory experiments in saturated sand which may not reflect the response of the lithified, stratified, clastic, target rocks present at White Valley. The gravity data indicates an anomaly profile consistent with an impact crater. Modelled as a sphere or vertical cylinder, the anomaly suggests a 30 to 100 kg/m³ density increase through the central uplift compared to the trough while well data indicates an overall density decrease between regional rocks and the central uplift of some 50 kg/m³. Although simplistic, these models seem to indicate that the gravity anomaly can be related to a typical density anomaly in the subsurface caused during crater formation. Combining this interpretation more rigorously with other geophysical data and the regional geological model may lead to a better understanding of the structural elements of the crater and whether or not the scaling criteria, particularly those which attempt to bridge the gap between the modification stage and the excavation stage, are appropriate for describing the morphometry of the structure. Nonetheless, based on the seismic data used in this interpretation, an impact origin is favoured.

PERIOD		FORMATION		LITH.	
Tertiary		Ravenscrag		Shale	
Cretaceous	Late	Battle/Whitemud		Sandstones and Shales	
		Eastend			
		Bearpaw			
		Belly River			
		Milk River			
	Early	Colorado GP		Shale	
		Mannville GP		Sandstone	
Jurassic		Vanguard *		Shale	
		Shaunavan *			
		Gravelbourg *			
Triassic	Late	Watrous			
	Mid.				
Mississippian		Charles *		Carbonate	
		Mission Canyon *			
		Lodge Pole *			
Devonian	Late	Three Forks GP		Shale	
		Saskatchewan GP	BirdBear *		Carbonate
			Duperow		
	Mid.	Manitoba GP			
		Elk Pt. GP			

Fig. 3.1 Generalized stratigraphy of southeastern Saskatchewan. The Birdbear formation (grey) was the target of the 07-07 well. The asterixes denote oil-bearing formations (from AGAT Laboratories, 1988a).

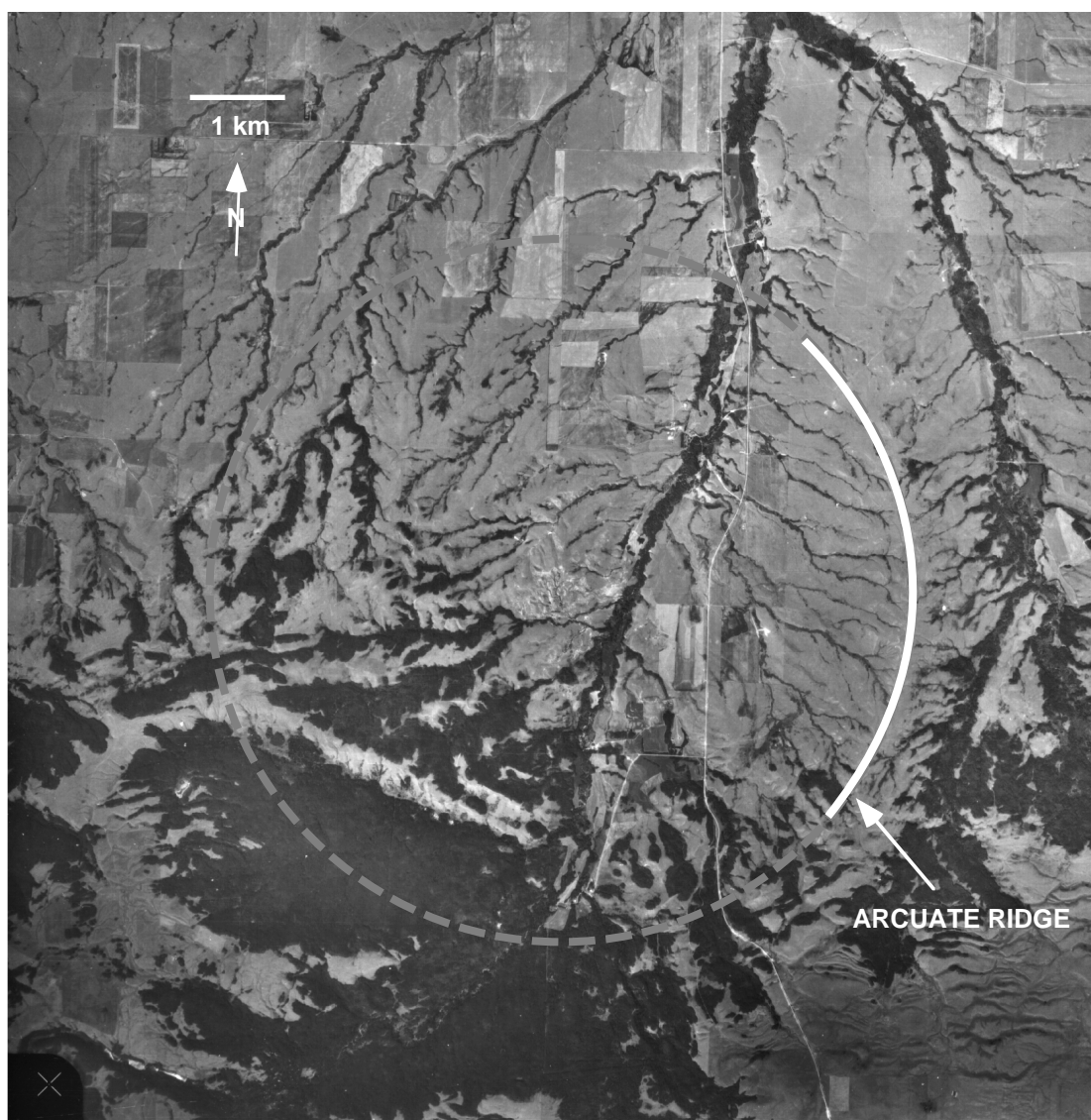


Fig. 3.2 Air photo over the White Valley structure showing a partially arcuate ridge to the east of the structure's center (solid line) which projects to a circle approximately 7.5 km in diameter (dashed line). The scale of the photo is approximately 1:80000.

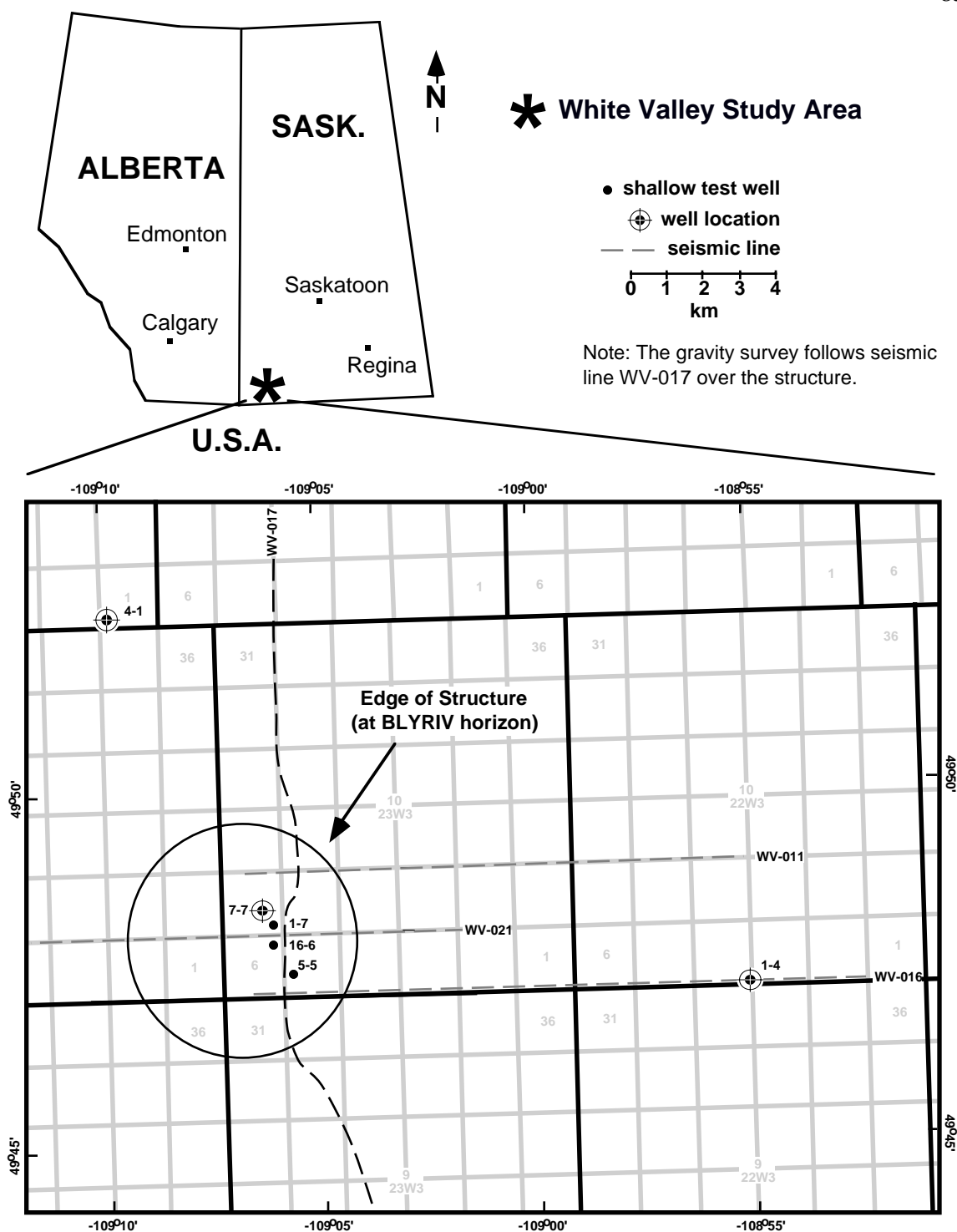


Fig. 3.3 Base map of the White Valley study area showing the seismic lines and the 07-07 well. The regional 01-04 and 04-01 wells are to the southeast and northwest of the base map respectively. The outline of the structure is depicted and is located at approximately 49°48'00'N, 109°06'30'W.

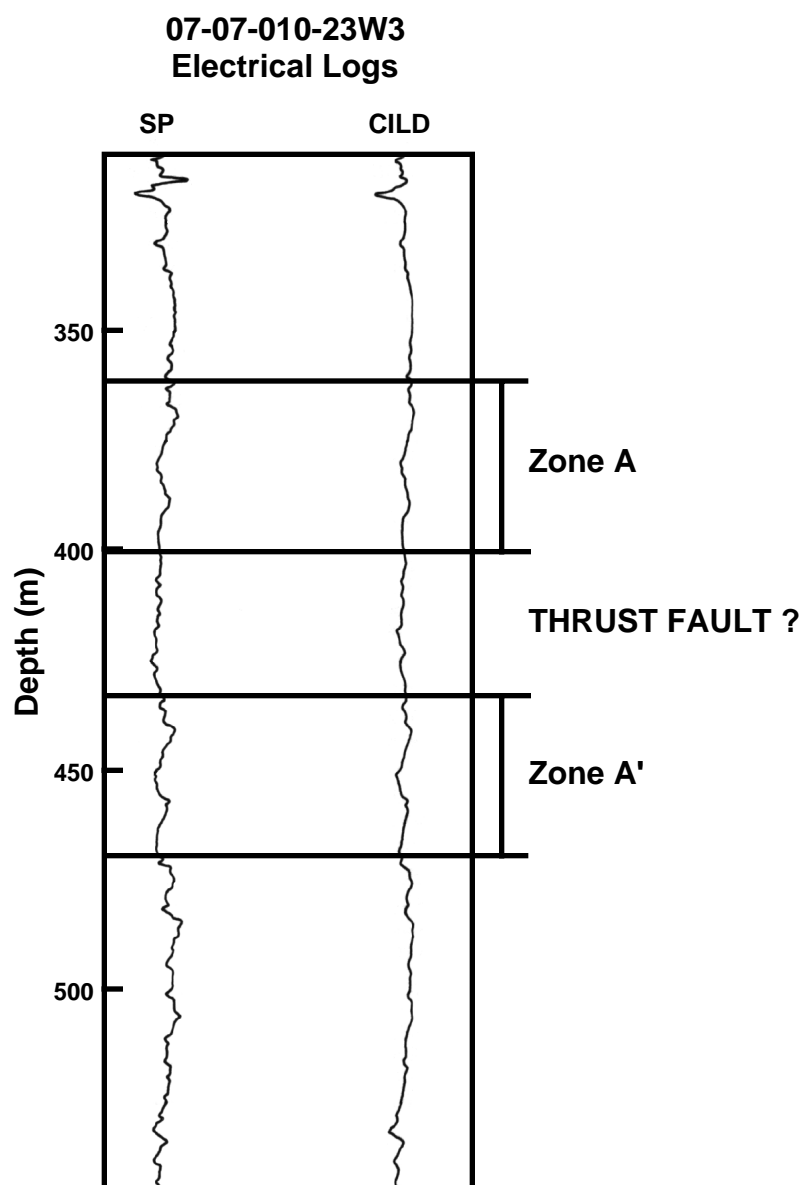


Fig. 3.4 The shallow portion of the electrical log from the 07-07 well. Zone A' and its repeat, Zone A are indicated. Whether or not this represents a true repeated zone divided by a detachment (the thrust fault) or an entire zone of allocthonous material from the top of Zone A to the bottom of Zone A' is discussed in the text.

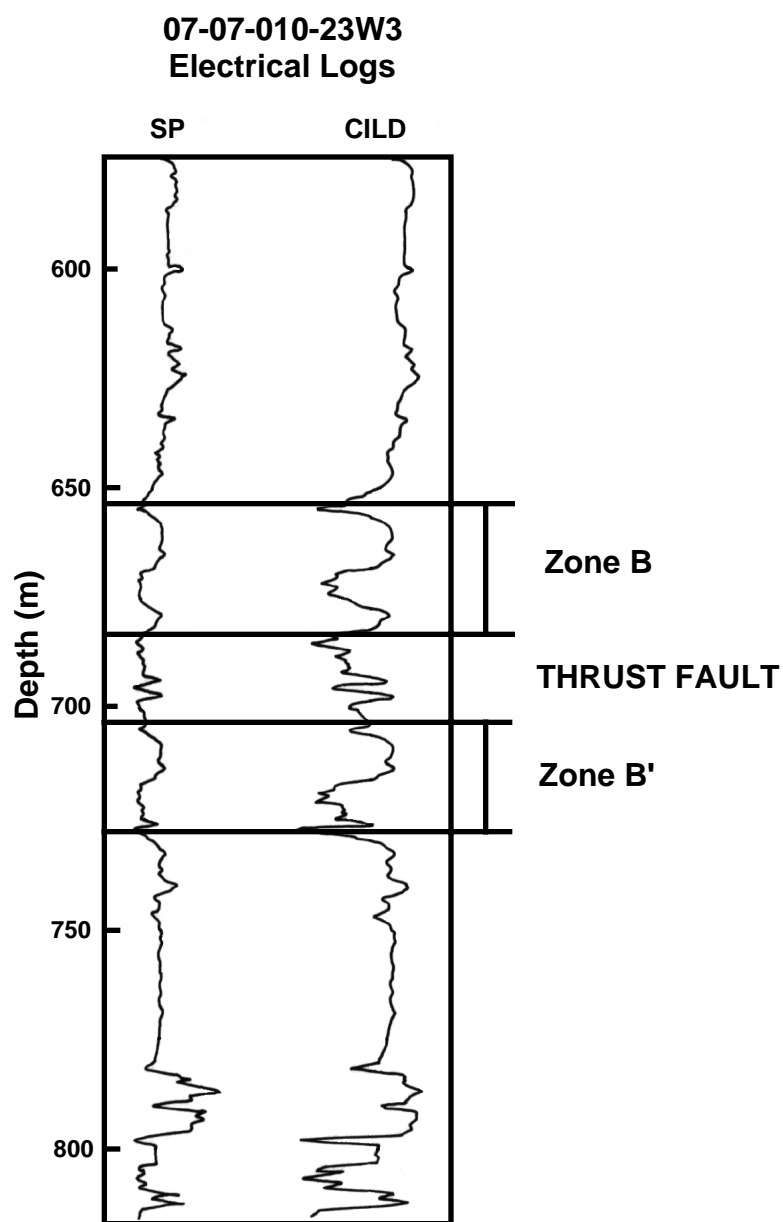


Fig. 3.5 The middle portion of the electrical log from the 07-07 well. Zone B' and its repeat, Zone B, are indicated along with the thrust fault separating the two.

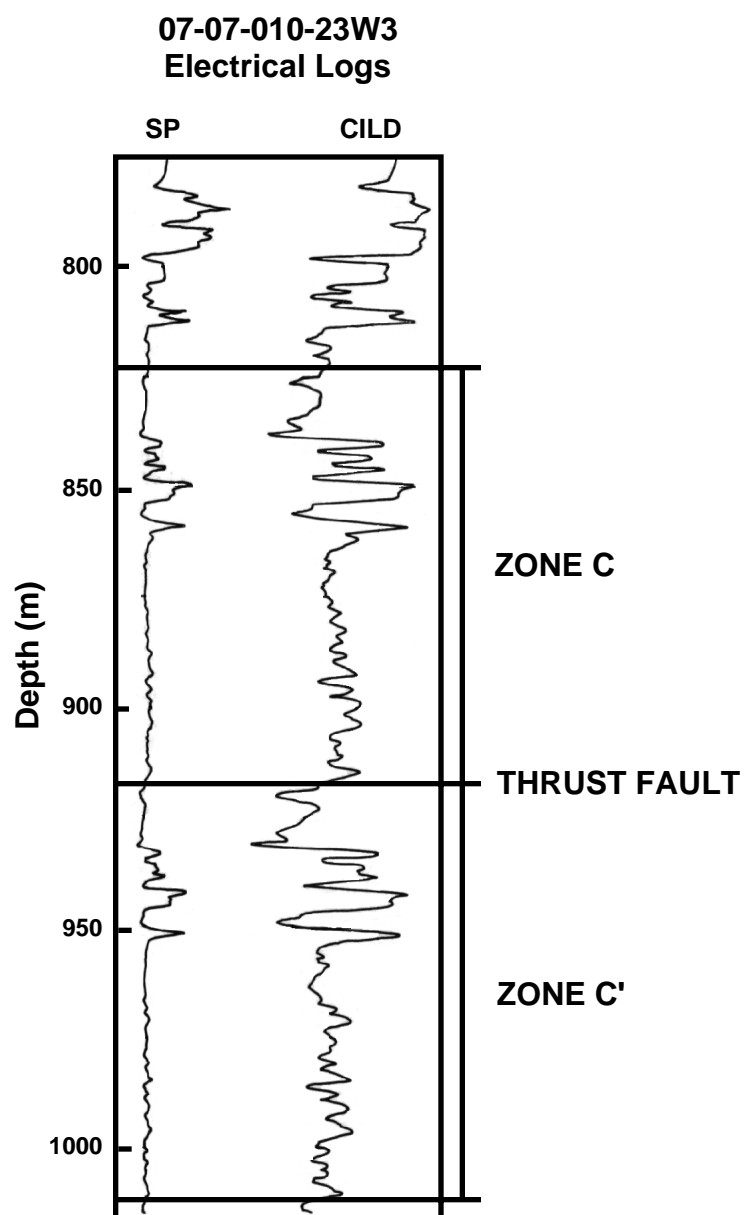


Fig. 3.6 The deepest portion of the electrical log from well 07-07. Zone C and its repeat are shown with the detachment between them.

