

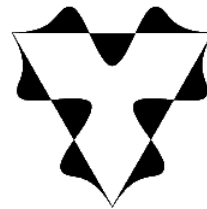
# AVAZ inversion for fracture orientation and intensity: A physical modeling study

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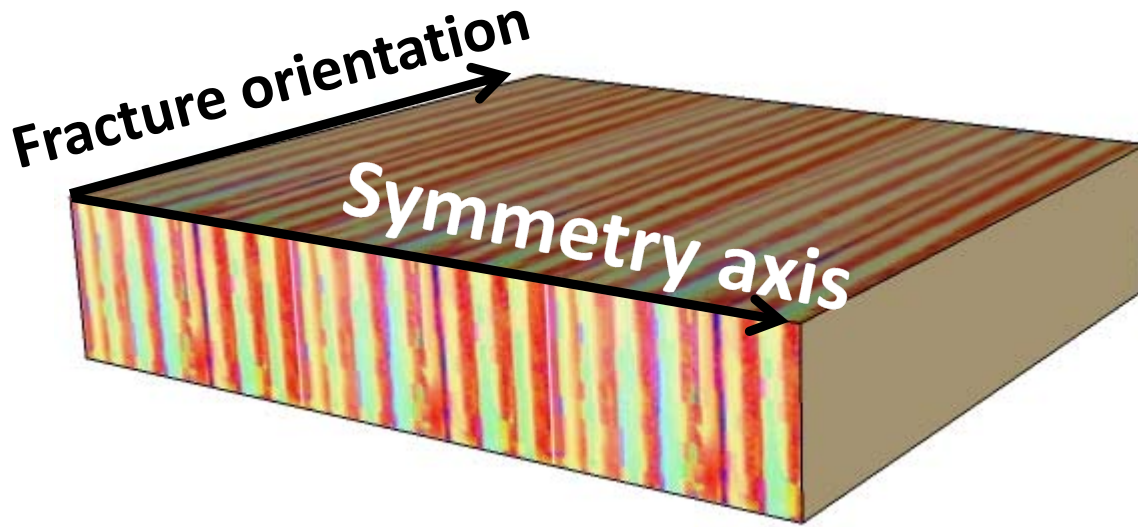


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**CREWES**

# Objective



**Fracture orientation:** direction of fracture planes

**Fracture intensity:** number of fractures in unit volume times (mean diameter)<sup>3</sup>

**P-wave AVAZ inversion for fracture orientation and intensity**

**Fracture orientation (Jenner, 2002)**

**AVAZ inversion using Rüger's equation for  $(\epsilon^{(v)}, \delta^{(v)}, \gamma)$ ,**

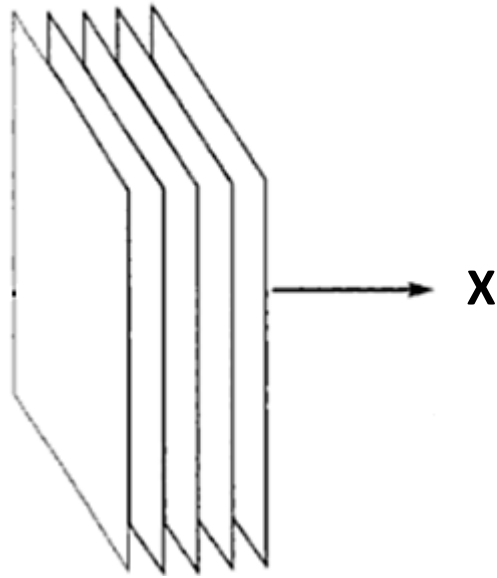
**$\gamma$  is directly related to fracture intensity**

# Outline

- HTI model
- Previous work on physical modeling
- Theory of AVAZ inversion
- Implementation on physical model data
- Conclusions
- Acknowledgements

# HTI (horizontal transverse isotropy)

Simple model to describe vertical fractures



- Vertical isotropic plane
- Horizontal symmetry axis
- $(\alpha, \beta, \varepsilon^{(V)}, \delta^{(V)}, \gamma)$  to describe the medium

$\alpha$  = P-vertical velocity

$\beta$  = S-vertical velocity ( $S^{\parallel}$ )

$$\varepsilon^{(V)} = \frac{V_{Px} - V_{Pz}}{V_{Pz}}$$

$$\gamma = \frac{V_{Sx} - V_{Sz}}{V_{Sz}}$$

$$\delta^{(V)} = \frac{(A_{13} + A_{55})^2 - (A_{33} - A_{55})}{2A_{33}(A_{33} - A_{55})}$$