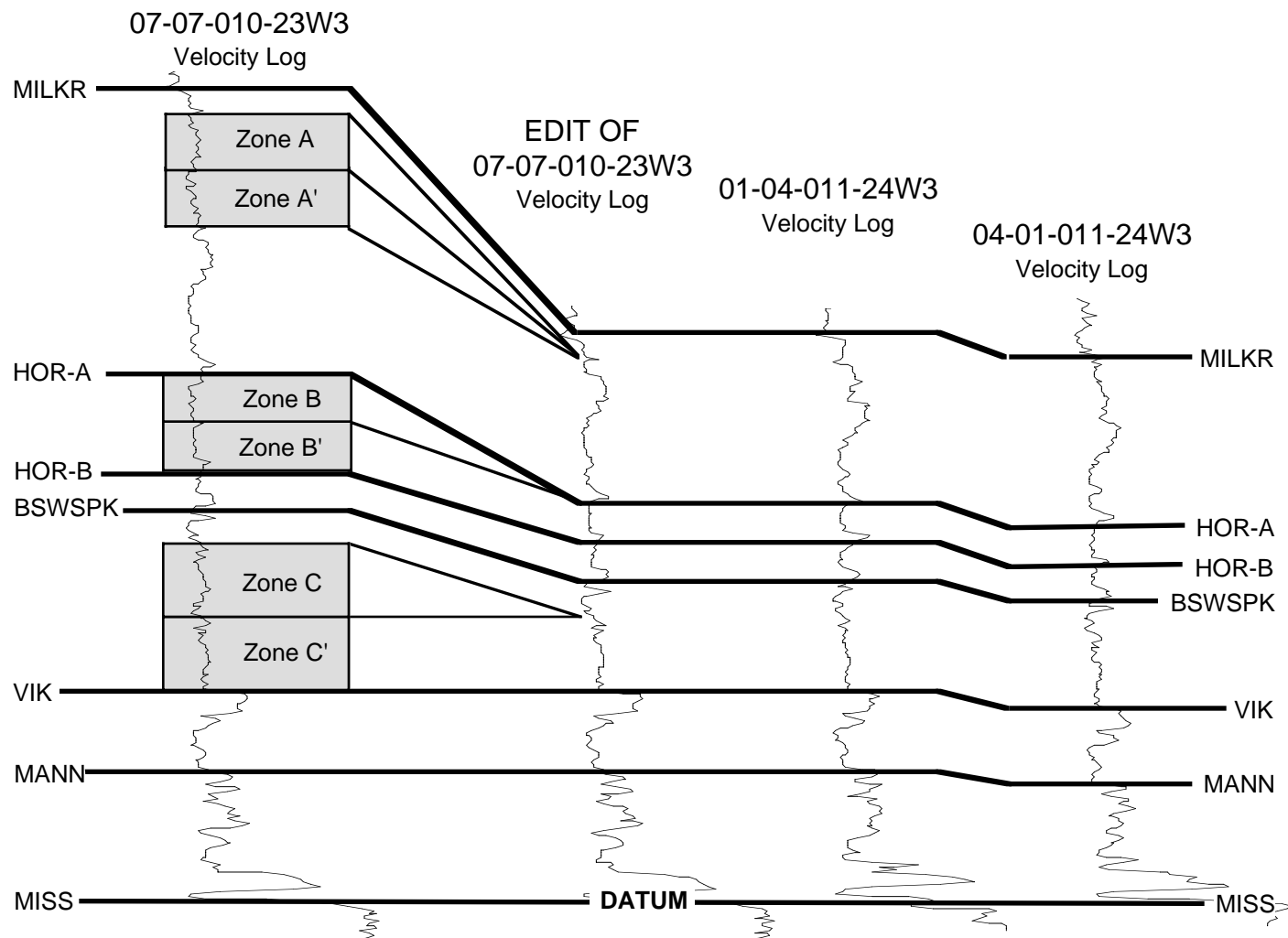


Fig 3.7 Comparison of the 07-07 velocity log and the regional 01-04 and 04-01 velocity log after removal of Zones A, A', B, and C. The edited 07-07 log has a signature very similar to the regional well logs.

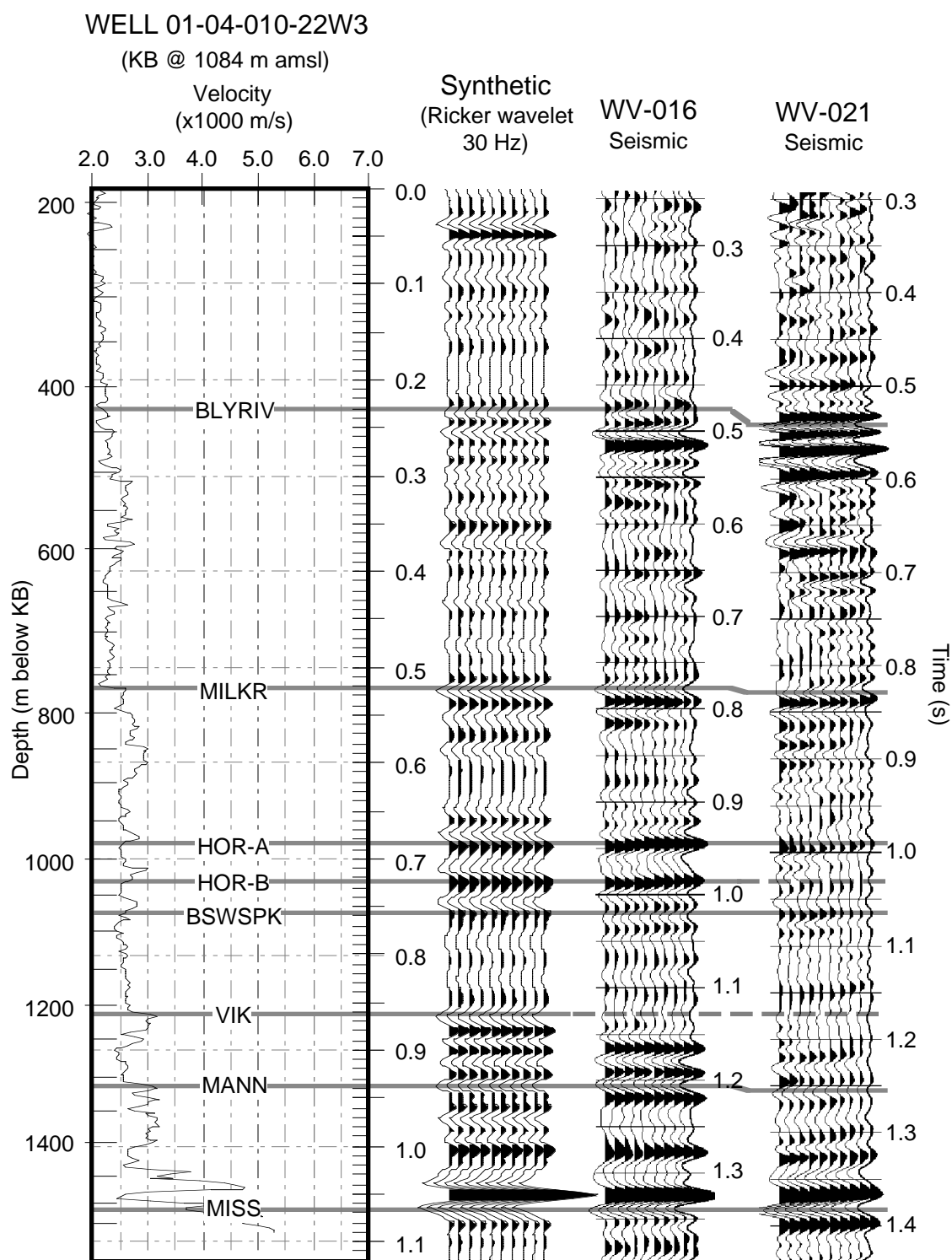


Fig. 3.8 Correlation of the 01-04 sonic log and the zero-offset synthetic seismogram with the seismic from WV-021 and WV-016. Note that the data are reverse polarity.

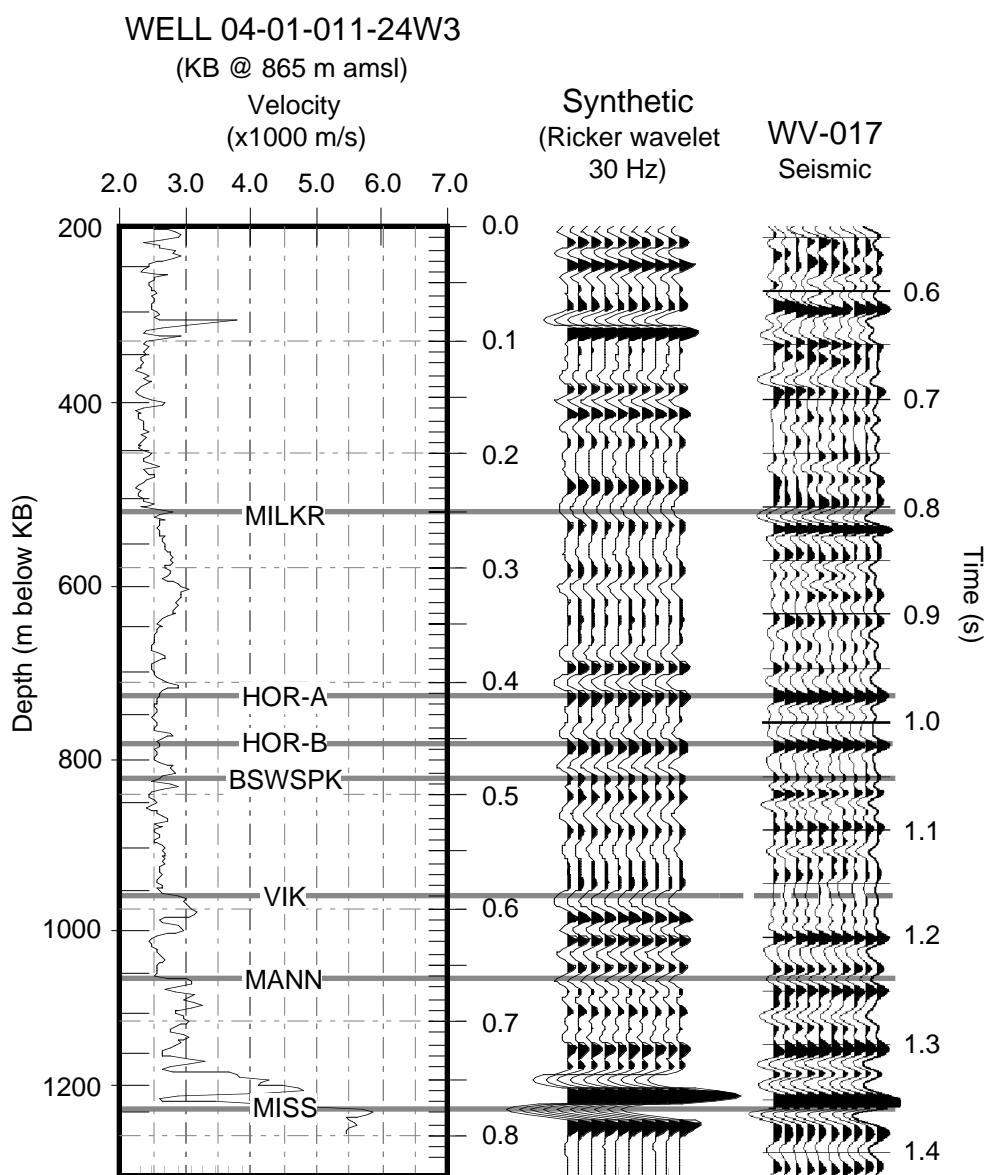


Fig. 3.9 Correlation of the 04-01 sonic log and the zero-offset synthetic seismogram with the seismic from WV-017. Note that the data are reverse polarity.

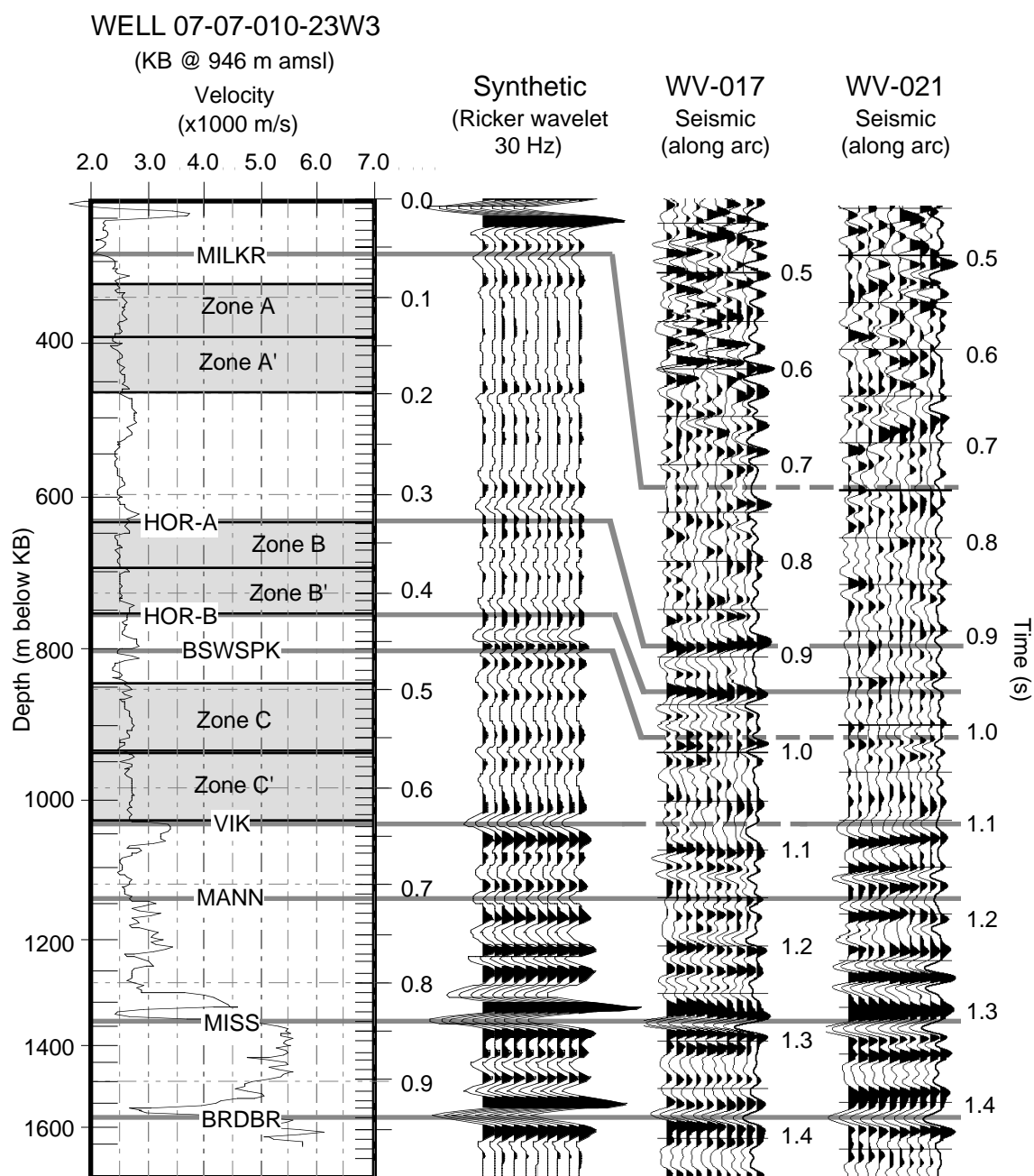


Fig. 3.10 Correlation of the 07-07 sonic log and the zero-offset synthetic seismogram with the seismic from WV-017 and WV-021. Note that the data are reverse polarity.

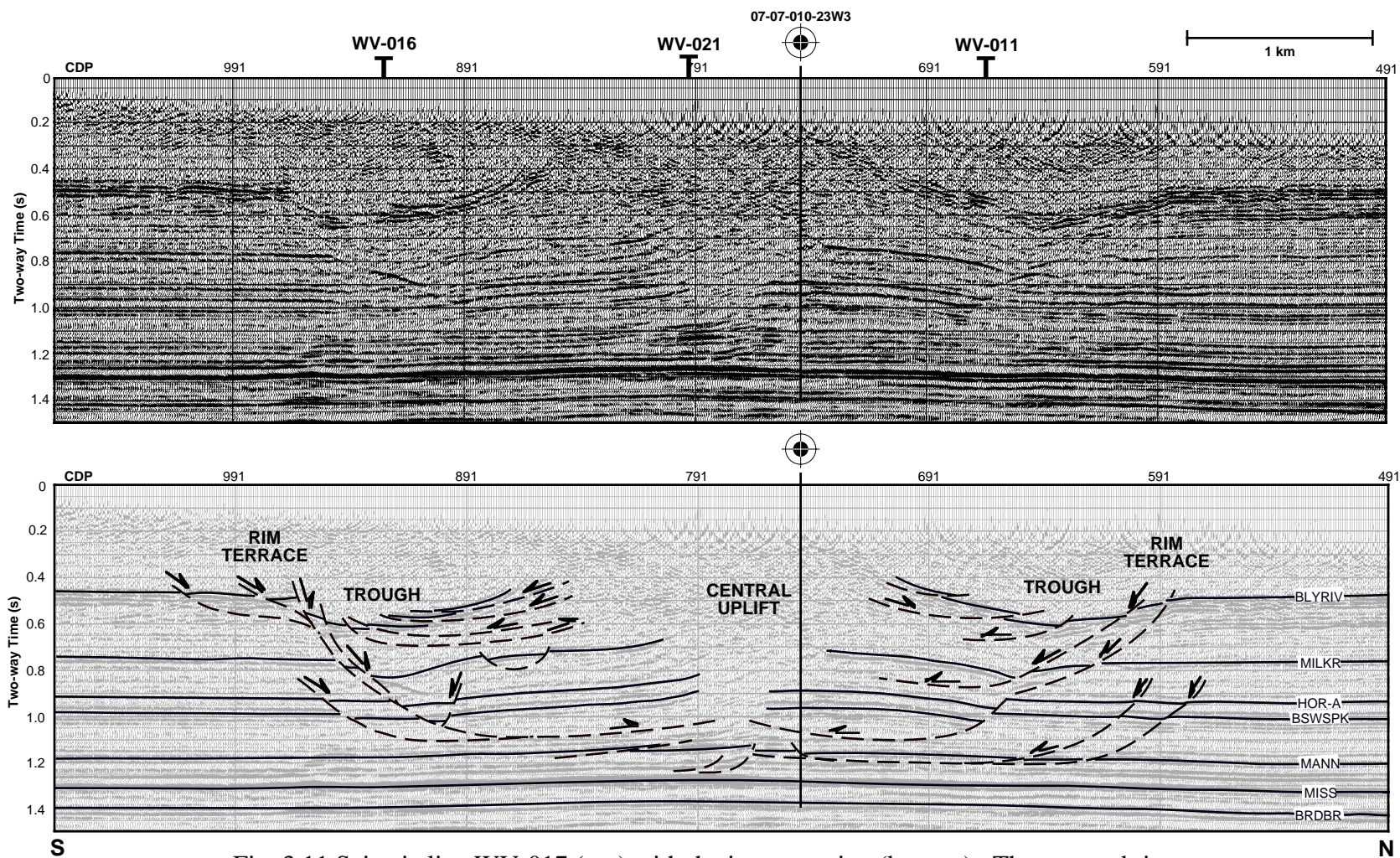


Fig. 3.11 Seismic line WV-017 (top) with the interpretation (bottom). The terraced rim, trough and central uplift are imaged by the seismic data.

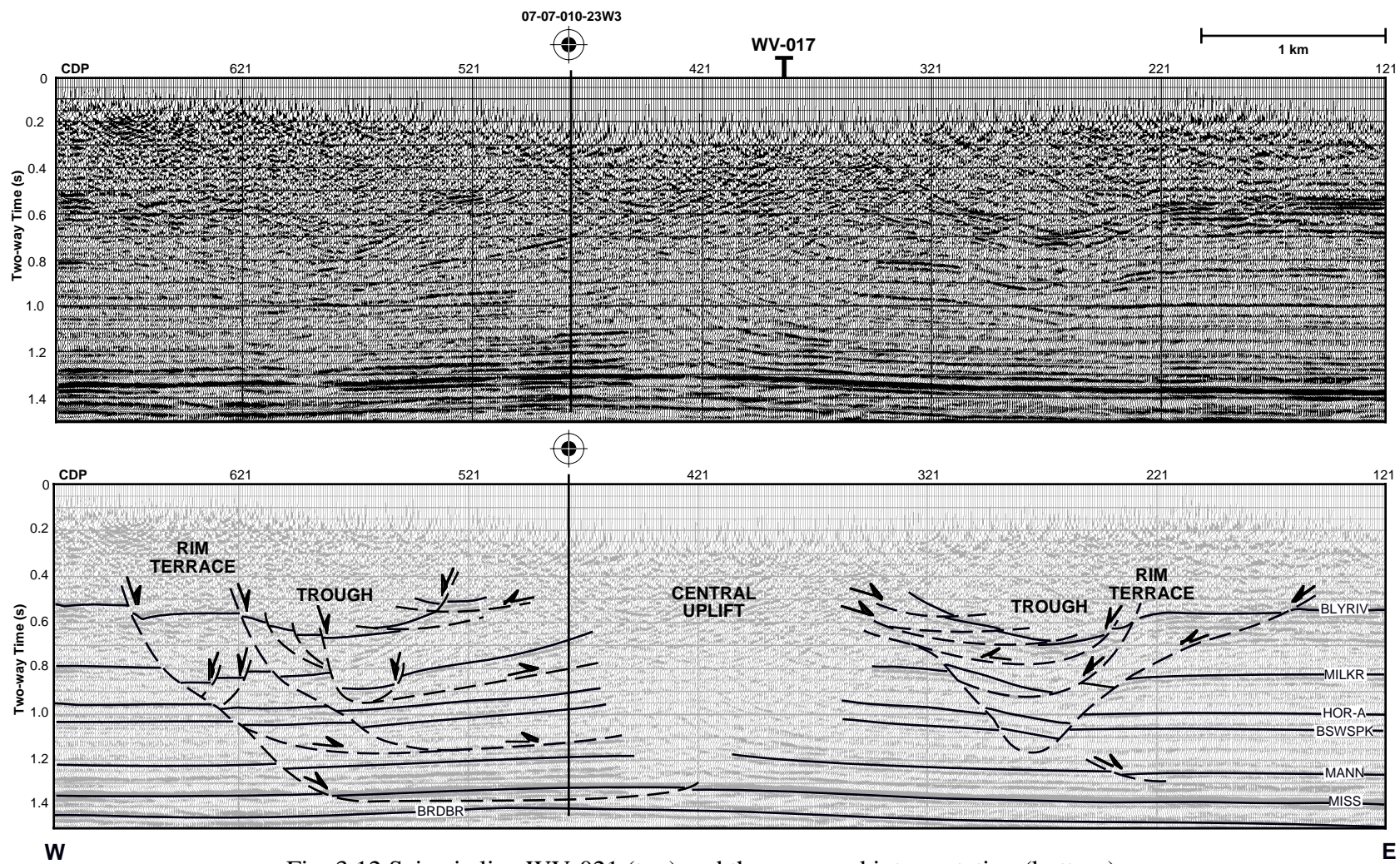


Fig. 3.12 Seismic line WV-021 (top) and the proposed interpretation (bottom).

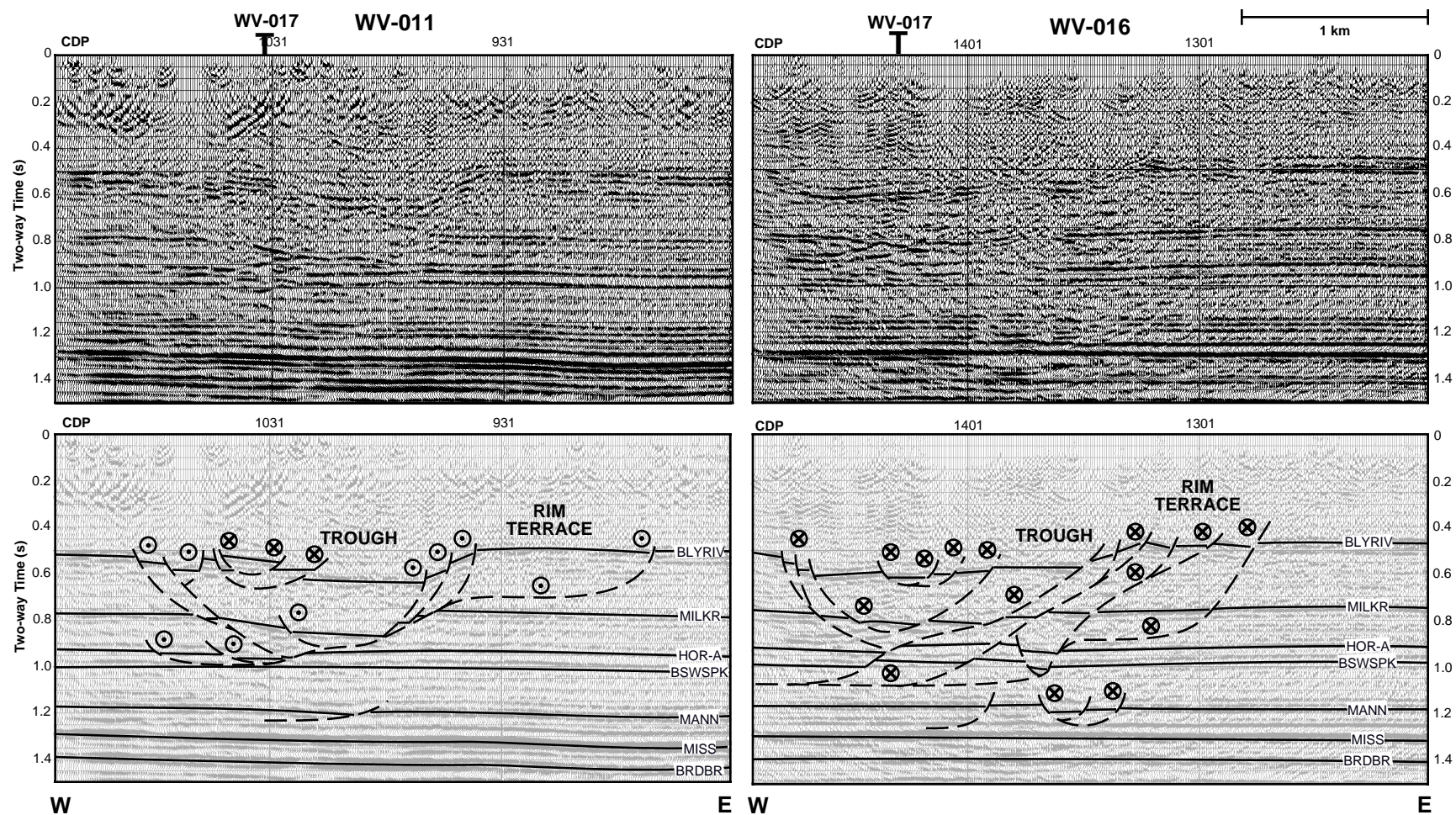


Fig. 3.13 Shown are the portions of lines WV-011 (left) and WV-016 (right) used in the interpretation. The interpretations of the seismic data (bottom) showed many graben-like structures probably indicative of out-of-plane movement.

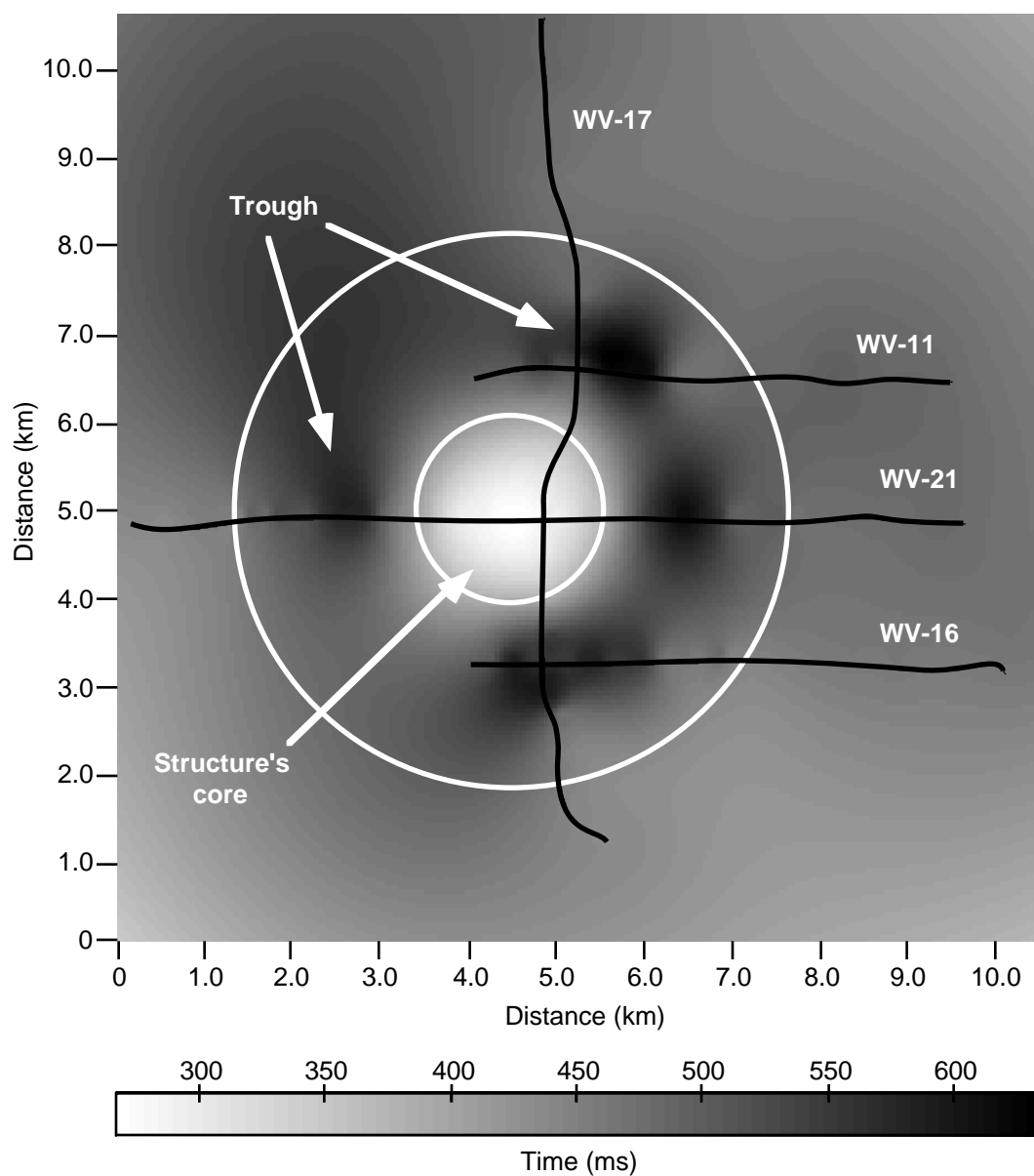


Fig. 3.14 Time structure map of the Belly River horizon (BLYRIV) as interpolated from the seismic lines. The gridding and interpolation would have benefited from a denser dataset, however, the trough still appears to surround the structure's raised core.

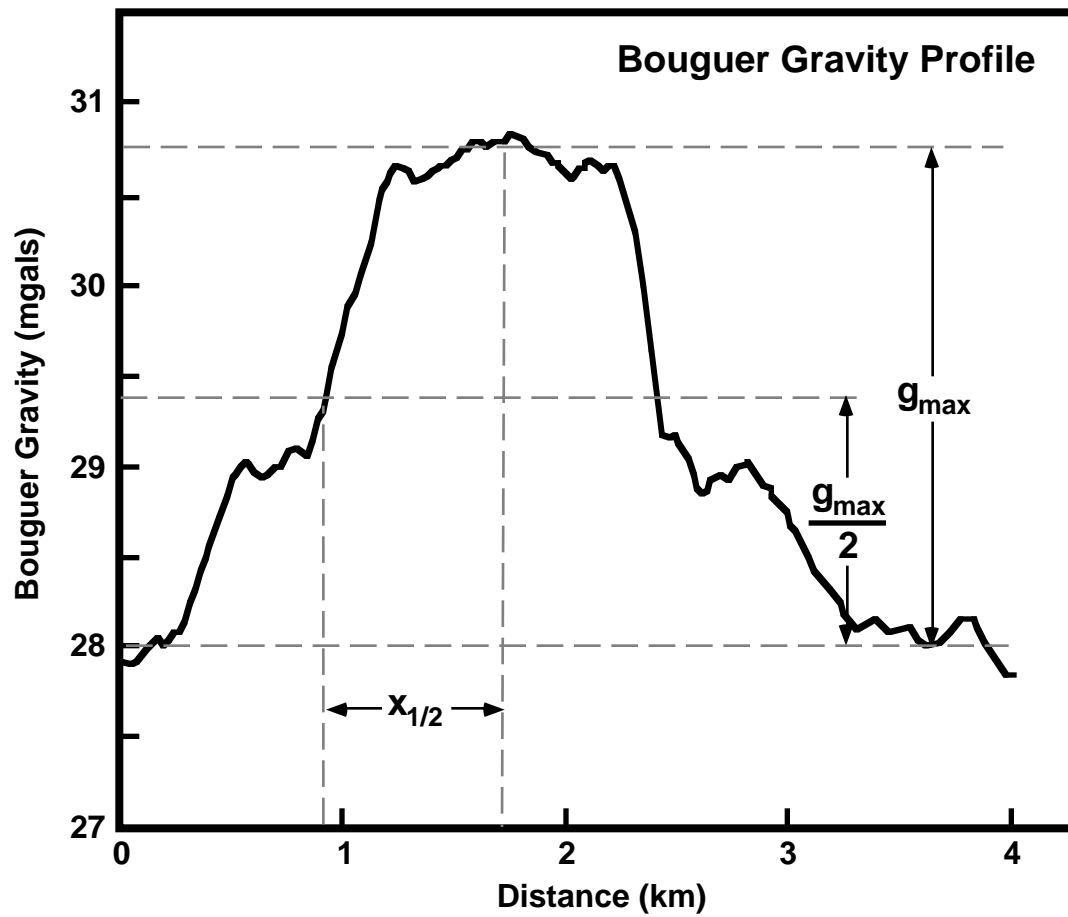


Fig. 3.15 Bouguer gravity anomaly over the White Valley structure. The profile shows a positive anomaly of about 3 mgal over the center of the structure (from Gent et al., 1992).

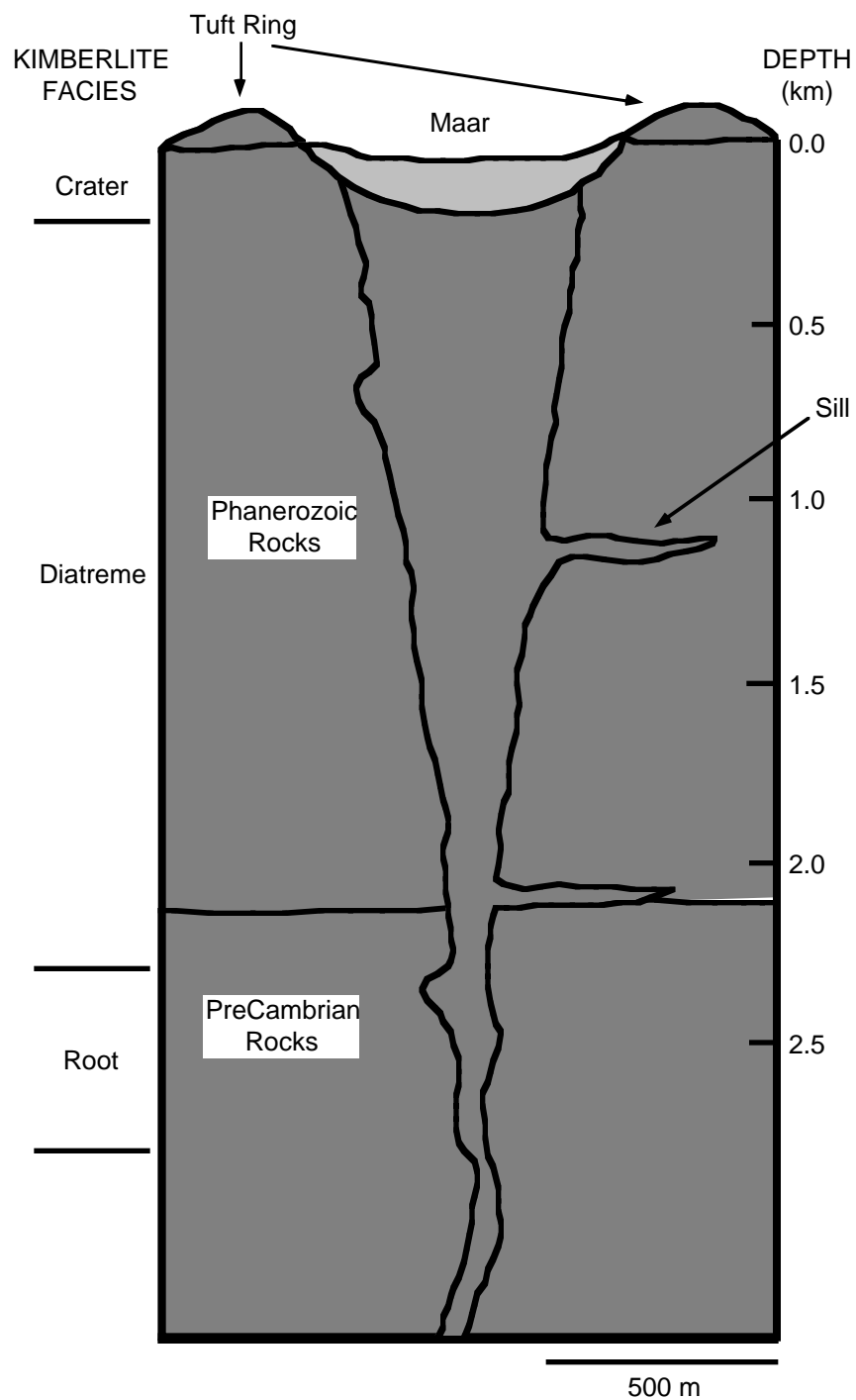


Fig. 3.16 Schematic drawing of a kimberlite pipe (from Hawthorne, 1975; Belisle, 1995).