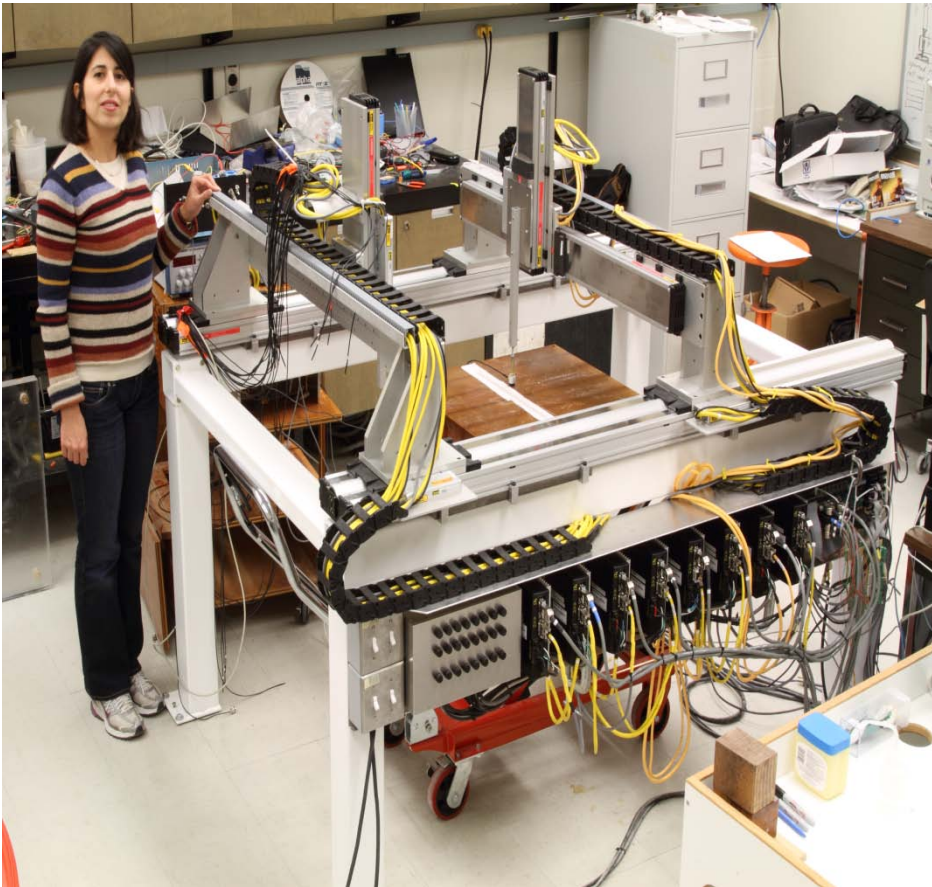
(Shear-wave splitting parameter) directly related to fracture intensity



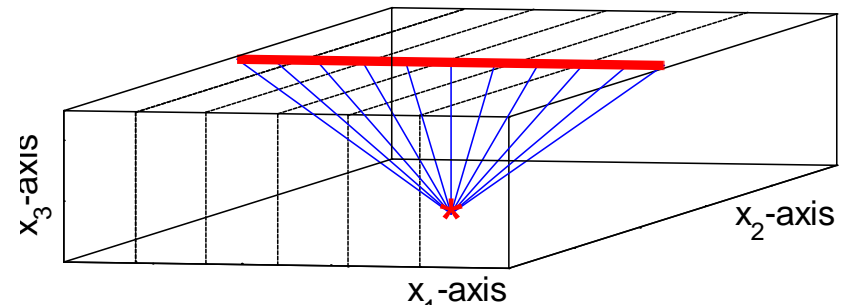
# Simulated fractured layer

(2010 work)