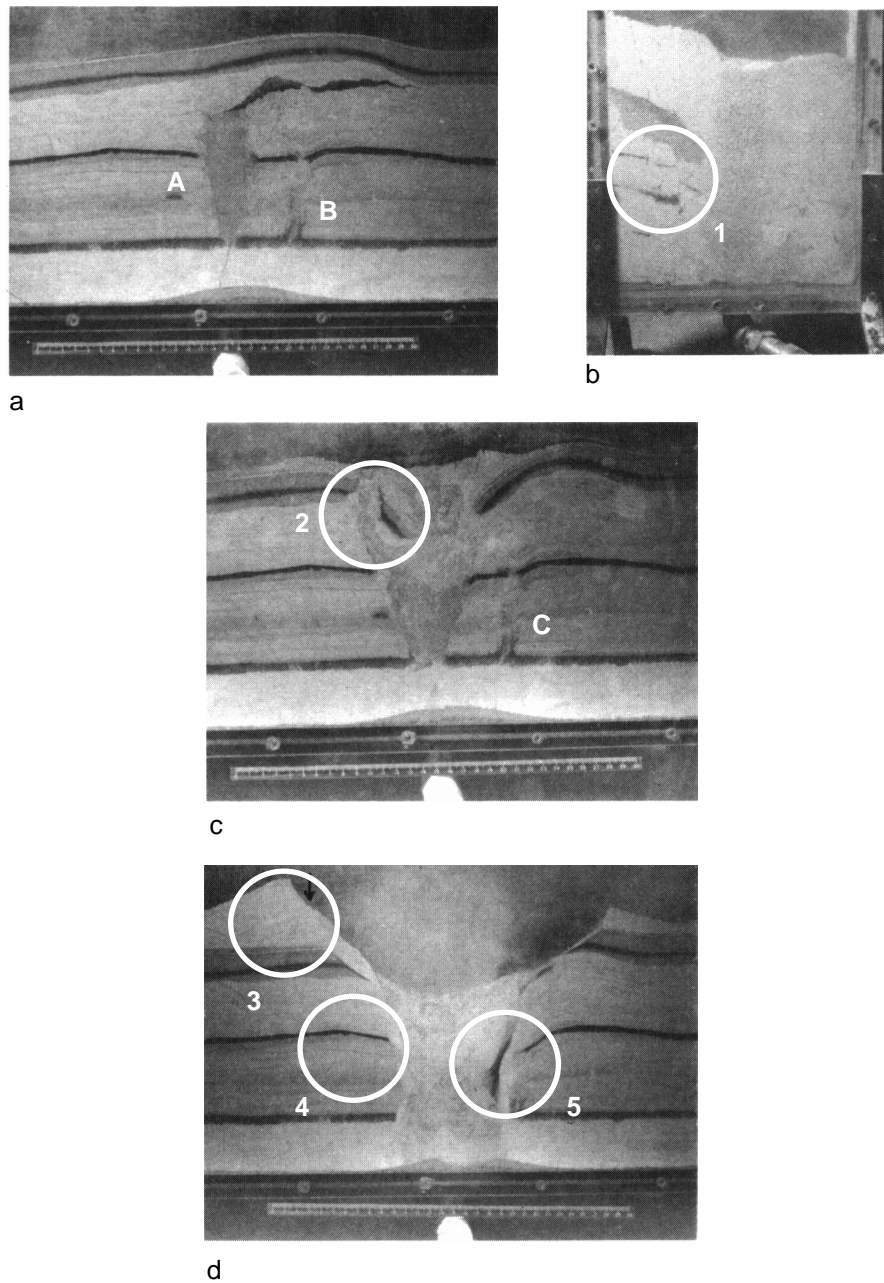


Fig. 3.17 Series of photographs from fluidization experiments used to model diatreme emplacement (from Woolsey et al., 1975). The following features can be seen: a) formation of two conduits (A and B) uplifting surface sediments; b) near-conduit normal block faulting (1); c) cohesive blocks sliding into growing primary conduit (2), secondary conduit is inactive (C); d) formation of rim (3), and downwarping of sediments adjacent to conduit (4 and 5).

CHAPTER 4 - THE PURPLE SPRINGS STRUCTURE

4.1 GEOLOGICAL SETTING

The Purple Springs structure is located at 49°52'30"N, 111°52'00"W in southcentral Alberta (Figure 4.1). The generalized stratigraphy is shown in Figure 4.2. Most Devonian and Mississippian strata dip northwest or west in the area. Slight deviations from this trend occur as the area was subjected to a series of transgressive and regressive events in lower Devonian time which subsequently became inundated and then reemerged (Meijer Drees, 1994; Oldale and Munday, 1994; Richards et al. 1994; Switzer et al. 1994). The Purple Springs area is east of the eastern margin of the main Mesozoic-Tertiary deformation front and thus is relatively undisturbed. Devonian and Mississippian strata are primarily carbonates with a few regional shale formations (e.g., Ireton, Calmar, Exshaw and Banff) and evaporites confined primarily to the Wabamun (up to 60% anhydrite), Nisku and Beaverhill Lake formations. Total evaporite thickness is probably less than 50-100 m (Halbertsma, 1994; Switzer et al., 1994). The Devonian Prairie Evaporite formation has its western depositional limit to the east of Purple Springs, although some localized occurrences have been found in southern Alberta (Gorrel and Alderman, 1968; Meijer Drees, 1994). Generally, the evaporite sequences become thicker to the north where extensive shallow, inland seas existed during this time (Oliver and Cowper, 1983; Anderson et al., 1988; Anderson, 1988; Anderson and Brown, 1991).

4.1.1 Well Control

Most wells in this area target the clastic portion of the section with fewer Mississippian penetrations at the Purple Springs location. For this interpretation, four wells were used to construct a stratigraphic cross section over the structure (Figure 4.1); these included 06-04-011-14W4, 01-36-009-13W4, 08-31-010-14W4 and 04-32-010-14W4. These wells were chosen primarily for their location as 08-31 and 04-32 were on the structure, 06-04 was adjacent to the structure, and 01-36 was distal from the structure. Three of these wells (01-36, 08-31 and 06-04) were also used because they penetrated to the Devonian strata of the Elk Point Group; the 04-32 well, situated over the structure, penetrated to the Mississippian only.

Nine horizons were chosen for correlation purposes including the Second White Speckled Shale (SWSPK), Bow Island (BOWISL), Mannville (MANN), an A-horizon (HOR-A), the Rierdon formation (RIERDN), the Sawtooth formation (SAWTH), the Mississippian (MISS), the Wabamun formation (WAB), and the Elk Point Group (ELKPT). I found that these horizons correlated reasonably well to continuous seismic reflectors as well as provided good delineation of the structure. Figures 4.3 shows the cross section through the four wells depicting the velocity logs, plotted in depth, and their corresponding horizon picks. The 06-04 and 01-36 well logs represent more regional trends while the 08-31 and 04-32 wells are located directly over the structure. The cross section indicates several interesting features.

The MISS is situated 180 m deeper within the structure than regional with both shallower and deeper formations demonstrating a similar trend albeit smaller in amplitude (compare 06-04 with 08-31 in Figure 4.3). The WAB is 30 m lower than regional and the ELKPT is 26 m lower. Moving shallower in the section, the SAWTH and RIERDN show some 130

m and 75 m of lowering, respectively, while the MANN and BOWISL are both about 40 m below regional levels. The SWSPK is 20 m below regional levels. The 04-32 well, when compared with 06-04, illustrates a similar trend in the horizons on-structure and regional placement.

In both 08-31 and 04-32, the MISS is characterized by an apparently anomalous lithology layer (gray zone in Figure 4.3). The lithology log from 08-31 indicates about 2 m of salt and anhydrite while the 04-32 logs indicate a 55 m washout of a similarly low density material ($\approx 2.1 \text{ g/cm}^3$) at the SAWTH-MISS contact. The velocity of this material is about 5000 m/s which is somewhat high for salt - more typically around 4600 m/s - and thus may indicate another rock type. Nonetheless, the result is a strong impedance contrast which manifests itself as an amplitude anomaly on the seismic data and is probably why the 04-32 well was drilled.

It is apparent that the WAB horizon deepens by some 50 m into the structure (compare 06-04 with 08-31, Figure 4.3). Further into the structure, the attitude of the WAB horizon becomes unclear although it is possible that it shallows by perhaps 65 m at 04-32. This is indicated by the lower dashed line in Figure 4.3.

Further, the cross section indicates thickening of early Mesozoic sediments within the structure, particularly at the SAWTH and RIERDN (which thicken on the order of 50-55 m) and, to a lesser extent, at the MANN horizons. The 01-36 well indicates an overall apparent dip to the northwest of less than a degree, consistent with regional trends.

4.2 GEOPHYSICAL CHARACTERISTICS

Seismic lines DBRR-1, DBRR-2 and DBRR-3, acquired during the course of oil and gas

exploration, all pass completely over the structure and gave initial evidence that the feature was somewhat circular and fairly extensive in area and in depth. These data were donated by Norcen Resources Ltd. and Amoco Canada Ltd. for this work. Tables 4.1 and 4.2 summarize the acquisition and processing parameters to migrated stack. The four wells discussed in Section 4.1.1 were used for correlation purposes.

4.2.1 Well Log to Seismic Data Correlations

Sonic logs were available for all four wells while only a few had density logs available. So

ACQUISITION PARAMETERS	
Source	<ul style="list-style-type: none"> • Dynamite, single hole • 0.5 kg at 18 m • Interval: 68 m
Receiver	<ul style="list-style-type: none"> • Interval: 17 m • Geometry: 9 inline per group (at 4 m)
Shot-Receiver Geometry	<ul style="list-style-type: none"> • 2D split spread • offset range of 17m to 810 m • 2 W-E lines, 1 N-S line
Sample Rate	<ul style="list-style-type: none"> • 2 ms

Table 4.1 Survey acquisition parameters.

sonic logs alone were used to make zero-offset synthetic seismograms with which to correlate the seismic data. In all cases, a 35 Hz, zero-phase, Ricker wavelet was used to produce the synthetic seismograms. Figures 4.4, 4.5, 4.6 and 4.7 show the velocity logs of 01-36, 06-04, 08-31 and 04-32, respectively, their corresponding synthetic seismograms, and their correlations to the seismic lines.

The 01-36 log, corresponding to the regional velocity trend, was correlated to seismic lines DBRR-1 and DBRR-2 over a distance of nearly 20 km, but the horizontal regional stratigraphy allowed for confident correlations. The 06-04 velocity log was correlated to

PROCESSING FLOW	
Demultiplex	• with trace editing
Amplitude Recovery	
Deconvolution	• min phase spiking • 100 ms operator length
Statics	• elevation, refraction • datum = 762 m
Velocity Analysis	
Normal Moveout Correction	
Residual Statics	• 450-1300 ms window
Mute	
Trim Statics	• 390-1300 ms window
Stack	
Filter	• bandpass: 13/48-70/96 Hz/dB
Migration	• finite difference

Table 4.2 Basic processing flow.

DBRR-3 over a distance of about 400 m. The 08-31 log was projected to all three lines, about 330 m to DBRR-1 and nearly 2 km to both DBRR-2 and DBRR-3. Lastly, the 04-32 velocity log and synthetic were correlated to all three lines over distances of 830 m to DBRR-1, 500 m to DBRR-2, and 660 m to DBRR-3. In all cases, good correlations were found between the synthetic seismograms and the seismic data (see Figures 4.4, 4.5, 4.6 and 4.7).

4.2.2 Seismic Data Interpretation

The three lines tied together very well with respect to all the horizons giving added confidence in the horizon picks and the well ties (Figure 4.8). Figures 4.9, 4.10 and 4.11 show the uninterpreted seismic data from lines DBRR-1, DBRR-2 and DBRR-3, respectively, with the location of the well ties and line ties annotated on each. Similarly, Figures 4.12, 4.13 and 4.14 show the interpreted versions.

All three seismic lines passed completely over the structure and helped to delineate its areal extent. In plan view, it appears slightly elliptical in shape (Figure 4.1) with a maximum

diameter of some 4 km. In section, the seismic data show the structure to dominate the carbonates of the Mississippian and Devonian with less structure occurring in the clastic portion of the section. In addition to the nine horizons discussed in Section 4.1.1, a tenth horizon was used to help delineate the structure and was simply labeled HOR-B. It lies between the WAB and ELKPT horizons. The seismic lines were received in their final migrated form and were not reprocessed. However, there are indications that the data are of questionable quality. The near-surface reflectors shallower than the SWSPK (the shallowest horizon correlated) abruptly show poor continuity compared to the reflectors deeper than the SWSPK. On the other hand, the reflectors within the time zone containing the structure appear quite coherent and there is little evidence of migration operator artifacts. The seismic data were therefore deemed of sufficient quality to proceed directly with the interpretation.

4.2.2.1 Horizon Description

Beginning with the shallow part of the section, the SWSPK is the first reflector correlated to the seismic data. It shows little structure except for normal faulting in the extreme western portion of lines DBRR-1 and DBRR-2 (Figures 4.12 and 4.13) as well as the extreme northern and southern portions of DBRR-3. The deeper BOWISL and MANN horizons continue this trend but also exhibit graben-type faulting on DBRR-3 (see CDP 651, 0.55 s, Figure 4.14) and an east-dipping normal fault on the eastern portion of lines DBRR-1 and DBRR-2.

All the deeper horizons, except for the ELKPT, show structural deformation near the rim of the structure in the form of normal faulting. These faults dip into the center of the structure and are interpreted as being listric. They delineate terraces along the rim which step down into the structure. Near the rim of the structure, both the SAWTH and RIERDN become

difficult to interpret and are denoted by dashed lines (Figures 4.12, 4.13 and 4.14). HOR-A is a regional marker which appears in the structure and is shallower than the SAWTH and RIERDN horizons. As it was possible to interpret this horizon with more confidence over the rim of the structure, it was used to guide the RIERDN and SAWTH horizons from their location in the structure to their positions regionally. Within the structure, the MISS horizon is also delineated by a dashed line. This is to stress the anomalous lithology that the well logs from 08-31 and 04-32 indicated. It is unclear what the true lateral extent of this lithology might be but there is possible evidence for it in both 08-31 and 04-32 and, in both cases, it appears to correlate to a relatively flat, coherent reflector on the seismic data. It was therefore interpreted to be equivalent to the top of the MISS horizon. Beneath the MISS, the WAB horizon also steps down into the structure. However, reflections within the core of the structure become completely incoherent. In fact the HOR-B horizon is only visible outside the structure. As it reaches the structure's side, it breaks up and is therefore only helpful in delineating the lateral extent of the structure at this depth (e.g. CDP 760, 0.9 s, Figure 4.12).

The ELKPT horizon was the deepest correlated reflector. Although it appears to be largely unaffected by faulting, line DBRR-3 does show some minor offsets in the ELKPT towards the southern end of the structure (CDP 601-551, 1.0 s, Figure 4.14). It is unclear whether or not this is a primary structure associated with the main deformation of shallower horizons or whether this is indicative of basement control. Recall also that the cross section (Figure 4.3) indicated the ELKPT was 26 m deeper than regional levels. This displacement is not readily apparent on the seismic data as a distinct reflector break and may be due to the lack of vertical resolution at this depth. The dominant frequency of the seismic data at this level is only about 20 Hz. The compressional wave velocity of the Devonian carbonates is about 5750 m/s (based on 06-04 velocity log, Figure 4.5) and thus the corresponding

vertical resolution is only some 70 m based on 1/4 of the dominant wavelength (Yilmaz, 1987). Thus any fault at this depth would have to exhibit a vertical displacement of at least 70 m before the foot wall and hanging wall could be imaged as separate reflections on the seismic data. However, displacements at or below this resolution threshold value may still manifest themselves as amplitude anomalies but this effect is also not evident at the ELKPT horizon. Of course, there is also no indication that the 26 m of structure has to occur in a single displacement or that it is laterally extensive enough to even be imaged on the seismic lines to which the wells are projected. It could easily occur as a series of smaller faults between 06-04 and 08-31.

4.2.2.2 Time Structure

Many of the horizons identified above show time structure. For the most part, the time structure shows a similar trend as that indicated by the cross section through the four control wells (Figure 4.3, Section 4.1.1). The MISS demonstrates the greatest time structure into the feature at some 110 ms of two-way travel time below regional levels. Horizons both shallower and deeper than the MISS show less time structure. Greater time structure may exist in the core of the feature but due to a lack of well control in this region and poor reflector coherency, though, it remains uninterpretable beneath the MISS (e.g., CDP 401-551, 0.85-0.95s, Figure 4.14).

Generally, the time structure is exaggerated by velocity affects as well, particularly beneath the feature. With thickening of the clastic horizons into the depression, higher velocity carbonates are essentially replaced by lower velocity clastics. Thus a velocity push-down is likely to contribute to the total time structure that is seen on the seismic data. For example, the ELKPT horizon shows a total time structure of some 45 ms of two-way travel time below regional levels. From the well control, it is known that some of this time

structure is due to an actual 26 m of ELKPT structure. This corresponds to about 9 ms of two way travel time (based on the carbonate rock's average P-wave velocity of 6000 m/s from the 08-31 well log). Thus the remaining 36 ms of time structure should be due to velocity push down. Most of this push-down is likely due to the clastic infill of the structure. As indicated earlier, this infill has a thickness of about 180 m and a P-wave velocity of about 3750 m/s. Juxtaposed against the Mississippian carbonates it replaces, which show an average P-wave velocity of 5750 m/s (from the 06-04 well log), the corresponding time effect is about 33 ms of push-down, in close agreement with the 36 ms estimated from the ELKPT horizon time structure.

4.2.2.3 General Morphology

The structure is approximately bowl-shaped with an elliptical expression in plan view. It appears grossly bilaterally symmetric in the seismic sections although there tends to be a greater density of normal faulting in the western portion of lines DBRR-1 and DBRR-2 and in the southern portion of line DBRR-3 (Figures 4.12, 4.13 and 4.14). These listric rim faults delineate terraces which step down into the structure towards its core, which is comprised primarily of chaotic reflections. The structure appears to disrupt primarily the Devonian and Mississippian carbonates down to the ELKPT horizon but it is possible that deeper structural deformation exists. Within the structure there is clastic infill above the apparently downdropped MISS horizon. The structure affects strata shallower than the MISS, manifested largely as thickening of clastic sediments, which dominates horizons shallower than HOR-A, as well as a combination of thickening and normal faulting in clastic horizons from HOR-A to the SAWTH. The ELKPT horizon shows time structure in addition to actual downdrop, believed to be a velocity push-down effect.

It is possible to estimate the geometric dimensions of the structure quantitatively by combining all the data described previously as well as the appropriate velocity information, and the horizontal trace scale. In plan view, the structure appears slightly elliptical with a major axis diameter of nearly 4 km and a minor axis diameter of nearly 3 km at the MISS horizon (Figure 4.1). The structure's total depth of disruption is estimated to include the MISS to ELKPT horizons - a thickness of some 750 m regionally. The structure of the MISS horizon from regional to its deeper location in the feature is estimated at 180 m. Thus, the maximum thickness of the clastic infill is also 180 m. The thickness of the remaining portion of the structure, primarily characterized by a lack of reflector coherency, is about 596 m (this includes the 26 m displacement of the ELKPT). The seismic data indicate about 200 ms of two-way time thickness for the structure's core (MISS to ELKPT) with an approximate carbonate rock P-wave velocity of about 6000 m/s (from 08-31). This corresponds to a thickness of 600 m, in good agreement with the well data.

Infilling of the structure over time has resulted in thickening of the clastic sediments within and above the structure. 160 m of additional Mesozoic sediment is present above the MISS within the structure compared to regional levels. This results in 20 m of structure still present at the SWSPK level. The thickening decreases with decreasing depth, amounting to about 50 m for the SAWTH-MISS interval, 55 m for the RIERDN-SAWTH interval, 35 m for the MANN-RIERDN interval, no apparent thickening of the BOWISL-MANN interval and about 20 m for the SWSPK-BOWISL interval.

The rim faults show downward vertical displacements up to about 90 m and the terraces are some 200-250 m wide. A schematic summary of these estimated dimensions can be seen in Figure 4.15.

4.3 DISCUSSION

The initial interpretation of a meteorite impact origin hinged largely on a stratigraphic cross section made over the feature which suggested a simple crater morphology at the Mississippian level. I will look again at this hypothesis in more detail and, with the aid of the scaling criteria introduced in Chapter 2, show that the structure is not a simple crater, but appears to satisfy some of the scaling requirements for a complex impact crater reasonably well. I will also look briefly at other possible explanations for the origin of this feature.

4.3.1 Meteorite Impact Origin

The Purple Springs structure is similar to a simple meteorite impact crater. It is bowl-shaped with a chaotic core and an elliptical plan - all characteristics of such an impact structure. However, there are some key differences in morphology between this structure and typical simple impact craters. For example, simple craters are not characterized by normal faulting and terracing along the rim as is evident from the seismic data at the MISS horizon. Furthermore, simple craters have depth-to-diameter ratios of about $1/5$, whereas the Purple Springs structure demonstrates a ratio of about $1/20$ indicating it is much shallower than typical simple craters.

A rim diameter of about 1.4 km is calculated (Eq. 2-11) based on the 180 m apparent depth of the structure and this is about three times smaller than the rim diameter apparent in the seismic data. Similarly, if the chaotic portion of the structure were a breccia lens as in simple craters, then the ratio of crater depth-to-breccia lens thickness should be about 2 (Eq. 2-10). However, the Purple Springs structure has a ratio of about $1/3$. This disparity may be due to erosion of the original impact surface thus making the crater shallower relative to the breccia lens thickness. However, if the breccia lens were left largely

uneroded, then its 596 m thickness implies a simple crater depth of nearly 1.2 km (by Equation 2-10) which in turn, corresponds to an expected rim diameter of about 8 km (using Equation 2-11). This is clearly beyond the crater diameter transition zone for simple-to-complex morphologies on Earth and hence, a simple morphology is unlikely for such a large crater.

Interpretation of the geophysical data indicates listric normal faulting and terraces along the rim. These are morphological characteristics more likely associated with complex craters, and certainly the nearly 4 km rim diameter falls within the complex crater range. Craters greater than 2 km in diameter, located in sedimentary target rocks, are expected to be of the complex form due to their decreased strength relative to crystalline rocks. With a rim diameter of 4 km, the anticipated crater depth, using Equation 2-16, is about 182 m, in excellent agreement with that measured from the seismic data. However, complex crater modification also tells of the formation of a structurally uplifted central peak which generally forms abruptly after the transition diameter is surpassed. By Equation 2-18, this uplift should be on the order of some 360 m for a 4 km complex crater, with a diameter of some 760 to 1000 m (Eq. 2-19). The data at Purple Springs give no indication that such a structurally uplifted central peak is present. Furthermore, the transient crater diameter is calculated to be 3.6 km with a corresponding transient crater depth of about 1.2 km (Eq. 2-15). The full thickness of the Mississippian-Devonian interval is only 750 m, implying erosion of the Mississippian of some 450 m just to accommodate the size of the transient crater. If structural uplift, the increase in rim diameter associated with “raising” the current event horizon (the MISS), and the added evidence of Mississippian-Devonian carbonates in the center of the structure is considered, then even greater erosion of the post-impact surface is implied. These measurements and scaling results are summarized in Table 4.3. Recall also that these scaling criteria, used in the White Valley case study presented in

Dimension	Measured Result	Scaling Equations
Depth	180 m	182 m
Structural Uplift	none	360 m
Central Peak Diameter	none	760-1000 m
Transient Crater Diameter	N/A	3.27-3.86 km
Transient Crater Depth	≤ 750 m	1200 m

Table 4.3 Comparison of measured dimensions and results from the scaling equations for the White Valley structure. Values are based on a rim diameter of 4 km and complex crater scaling equations. The data do not include any estimates for possible erosion.

Chapter 3 to connect the post-impact morphology to the transient crater size, did not appear adequate. It is also possible that the impact itself was atypical thus making the scaling criteria inappropriate. For example, the elongate shape of the structure may be due to a fairly oblique impact.

Fragmentation of the projectile will also alter the crater morphology producing shallower and flatter than expected simple craters (Shultz and Gault, 1985). While the Purple Springs structure is shallower than typical simple craters, the region corresponding to the breccia lens is much too thick. Alternatively, fragmentation leads to the formation of crater fields - an elliptical area in which several impacts occur - sometimes leaving only one major depression (Passey and Melosh, 1980). However, this also does not appear to be the case at Purple Springs. Possible fragmentation also fails to explain the rim terracing at Purple Springs as far as it being a possible simple crater goes. It is not apparent whether fragmentation events significantly alter complex crater morphology since the result of fragmented projectile impacts becomes less important with increasing meteorite size (Melosh, 1989).

Another possible explanation is that the carbonate rocks into which the impact occurred, behave uniquely enough during crater formation as to be poorly represented by the scaling criteria. The strength of the carbonates may be great enough that the transition diameter is

greater than for impacts in purely clastic sedimentary rocks. The Purple Springs structure may therefore be closer to the transition diameter. It may therefore be representative of a structure at the onset of complex crater development, having properties of both morphological end members. For the moment, these ideas are speculative and require greater investigation to be substantiated.

4.3.2 Dissolution Phenomena

The extensive deposition of salts in the Western Canada Sedimentary Basin and the prominence with which many structures can be attributed to dissolution phenomena (the leaching of salt and subsequent collapse of overburden), led to the idea that dissolution may have played a role in the formation of the Purple Springs structure. However, in reviewing these types of structures, it would appear that the dissolution hypothesis alone can not account for all the characteristics of the Purple Springs feature.

Although the base of the Purple Springs structure is coincident with the base of the Devonian, where the deepest salt-bearing formations are found, the total evaporite thickness is less than 100 m and is primarily anhydrite - salt probably makes up less than 1/3 to 1/2 of this thickness (Gorrel and Alderman, 1968; Halbertsma, 1994; Switzer et al., 1994; Meijer Drees, 1994). Thus the 180 m structure on the Mississippian appears to require an anomalously thick salt sequence that has no precedent in the immediate area. Alternatively, leaching of other evaporites other than salt (such as the anhydrite) as well as leaching of carbonates would have had to accompany salt dissolution to allow for the 180 m of structure. However, it is unknown how significant dissolution of these other rock types might be. Sub-aerial exposure occurred in the Carboniferous and may have led to karsting and subsequent collapse. However, the disrupted zone at Purple Springs extends

to the Elk Point Group, indicating that any dissolution-initiated collapse likely included dissolution at that horizon.

Salt collapse features have the potential to disrupt thick sections of stratigraphy but their surface expression is usually small in area. For example, Crater Lake in southeastern Saskatchewan is only 244 m in diameter and is the surface expression of a breccia-filled collapse chimney that extends 914 m below the surface (Gendzwill and Hajnal, 1971). Similarly, the Wink Sink, a 110 m diameter collapse structure in Kansas, is the surface expression of a collapse chimney that rises some 500 m from a dissolution channel in Permian salts (Baumgardner et al., 1982). Interestingly, in the Crater Lake case, Gendzwill and Hajnal (1972) suggest that the dissolution of only 38 m of salt was followed by stoping of the cavern roof which led to a cavern height of some 114 m prior to wholesale block faulting to the surface. They also note that the initial solution cavity appears circular as opposed to linear as is typical for these features. A similar mechanism is described by Terzaghi (1970) as a possible reason for the Sandwich brinefield collapse structure near Windsor, Ontario. Thus it is conceivable that the total vertical displacement at Purple Springs may be a result of salt dissolution as well as stoping and leaching of country rock and possible compaction of the collapse breccias by an increasing overburden load during Mesozoic and Cenozoic deposition. However, the 4 km diameter span of such a structure appears unlikely as the overlying rocks making up the roof of the cavity probably could not support the overburden weight to allow for such a large solution cavity. This mechanism also fails to explain the normal faulting associated with the rim of the Purple Springs structure, although this may be a normal consequence of such large-scale collapse. The seismic data do not appear to image an elongate trough into which collapse might have taken place. It must also be presumed, therefore, that the solution cavity was essentially circular, similar to the Crater Lake example. Possible basement faulting,

indirectly indicated by structure on the Elk Point horizon may have been the conduit for the required brines. Dissolution, then, while not singularly able to explain the Purple Springs structure, still may have played a role in its formation. Perhaps a more likely scenario is that dissolution altered what was initially a meteorite impact crater. This may partially explain the lack of a prominent central peak which, due to the fractured nature of the core, may have been preferentially eroded by dissolution and surface erosion processes. Nonetheless, scaling criteria indicate some 360 m of expected structural uplift, half of which would have had to have been removed to result in the current morphometry.

4.4 CONCLUSIONS

In summary the Purple Springs structure is an enigmatic, slightly elliptical depression in Mississippian and Devonian carbonates characterized by normal faulting at the rim, which delineate terraced blocks downdropped into the center of the structure. The maximum vertical displacement of this 4 km diameter feature is about 180 m below regional levels at the MISS horizon. Infilling of this basin began at Jurassic time evidenced by thickening and draping of clastic sediments. Total thickening of the clastics amounts to 160 m, leaving 20 m of structural downdrop on the shallowest correlated reflector (SWSPK). Fracturing associated with the main structure crosscuts the deepest of these clastic horizons (SAWTH and RIERDN) with some more minor fracturing of the shallower horizons. This suggests that the formation of the Purple Springs structure occurred primarily at Mississippian time but further deformation took place through to at least the end of the Early Cretaceous.

Two hypotheses for the origin of the structure are presented. The first, based on initial industry interpretations of the structure, suggests a meteorite impact origin. The second, based on the prevalence of dissolution features in the Western Canadian Sedimentary

Basin, suggests that dissolution resulted in the feature or played a role in its genesis. The proposal that the Purple Springs structure is the result of dissolution phenomena is not satisfactory. The major problem with this mechanism is the lack of any analogous features in southern Alberta that show the same magnitude of deformation over such a large area. The dissolution hypothesis also requires a combination of an anomalously thick evaporite deposit and leaching of carbonates to accommodate the structural downdrop, although compaction of collapse breccia might account for some of this structure. None of these processes have analogs in the area for such a large structure. The meteorite impact theory is still favorable based simply on the lack of evidence for any endogenic processes in the area that could create such a large structure. However, this theory is also not perfectly aligned with the evidence currently at hand. Scaling criteria indicate the structure is not a simple crater but is more likely of the complex form. The seismic data indicate a terraced rim and the apparent depth of the structure matches that which is predicted from scaling. The lack of any obvious structural uplift, predicted to be 360 m is not easily explained, however. Possible post-impact, differential erosion and dissolution may have reduced the size of the central peak. Basement faulting can also not be ruled out as a possible contributor to the structure. It should also be noted that some impact conditions such as oblique impacts (which are expected to be the norm) are not well understood, and when one considers that not all known terrestrial impact craters are “typical”, further results from high-velocity impact research may shed new light on this hypothesis. Sharpton (1994), for example, showed evidence for unusually deep complex impact craters on Venus. Perhaps impacts in stratigraphic targets on Earth are not properly represented by the current scaling criteria either. Nonetheless, the impact theory remains one of the more likely explanations for the origin of this structure.

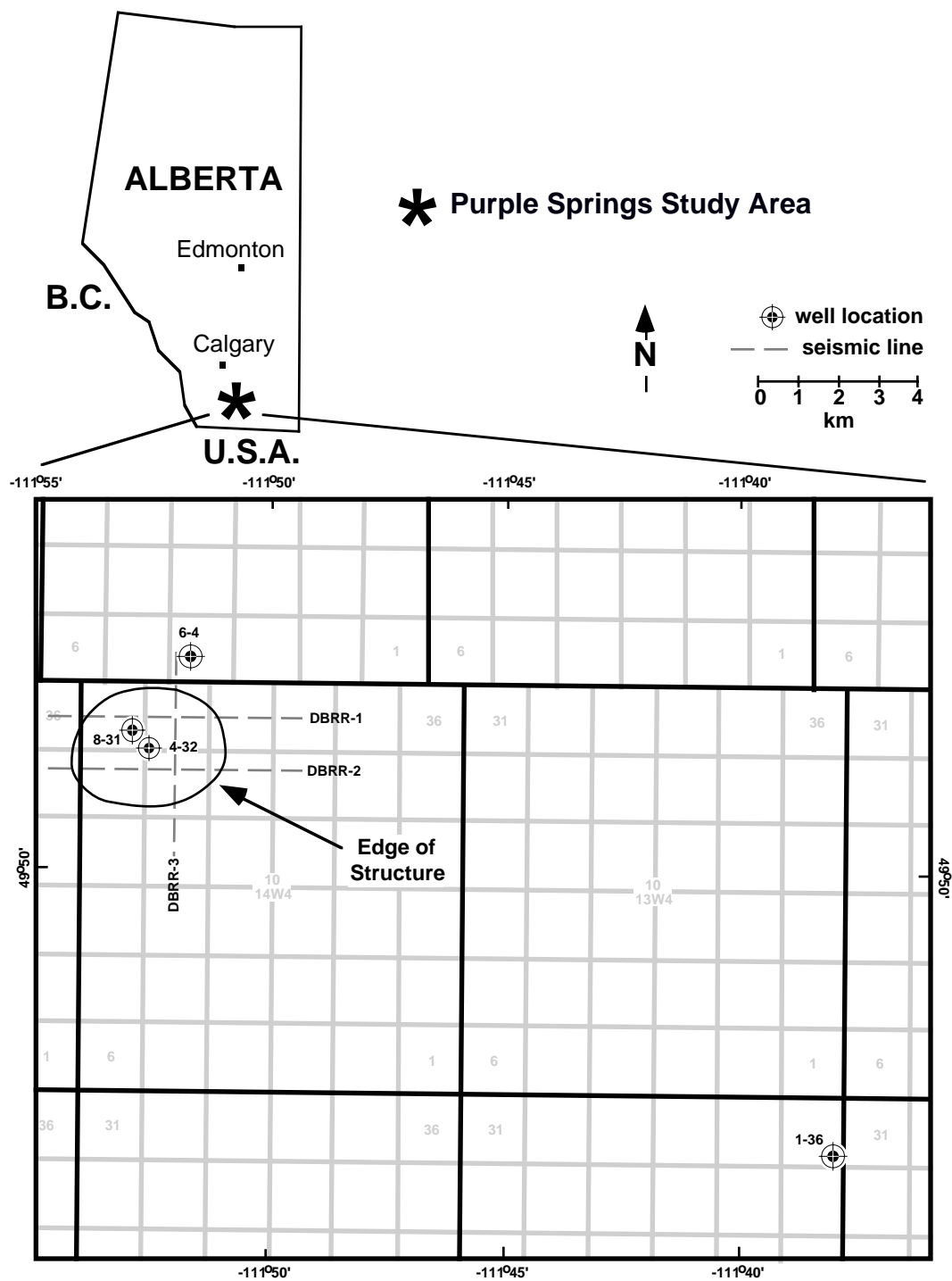


Fig. 4.1 Base map of the Purple Springs area including the seismic lines, well control points and edge of the structure, based on the Mississippian horizon.

PERIOD		FORMATION	LITH.
Tertiary		Porc. Hills / Ravenscrag	Sandstone
Cretaceous	Late	Battle/Whitemud	Sandstones and Shales
		Eastend	
		Bear Paw	
		Belly River	
		Milk River	
		Colorado GP *	Shale
Jurassic	Early	Mannville GP *	Shale/SST
	Late	Ellis GP	Shale/SST
		Swift *	
		Rierdon	
		Sawtooth *	
		Vanguard	
Mississippian			Carb/Shale
Devonian	Late	Mt. Head	Carbonate
		Turner Valley *	
		Shunda *	
		Pekisko *	
		Banff	
		Exshaw	Shale
		* Bakken	
		Wabamun *	Carbonate
		Calamar	
		Nisku *	
		Ireton	
		Leduc	
		Cooking Lake	
	Mid.	Beaverhill Lake	
		Mildred	
		Swan Hills	
		Elk Pt. GP	

Fig. 4.2 Generalized stratigraphy of the Purple Springs area. Shading indicates salt-bearing formations and asterixes (*) indicate hydrocarbon-bearing formations (from AGAT Laboratories, 1988).

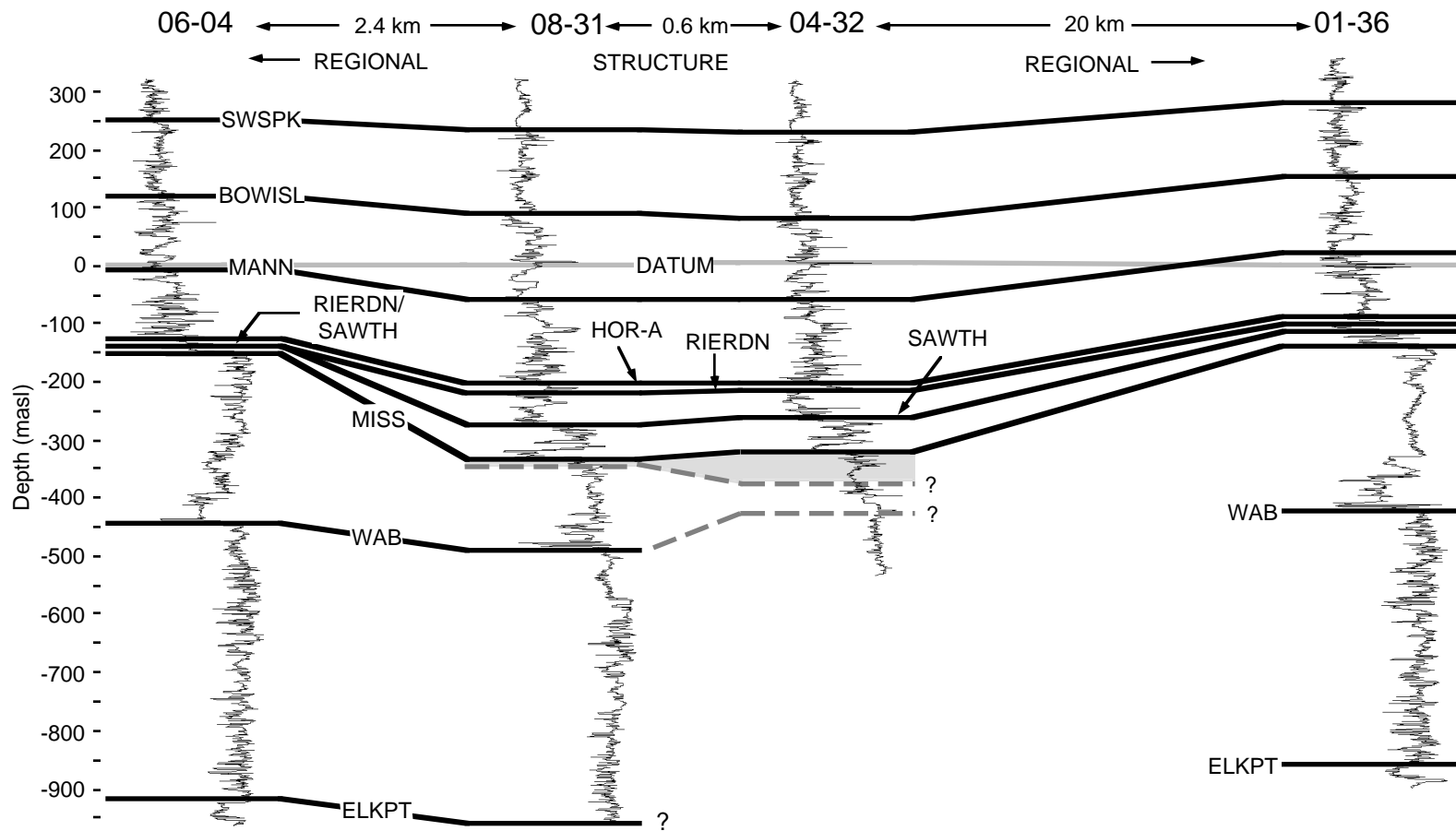


Fig. 4.3 Structural cross section using the velocity logs of the four wells. The wells are datumed on average sea level. The horizons are marked based on the log signatures and the well-to-seismic and seismic-to-seismic correlations.