Phenolic layer  $\approx$  HTI

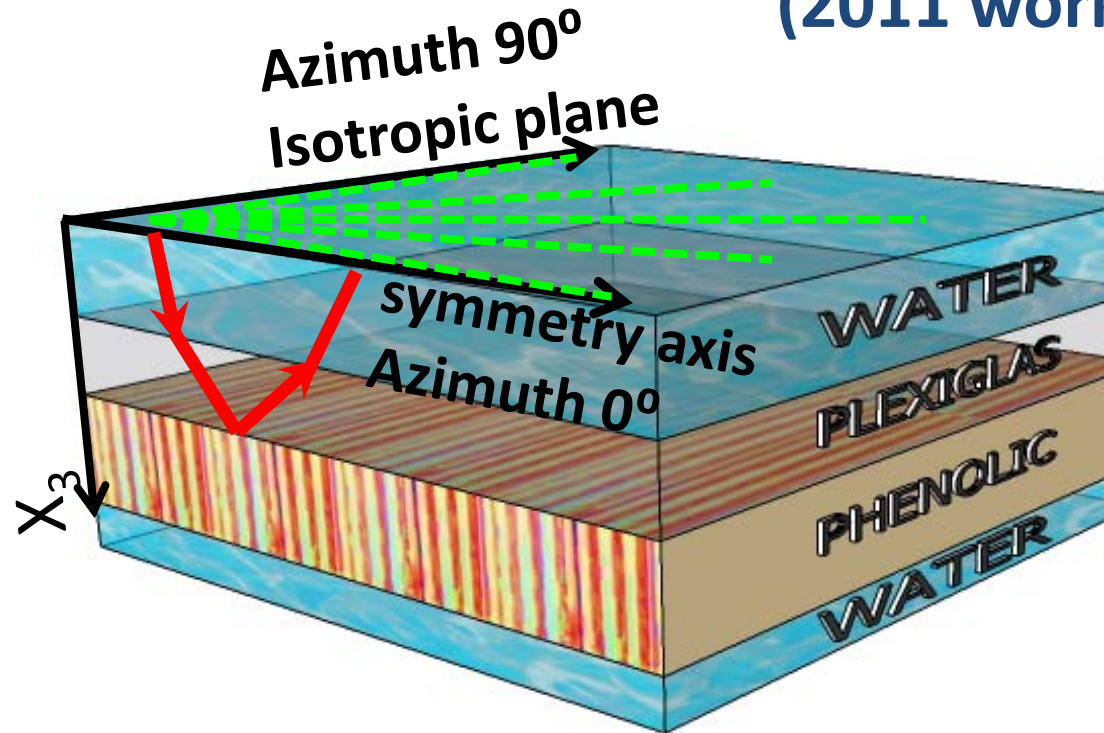


- Transmission shot gathers on single layer
- Traveltime inversion
- True  $(\epsilon^{(V)}, \delta^{(V)}, \gamma)$