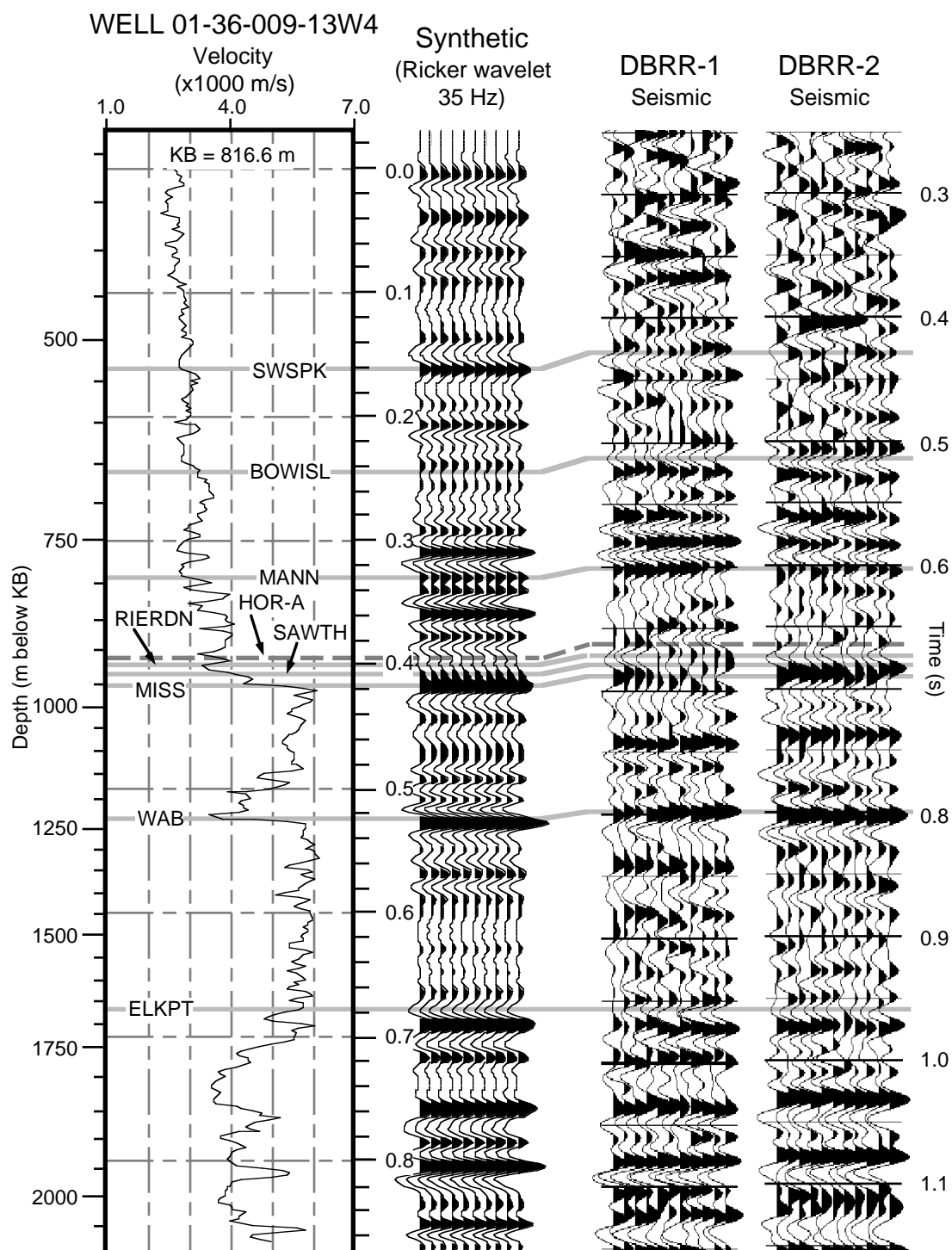


Fig. 4.4 Correlation of the sonic log and zero offset synthetic from the 01-36 well to the seismic data. The data are shown normal polarity such that a peak corresponds to an impedance increase.

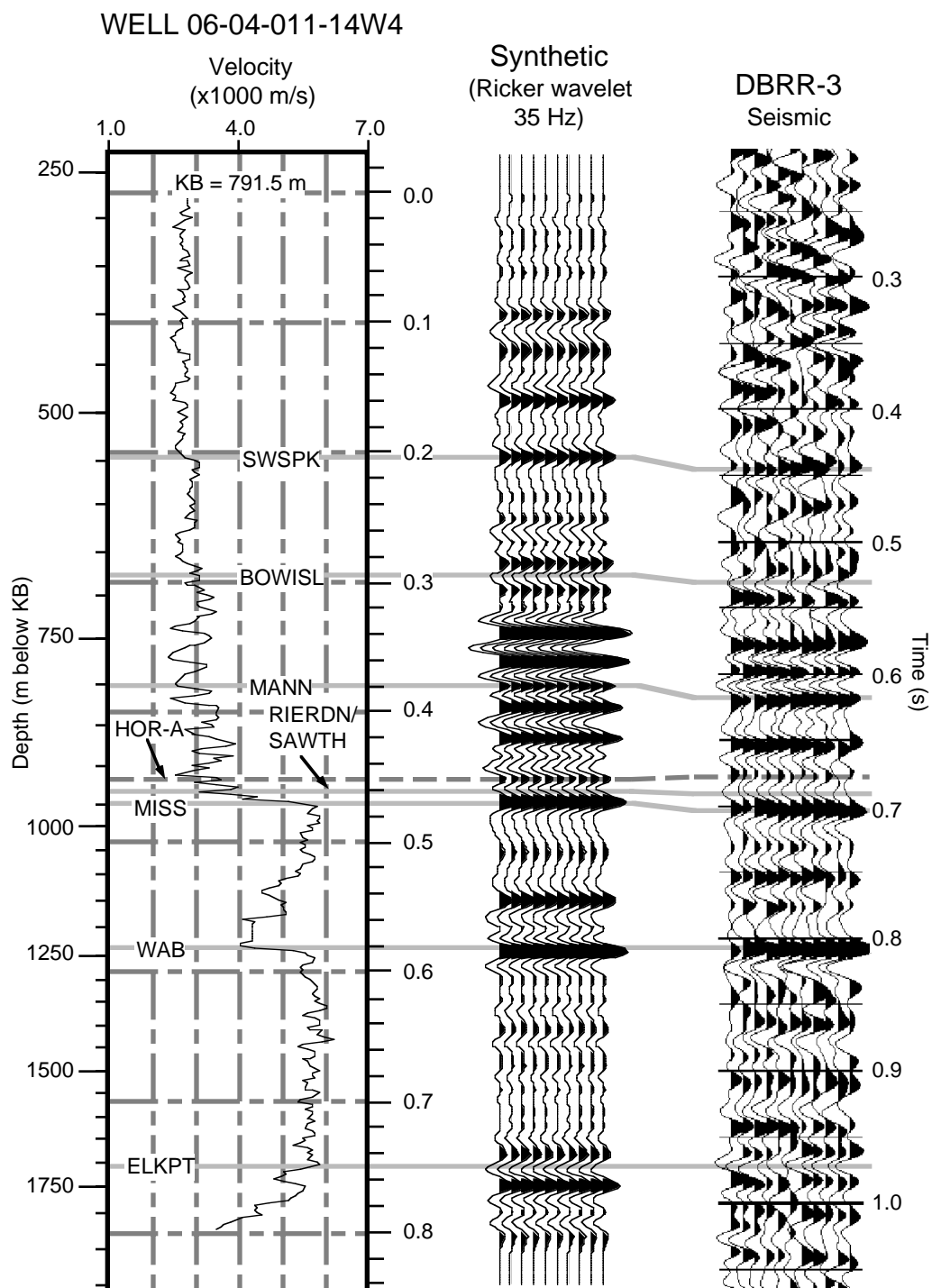


Fig 4.5 Correlation of the sonic log and zero offset synthetic from 06-04 to the seismic data from the end of line DBRR-3. The data are normal polarity.

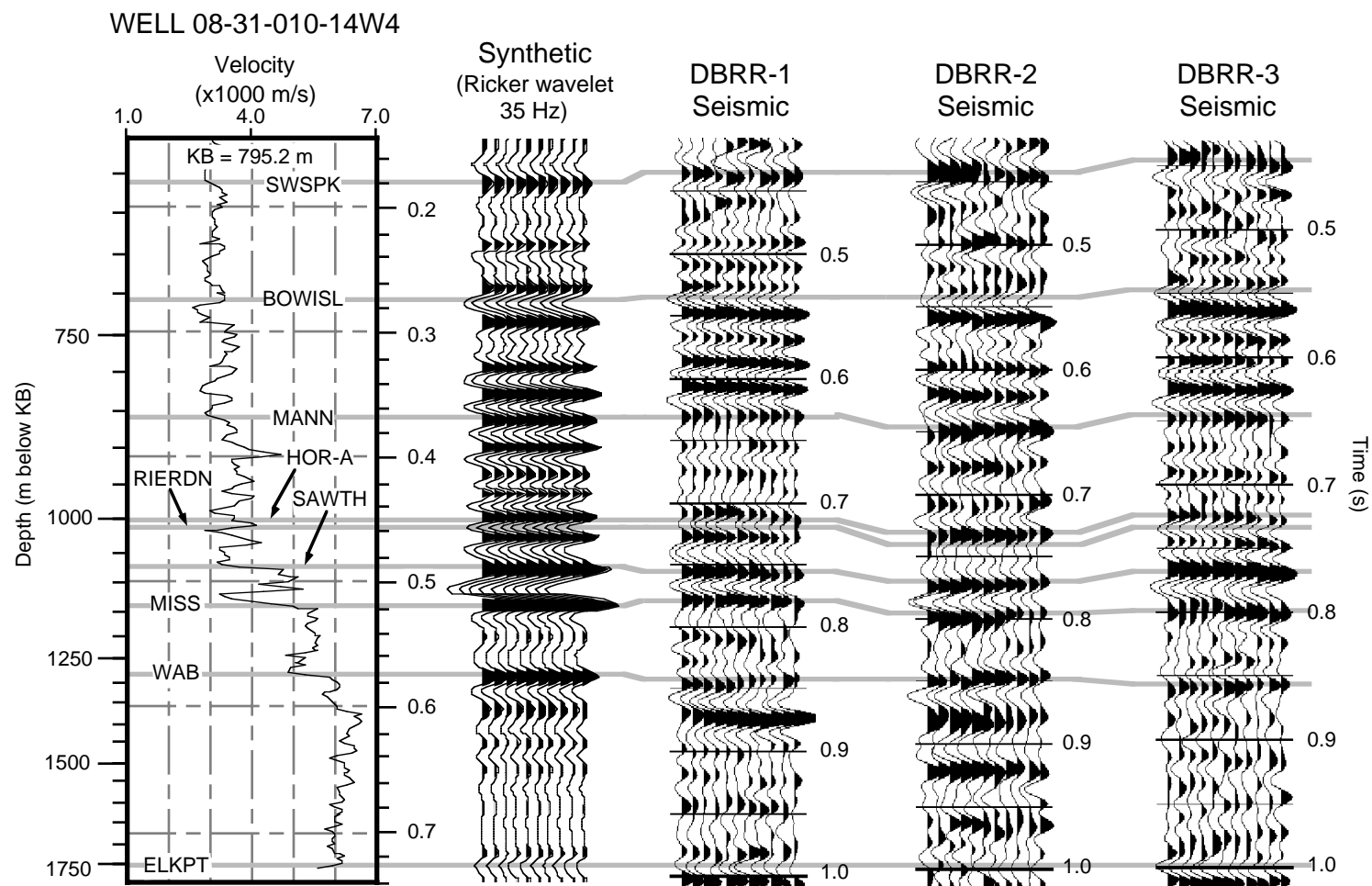


Fig. 4.6 Correlation of the sonic log and zero offset synthetic from 08-31 to all three seismic lines. The data are normal polarity.

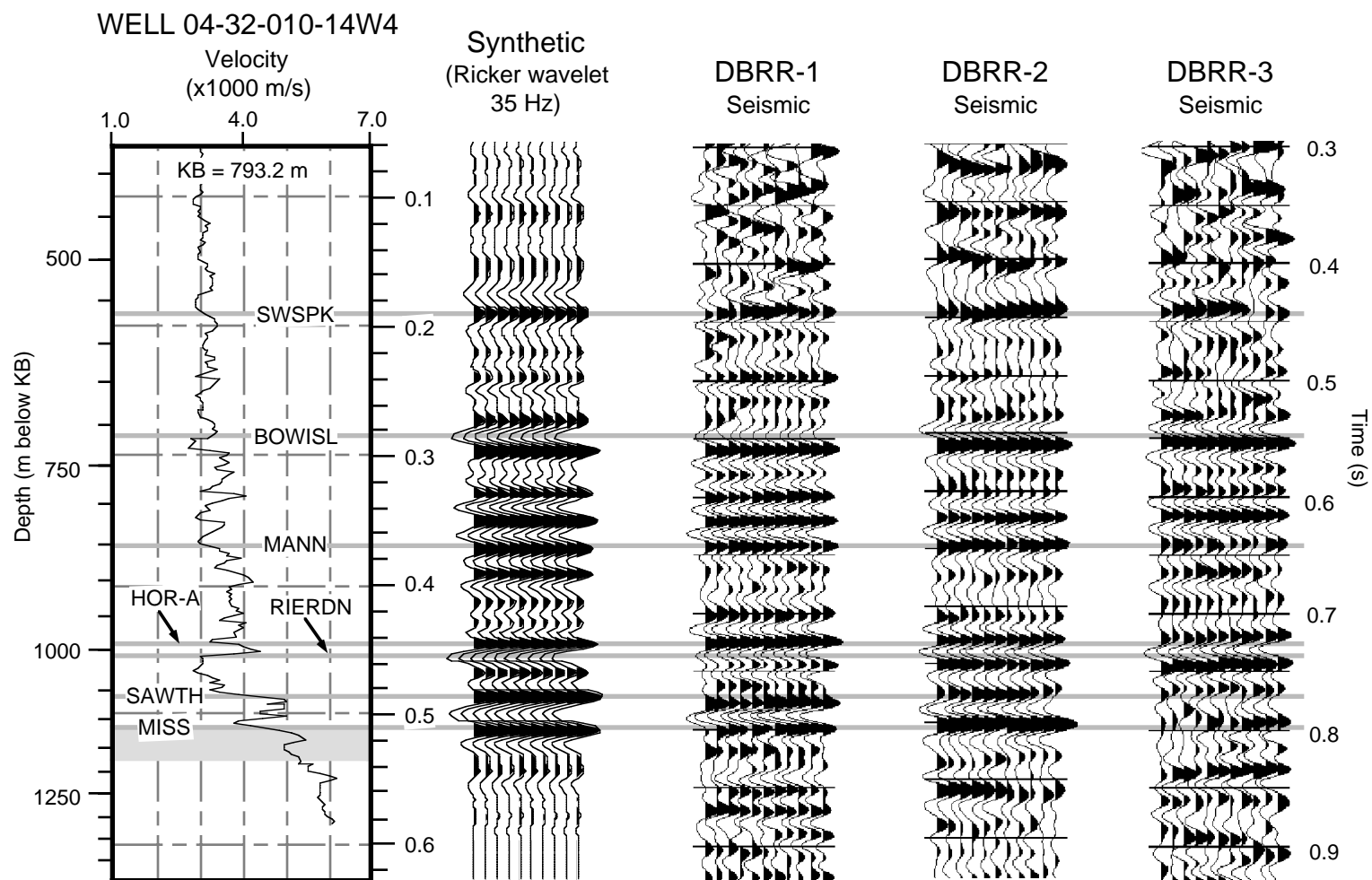


Fig. 4.7 Correlation of the sonic log and zero offset synthetic from 04-32 to all three seismic lines. The data are normal polarity. Note the salt occurrence at approximately 1100 m depth.

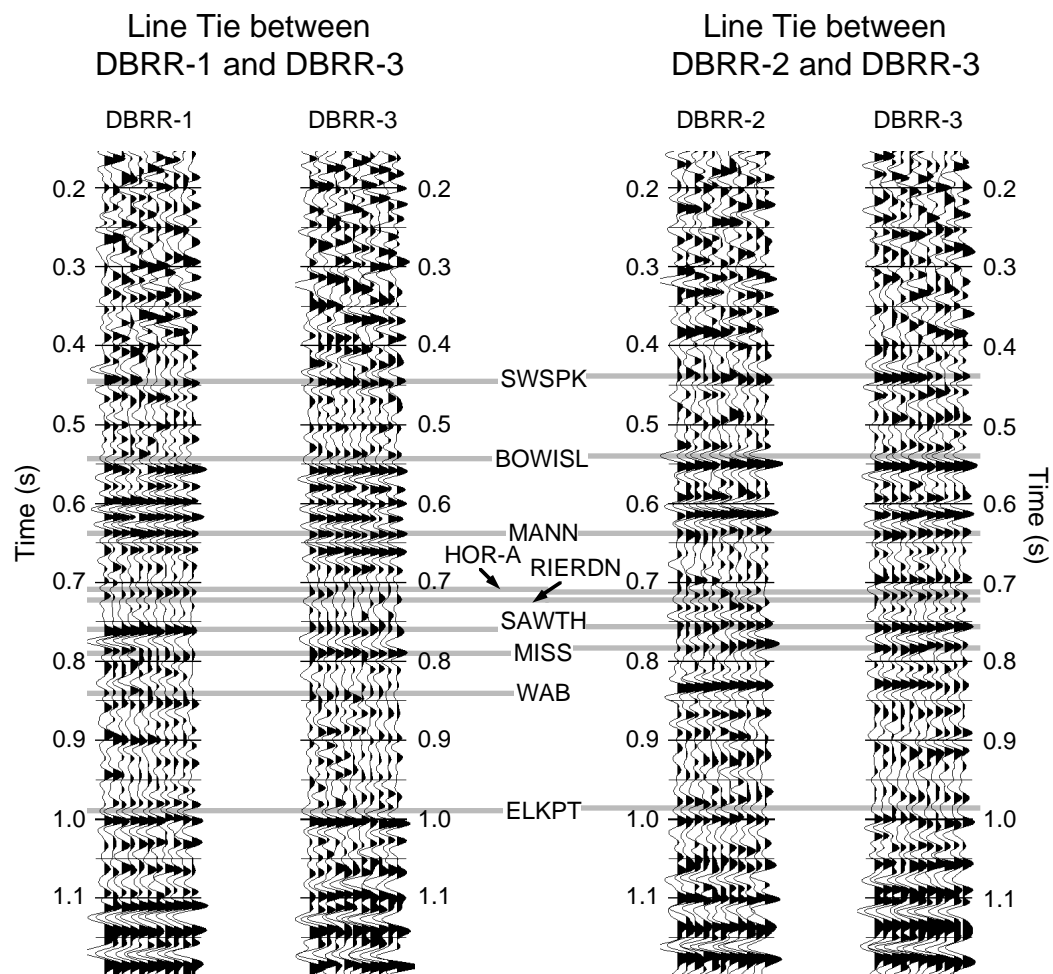


Fig. 4.8 Line ties from DBRR-3 to DBRR-1 (left) and DBRR-2 (right).