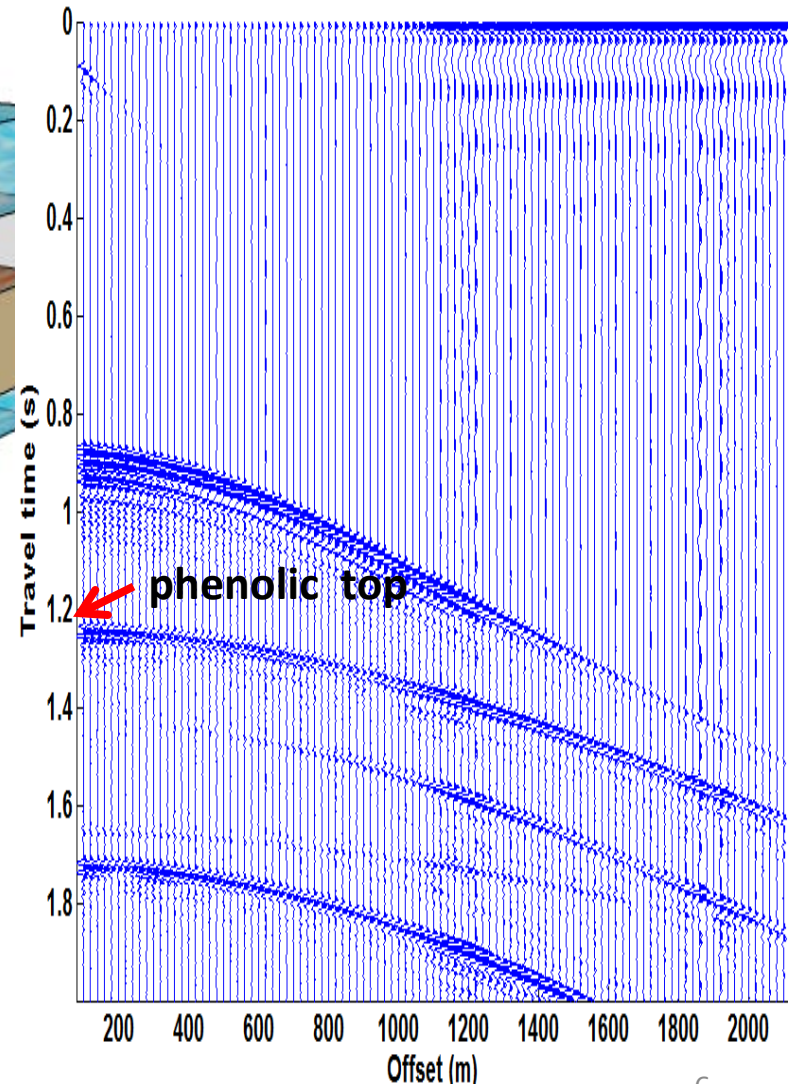


# Azimuthal AVO from reflection data

(2011 work)



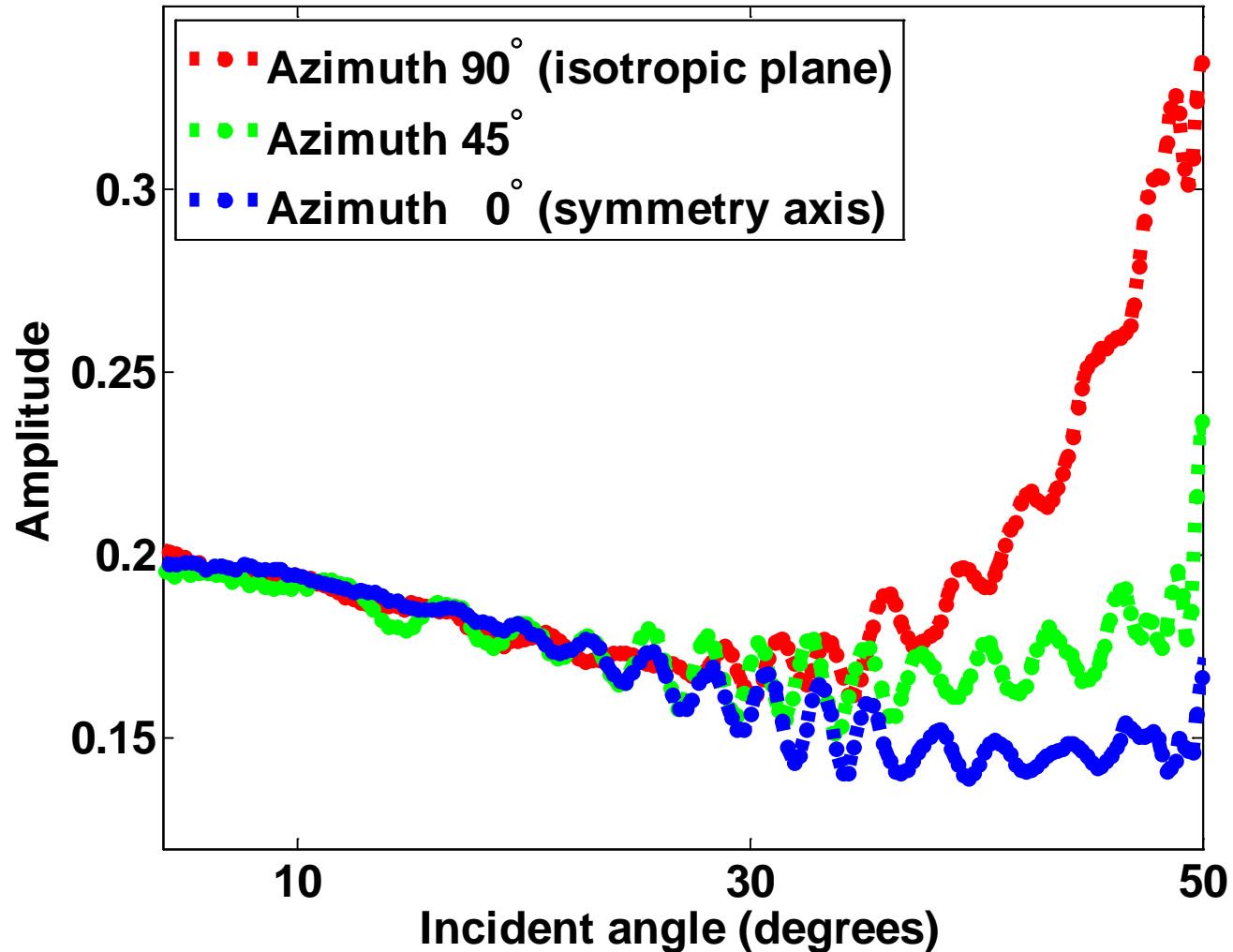
## Azimuth 90°



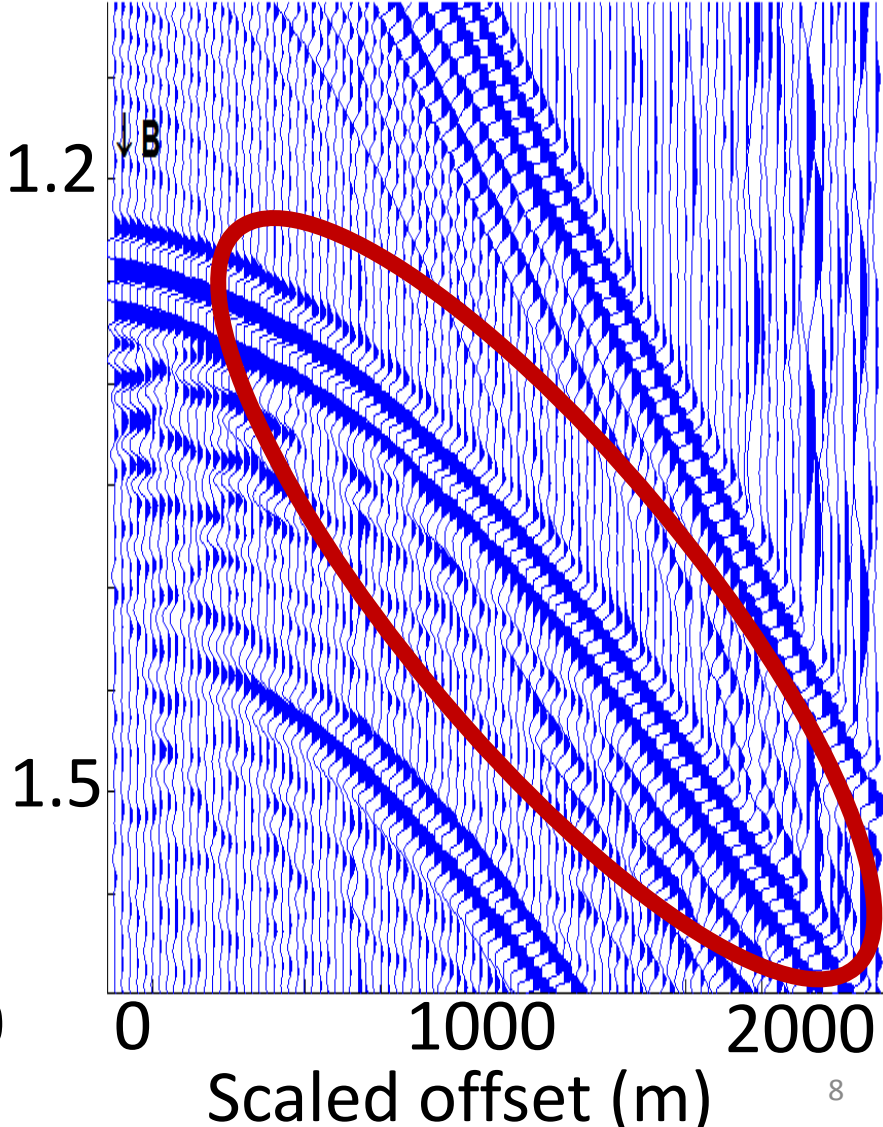
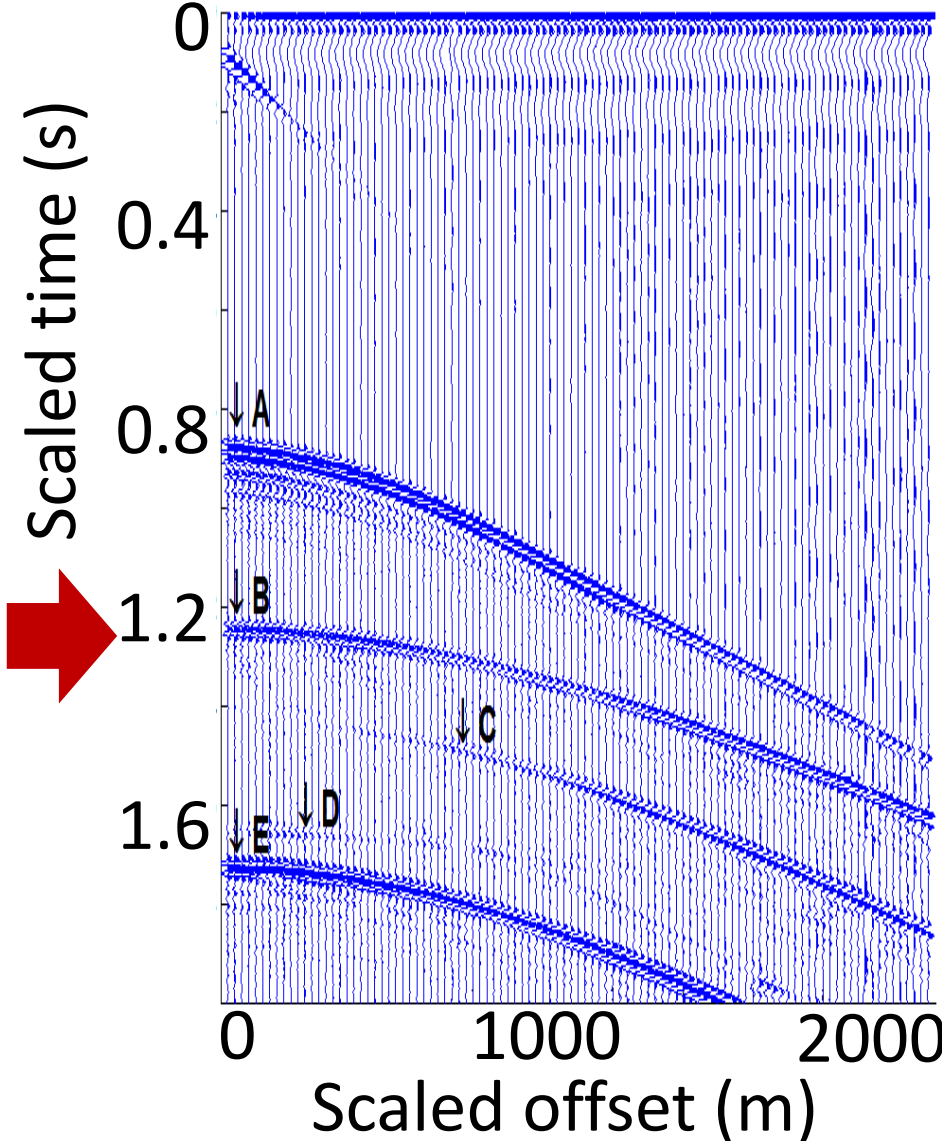
- Acquisition coordinate system along fracture system
- Azimuth lines: 0° to 90°
- Large offset data