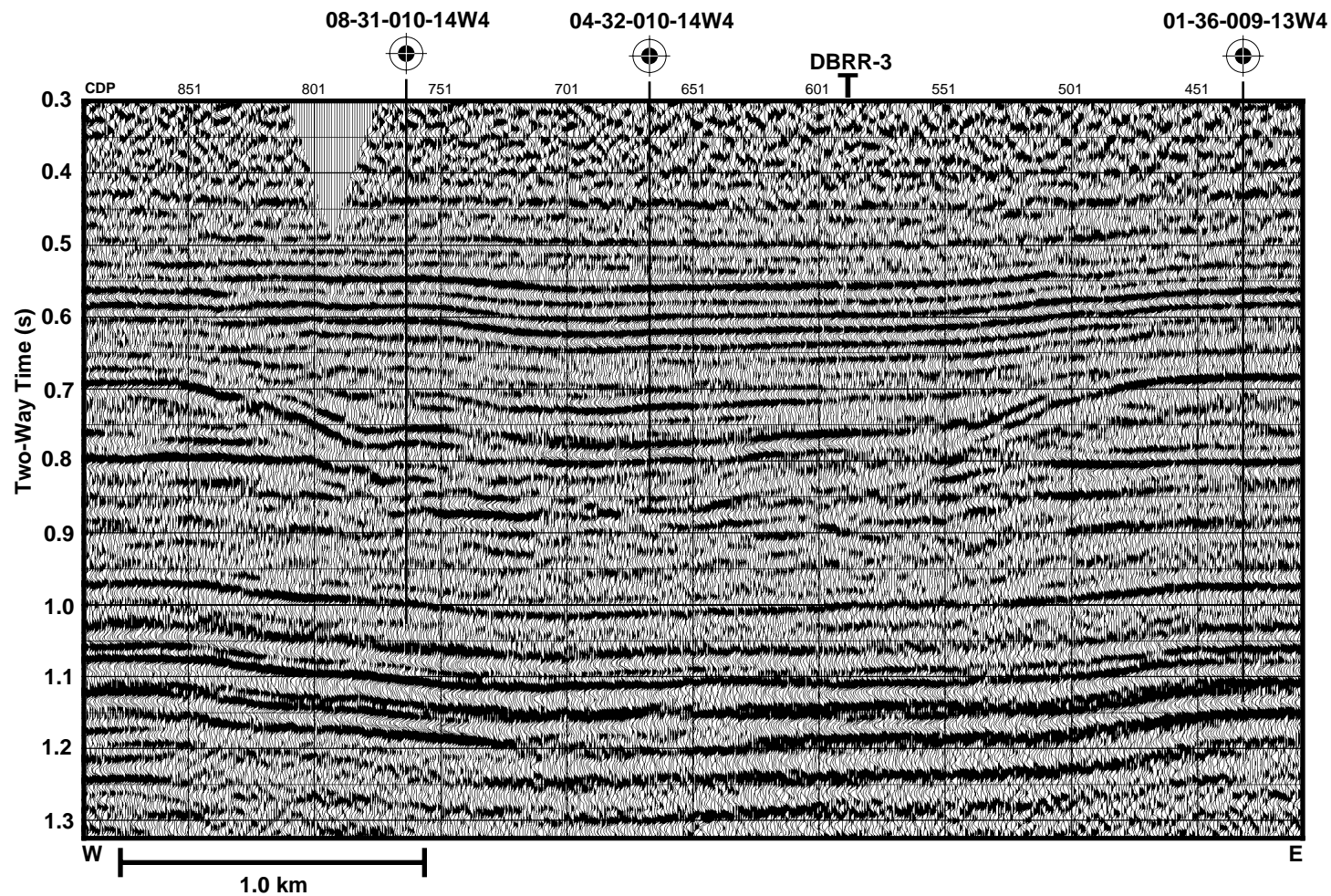


Fig. 4.9 Seismic line DBRR-1 over the Purple Springs structure. The three wells used for correlation and the tie with seismic line DBRR-3 are also labelled.

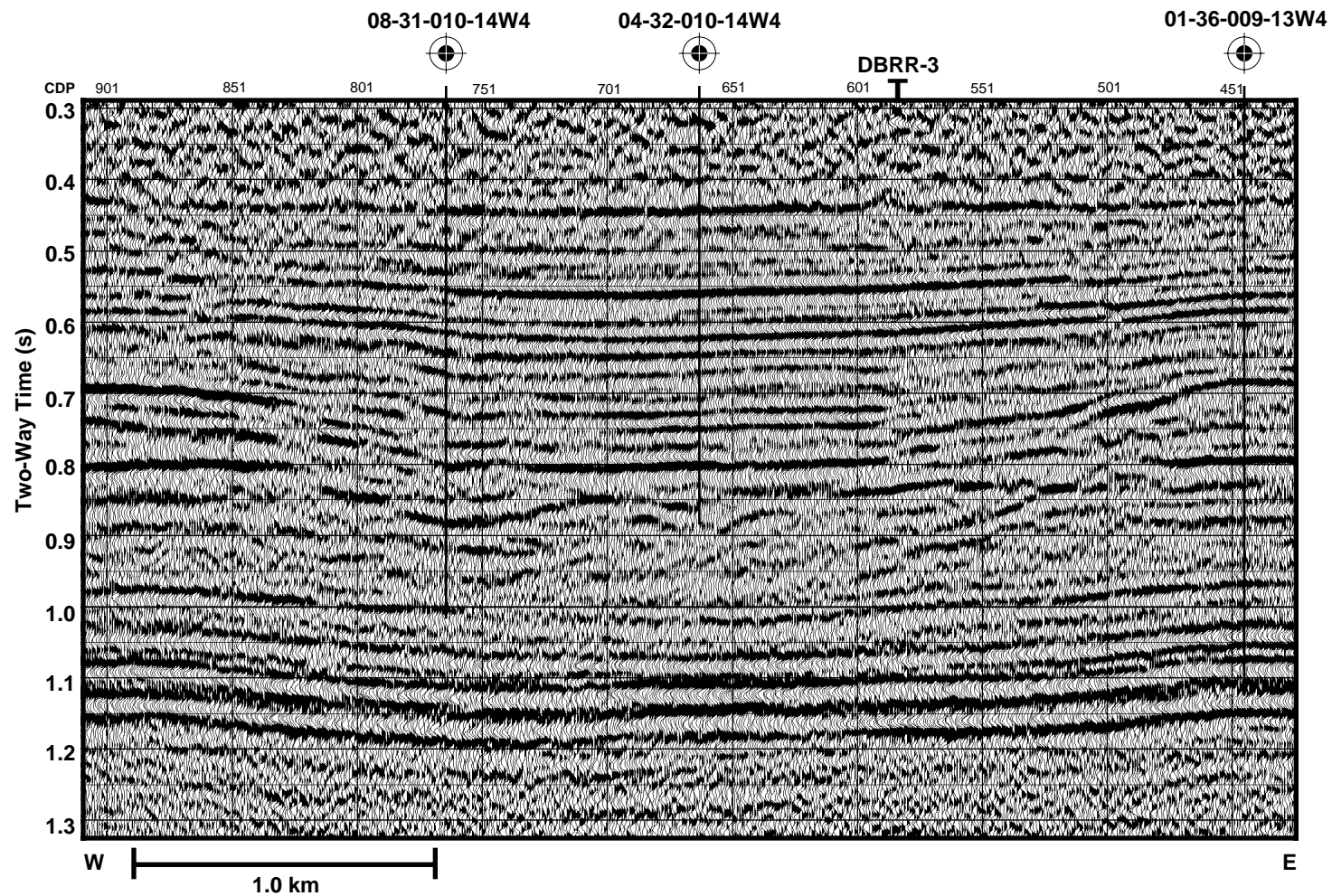


Fig. 4.10 Portion of seismic line DBRR-2 over the Purple Springs structure. Annotated above are the three wells used for correlation and the tie with line DBRR-3.

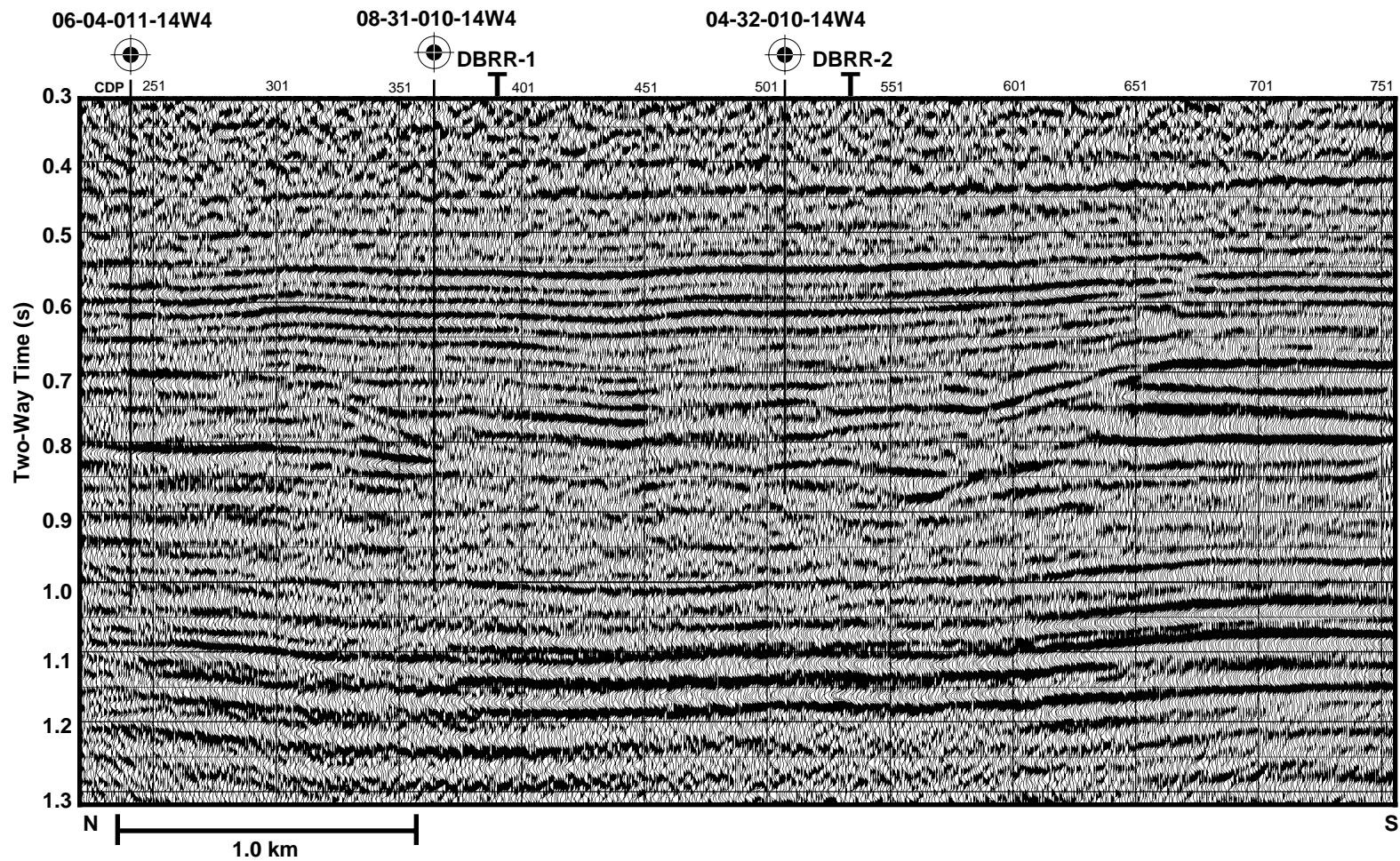


Fig. 4.11 Seismic line DBRR-3 over the Purple Springs structure. The three wells used for correlation and the tie with seismic lines DBRR-1 and DBRR-2 are also shown.

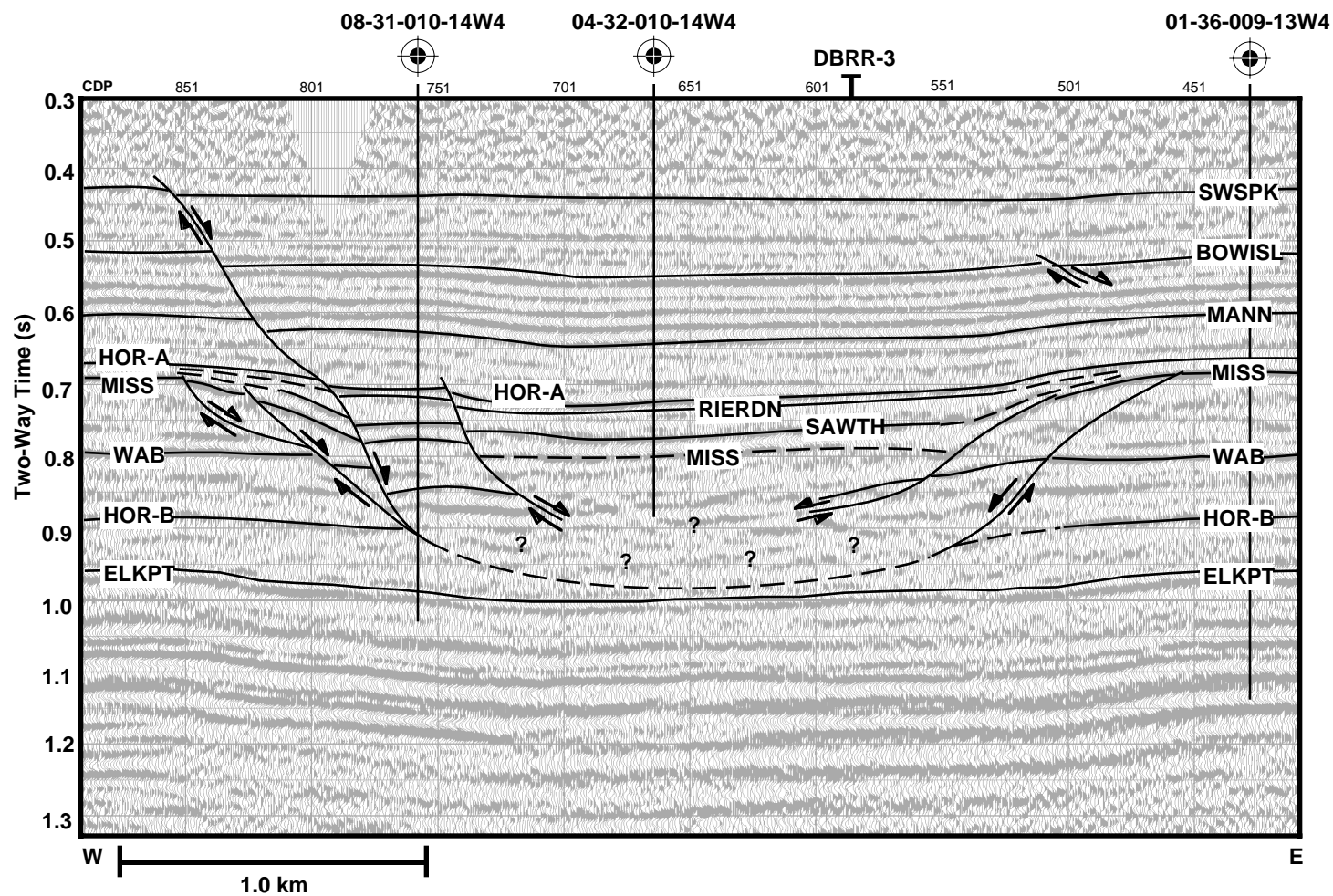


Fig. 4.12 Interpretation of seismic line DBRR-1. The structure appears to be bowl-shaped with rim faulting and a chaotic core denoted by "?".

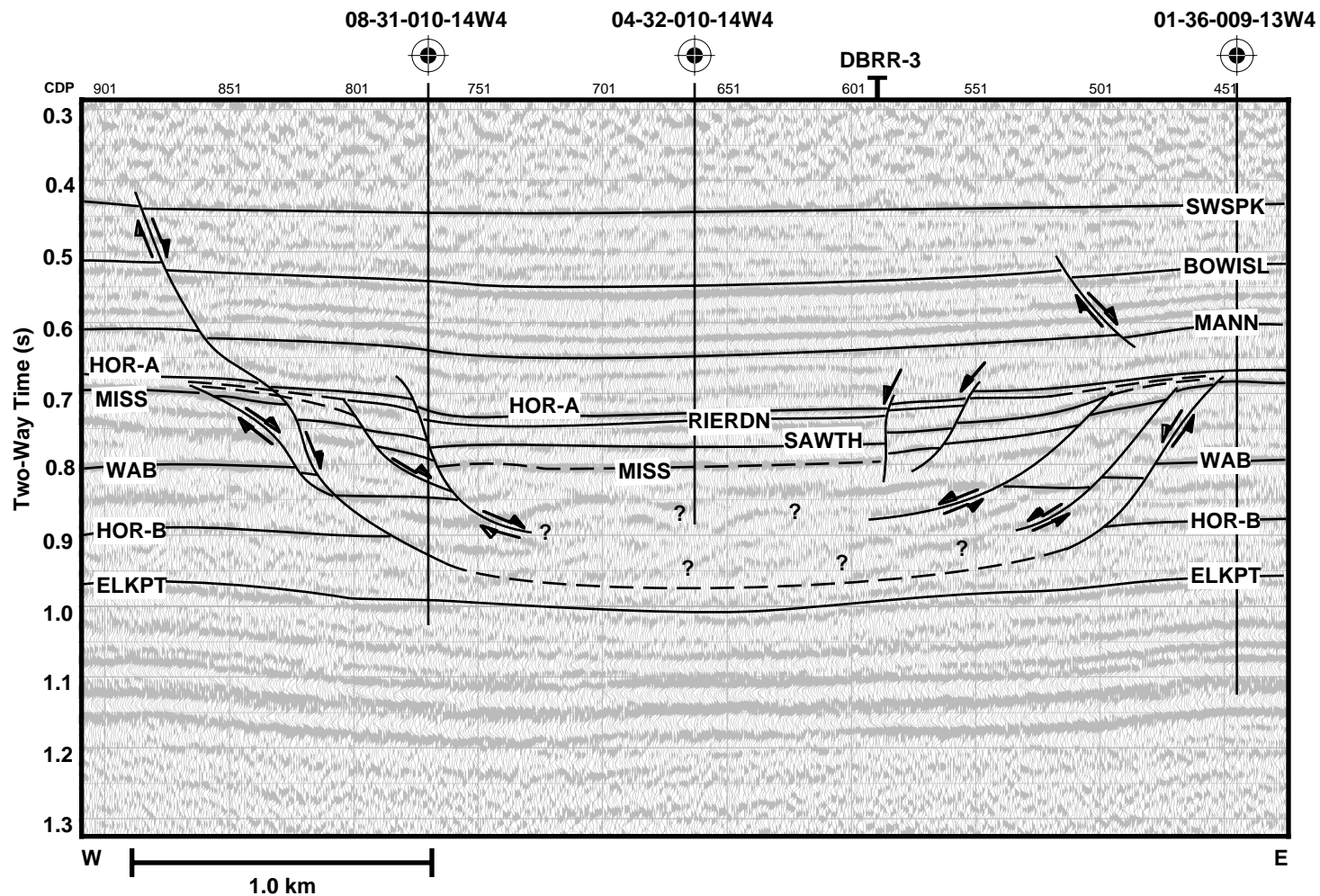


Fig. 4.13 Interpretation of seismic line DBRR-2. Parralleling line DBRR-1, which lies to the north, the interpreted structure appears similar.