# Amplitudes top fracture

## corrected amplitudes

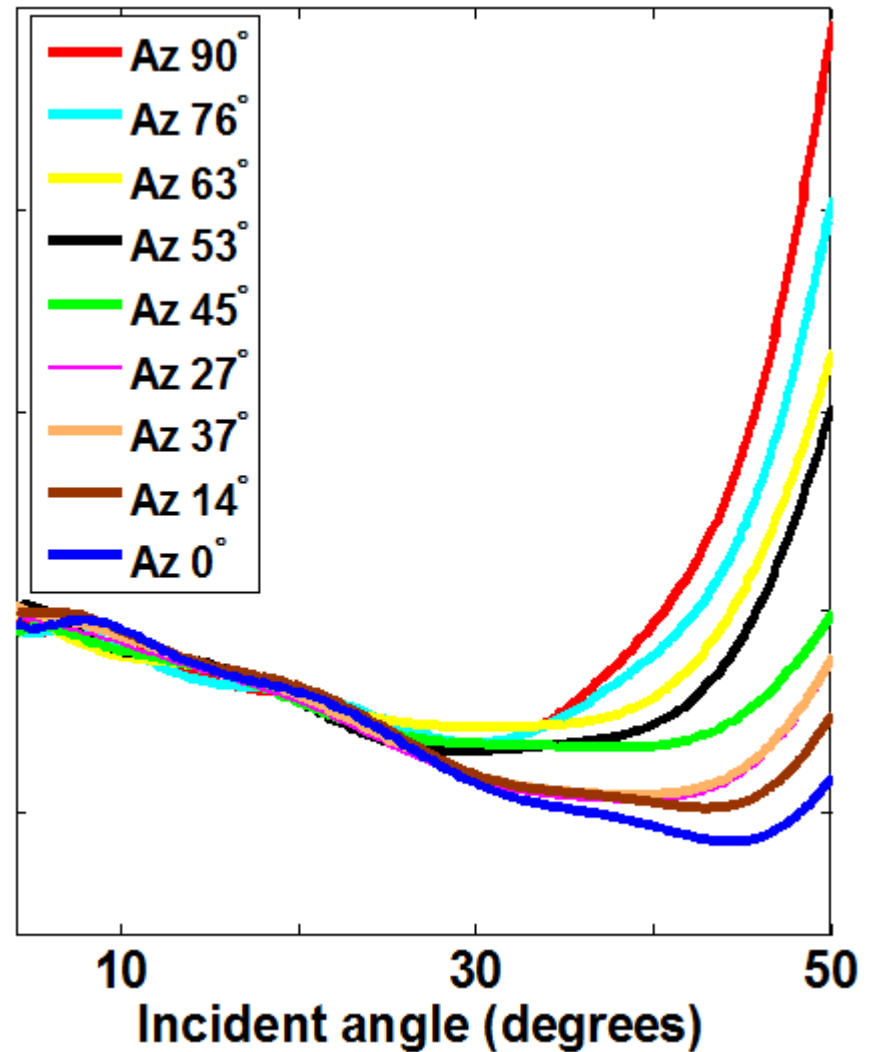
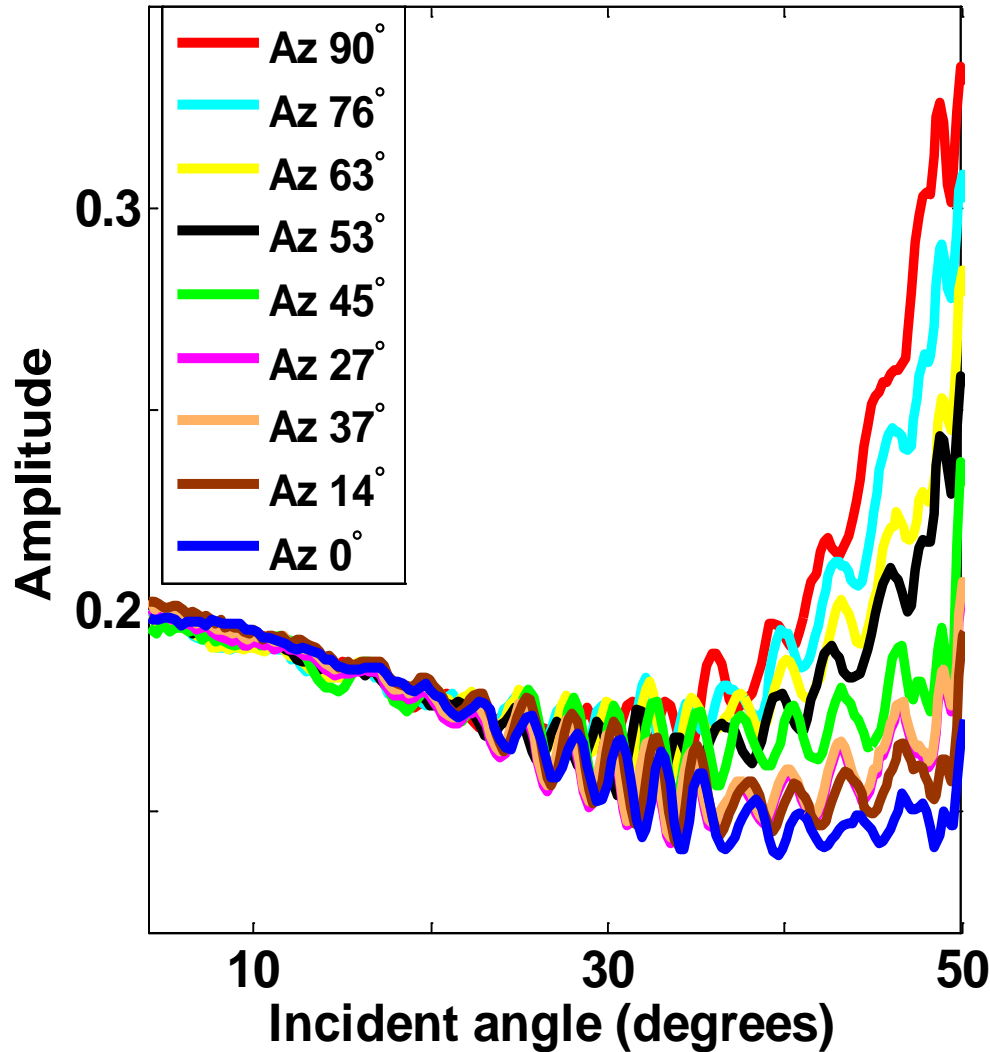