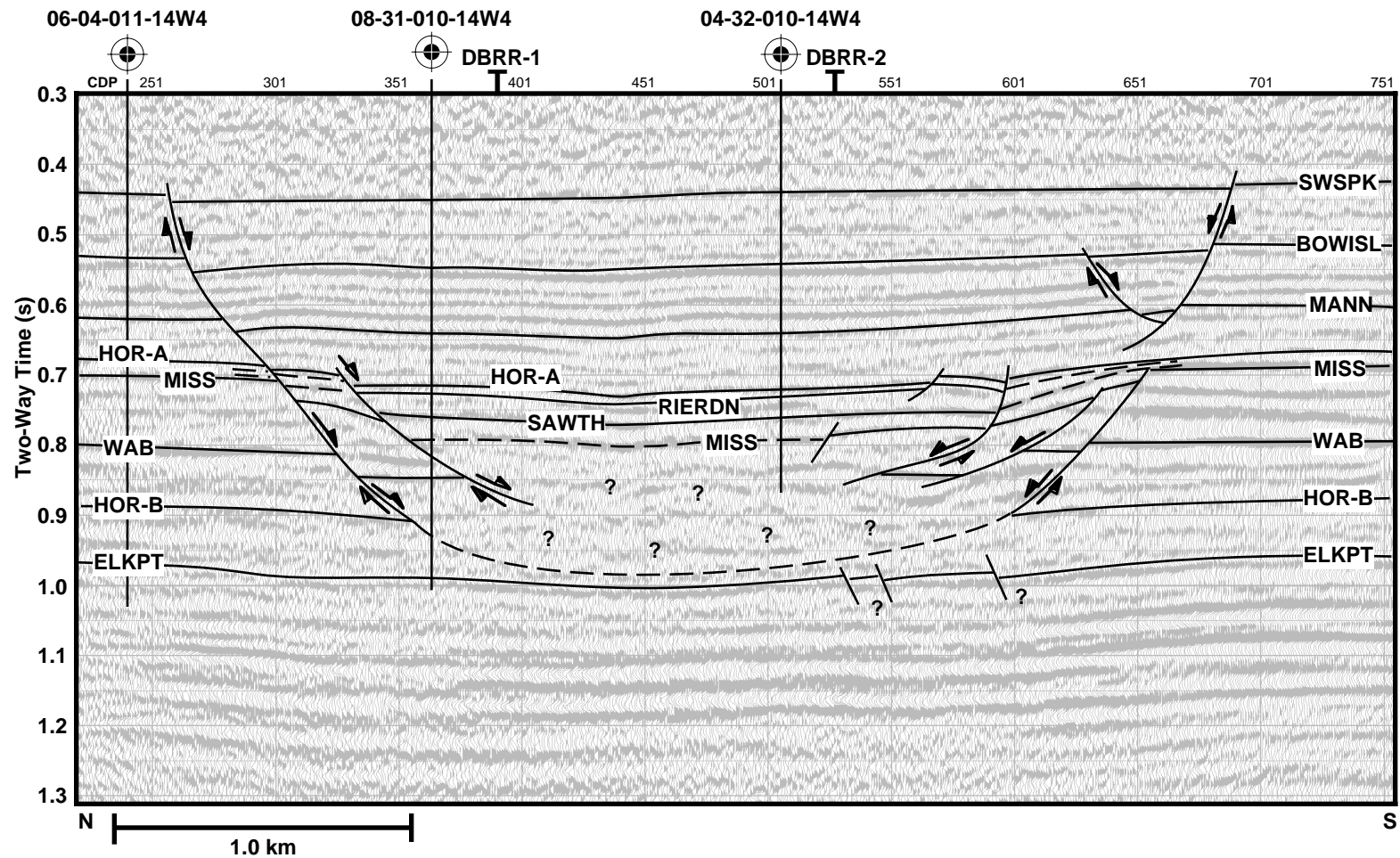


Fig. 4.14 Interpretation of seismic line DBRR-3. This line shows possible faulting at the ELKPT horizon. It is unclear what causal association these faults may have to the structure.

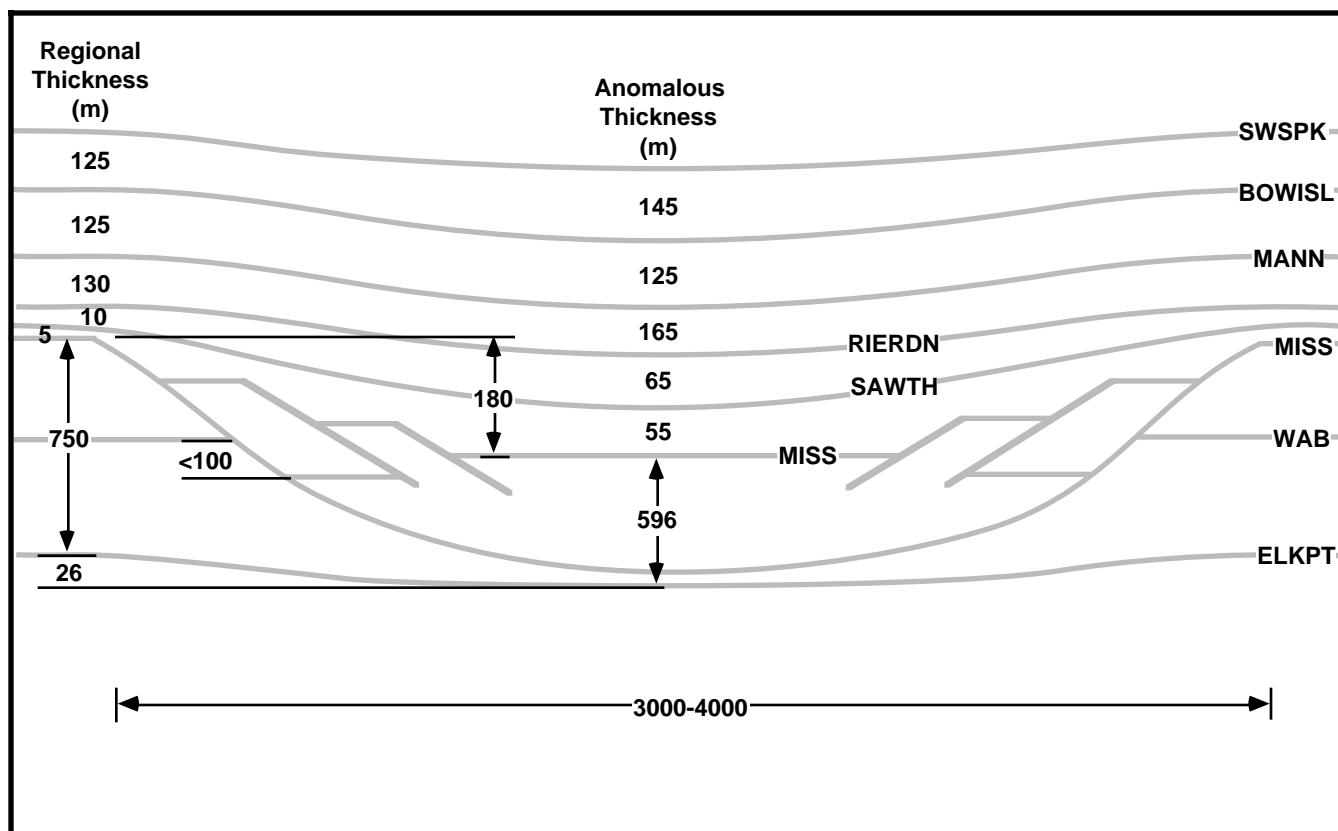


Fig. 4.15 Schematic representation of the Purple Springs structure showing relevant dimensions as measured from the seismic and well data. Diagram is not to scale and all measurements are in meters.

CHAPTER 5 - CONCLUSIONS

5.1 INTRODUCTION

The purpose of this work was to study the use of reflection seismic data as a tool to help recognize an impact origin for subsurface structures. Currently, the only accepted method of determining such an origin without direct evidence of the meteorite itself or its characteristic geochemical signature in target rocks, is through the discovery of shock metamorphic affects in the target rocks, whether they manifest themselves as shatter cones, high-pressure mineralogical phases or shock lamellae in minerals. In the case of surface features on land, these data can be relatively easy to gather, particularly if rocks outcrop in the area, and the crater itself has a topographic expression. However, in the cases where the features are buried beneath the surface, or occur beneath the oceans, this type of conclusive data can be extremely difficult or expensive to obtain. Often, these features are located indirectly by an anomalous geophysical measurement and sometimes explored further by drilling in the quest for resources. In the case of the oil and gas industry, by far the most important exploration tool is the reflection seismic technique. In this work, I study two enigmatic structures of unknown origin, both of which are imaged on reflection seismic profiles. One, at White Valley, Saskatchewan appears similar to a complex impact crater, and the other, near Purple Springs, Alberta, was originally interpreted to be a simple impact crater. Both are major structural features of possible meteorite impact origin, however, as noted above, without definitive evidence of shock metamorphism, neither of these structures can be proven to be of impact origin. The hope is that by careful study of their seismic character, the impact hypothesis can be more readily substantiated or refuted.

5.2 THE WHITE VALLEY STRUCTURE

Interpretation of this structure, based on seismic reflection data and available well control, leads to the following specific conclusions. The feature is an obvious structural anomaly on seismic data as it disrupts an otherwise normal stratigraphic sequence apparently from near surface to a depth of some 1300 m. The Mississippian appears to be the deepest horizon affected by the structure with only some minor faulting and velocity pull-up apparent on the seismic profiles. The topography of the area, as seen on aerial photographs, shows what appears to be an erosional remnant ridge, arcuate in form, that can be extended to a circle with a diameter of 7.5 km. The structure itself is imaged primarily in horizons deeper than the Belly River formation, but extrapolation of its lateral limits to the surface gives a similar diameter for the structure. The rim of the White Valley structure is characterized by listric normal faults which delineate separate terraces which, in turn, step down towards an annular trough about 4 km in diameter. The core of the structure, some 2 km in diameter, demonstrates stratigraphic uplift of some 450-620 m and is characterized by incoherent reflections. The flanks of this central peak show evidence of slumping. Repeated sections apparent in logs from the 07-07 well, drilled on the flanks of the central core, indicate thrust rock units deeper in the structure as well as possible interfingering of material, although these repeats do not appear to be imaged on the seismic profiles. A gravity survey over the trough and central peak of the feature, coincident with seismic line WV-017, demonstrated a positive anomaly of nearly 3 mgal over the center of the structure. This profile is also bilaterally symmetric and is coincident with the general morphology of the structure as imaged in the seismic data. Using two simple models (a sphere and vertical cylinder), the anomaly can be explained by a realistic density anomaly of some 30 to 100 kg/m³ over the central portion of the structure. However, the well data

indicates a nearly 50 kg/m^3 density decrease over the center of the structure when compared to regional values.

Two possible origins for this structure were investigated. The first suggested that the structure was a kimberlite pipe and had been previously cited as a mechanism of origin in the literature. The kimberlite model was initially proposed largely due to the inverted cone shape of the central core of the structure and that the gravity anomaly could be modelled as a complex form of such a structure. However, a more detailed look at the physical characteristics of kimberlite pipes indicated deficiencies with this model. Kimberlites do not show extensive terraced rim structures such as is present at White Valley and are not expected to be greater than 1 km in diameter. The sides of the core of the structure dip at about $50\text{-}60^\circ$, not the typical $80\text{-}85^\circ$ noted for kimberlite pipes. Kimberlites also fail to show any structural uplift; horizons are usually tilted down toward the main pipe with little or no terracing. Coupled with the lack of any kimberlitic material in the 07-07 well, this model becomes even less plausible.

The second theory suggested a meteorite impact origin for the structure. The general morphology of the structure fits well with the predicted features from the model for a complex impact crater formed by high-velocity impact. The terraced rim, annular trough and central peak showing stratigraphic uplift are all commensurate with the impact hypothesis. The gravity data seems to indicate an overall negative anomaly over the structure with the central peak demonstrating a positive anomaly relative to the trough. This is not unusual based on other terrestrial examples of impact craters, however, more detailed modelling of the gravity response would help to constrain the gravity data better. The calculated transient crater, based on the rim diameter of the structure projected to the surface, does not fit the seismic data well unless some 200 to 1000 m of post-impact

erosion is invoked. This discrepancy may reflect an actual erosional component to the post-impact history of the structure or an inherent inadequacy with the chosen scaling criteria. Most other scaling criteria pertaining to the final geometry of the crater agree well with the seismic data. Thus, the meteorite impact hypothesis is favoured over the kimberlite model for the origin of this structure.

5.3 THE PURPLE SPRINGS STRUCTURE

The specific results of this interpretation, based on seismic data and well control can be summarized as follows. The regional geological setting is that of a fairly typical succession throughout the stratigraphic column from Paleozoic carbonates into Mesozoic and Cenozoic clastics. The paleogeography of this location was one of an emergent upland during the Lower Devonian with subsequent transgression-regression events in response to relative sea level changes and/or orogenic episodes. Most of the structural deformation occurred to the west of the Purple Springs area and this particular location would have been near the coastline of inland seas that generally stretched from northwestern Alberta and northeastern British Columbia into southern Saskatchewan, Manitoba and the mid-western United States. The structure itself is an elliptical depression with a maximum diameter of nearly 4 km and a minimum diameter of some 3 km. The structure disrupts primarily Mississippian and Devonian carbonate rocks with minor, simpler structure occurring shallower in the section. The deepest Devonian carbonates of the Elk Point Group are downdropped 26 m beneath the structure. Maximum vertical displacement occurs at the Mississippian horizon which is 180 m below regional levels at the center of the structure. The core of the structure, nearly 600 m thick, is characterized by incoherent reflections and is laterally delineated by normal faults at the rim of the structure. Terraces, with maximum vertical displacements of some 90 m, are imaged along the rim and step down into the structure. The structure is infilled with clastic sediments primarily Jurassic in age although thickening

of formations occurs up into the Cretaceous as well. The deepest clastic formations show the greatest thickening of some 50-55 m with shallower formations showing less thickening. Nonetheless, the shallowest correlated horizon, the Second White Speckled Shale formation, shows 20 m of structure indicating that the total thickening of sediments shallower than the Mississippian compensates for 160 m. Normal faulting, also more apparent in the lower clastics but continuing in some cases to the Second White Speckled Shale formation, indicates that structural deformation continued after the main Mississippian event. This may have been caused by processes within the Mississippian-Devonian portion of the structure in combination with increased overburden loading and compression during Mesozoic deposition.

Two hypotheses are put forward to explain the structure's origin. The first, based on original industry interpretations, is that the structure is the remnant simple crater left by a high-velocity impact. However, the application of scaling criteria and morphological considerations suggests the Purple Springs structure is more likely a complex impact crater. The structure does not compare favourably to a typical simple impact crater due to the presence of rim terraces, its large diameter compared to the simple-to-complex transition diameter expected for sedimentary rocks, the large thickness of the apparent breccia lens relative to its shallow depth, and its elliptical shape in plan view. However, it does not compare perfectly to typical complex craters mainly because of the lack of structural uplift in the center of the structure and the greater depth of the transient crater than the allowable stratigraphic thickness regionally. It is thought that post-impact processes altered the structure substantially to its current form.

The second hypothesis proposed the structure was the result of dissolution phenomena. Unfortunately, this hypothesis, while possibly able to explain the amount of vertical

structure, does not seem to justify a dissolution collapse feature covering such a large area. There appears to be no analogous structure of similar dimensions that has been attributed solely to dissolution. Nonetheless, dissolution may have played a role in deforming the original impact structure perhaps leading to preferential removal of the central uplift. The question of basement reactivation as a possible contributor to the formation of the structure is also still open since there is presently a lack of basement control to definitively say to what extent such structure exists. If such basement faulting was present, it may have provided a conduit for the brines required for dissolution. Further work is required to substantiate or refute these alternative hypotheses, but the impact theory remains the most likely.

5.4 GENERAL COMMENTS AND FUTURE WORK

In the course of interpreting the structures at White Valley, Saskatchewan and Purple Springs, Alberta, a number of general comments can be made about the difficulties encountered in trying to determine an impact origin for a structure based on seismic reflection data.

It appears that complex craters, being more distinct in their morphology are less likely to be confused with other endogenically produced structures. The White Valley structure, which seems to fit scaling criteria reasonably well, and lacks evidence for other endogenic mechanisms of origin, is likely a meteorite impact feature. On the other hand, the Purple Springs structure, which was originally interpreted to be a simple impact crater fits the scaling criteria for a complex impact crater better. Some problems with this analysis, however, suggests that endogenic processes contributed to the current form of the structure. An understanding of the expected geometrical relationships of crater morphology was therefore critical for this interpretation.

Definitive interpretations hinge a great deal on the level of preservation of the structure. Better preservation of the original impact structure will result in a better comparison with the models proposed by the scaling criteria. How other geological processes (e.g., dissolution, surface erosion, basement fault reactivation, tectonic movement) might affect these geometric relationships is important for correctly assessing the geometry of a given structure as seen on seismic data.

There are several endeavours which might help to further the usefulness of seismic data in the interpretation of impact structures and aid in our understanding of how they form. Searching for more examples of seismic data over these structures adds to the database of known structures and would help to refine scaling criteria for terrestrial craters. Palinspastic reconstruction of complex craters to their pre-modified state would help to define the size of the transient crater and may shed light on the mechanics of central uplift generation and rim faulting. For both case studies, a fairly typical processing runstream was used to produce a final migrated stack from which the interpretations were done. Seismic modelling of impact structures may help to understand imaging problems associated with processing of these seismic data such as velocity issues, the appropriateness of time migration versus depth migration, and the possible problems of side scatter energy contaminating 2-D seismic datasets. In the acquisition of seismic data, we have already seen that 3-D seismic data gives superior images of crater morphologies whereby individual blocks of rock can be seen displaced from their pre-impact positions (refer to the James River structure, Chapter 1, Figure 1.16). However, 2-D datasets, acquired diametrically across the structure, reducing side-scatter noise are still useful. Finally, incorporating other datasets into the interpretation, such as gravity and aeromagnetic data, as well as geological information, both regionally and locally to the

structure, can only help to constrain the interpretation further, giving this unique hypothesis of structure origin more impact.

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