# Oscillations on amplitude data

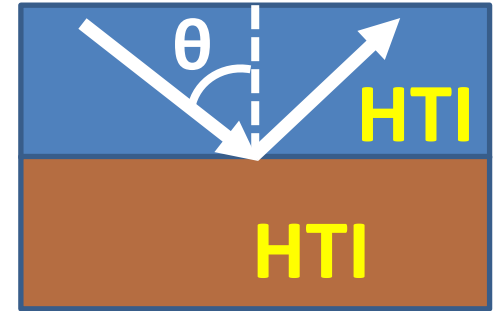




# Smoothing the amplitude data



# HTI: PP reflection coefficient (Rüger, 1997) ( known fracture orientation )



# HTI: PP reflection coefficient (Rüger, 1997)

## ( known fracture orientation )

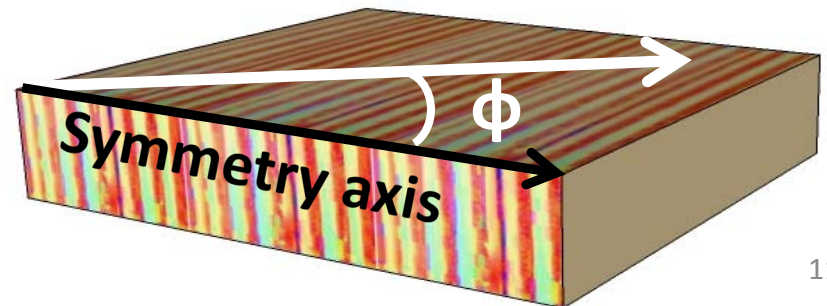
$$R_{PP}^{HTI}(\theta, \phi) \cong \frac{1}{2 \cos^2 \theta} \frac{\Delta \alpha}{\bar{\alpha}} - \frac{4\beta^2}{\alpha^2} \sin^2 \theta \frac{\Delta \beta}{\bar{\beta}} + \frac{1}{2} \left( 1 - \frac{4\beta^2}{\alpha^2} \sin^2 \theta \right) \frac{\Delta \rho}{\bar{\rho}} +$$

$$\frac{1}{2} \left( \cos^4 \phi \sin^2 \theta \tan^2 \theta \right) \Delta \varepsilon^{(V)} + \left( \frac{4\beta^2}{\alpha^2} \cos^2 \phi \sin^2 \theta \right) \Delta \gamma +$$

$$\frac{1}{2} \left( \cos^2 \phi \sin^2 \theta + \cos^2 \phi \sin^2 \phi \sin^2 \theta \tan^2 \theta \right) \Delta \delta^{(V)}$$

**$\theta$  : incident angle**

**$\phi$  : angle between source-receiver azimuth  
and fracture symmetry axis**



# Rüger's approximation

Aki and Richard approximation

$$R_{PP}^{HTI}(\theta, \varphi) \cong \frac{1}{2 \cos^2 \theta} \frac{\Delta \alpha}{\bar{\alpha}} - \frac{4\beta^2}{\alpha^2} \sin^2 \theta \frac{\Delta \beta}{\bar{\beta}} + \frac{1}{2} \left( 1 - \frac{4\beta^2}{\alpha^2} \sin^2 \theta \right) \frac{\Delta \rho}{\bar{\rho}} +$$

azimuthal  
dependent  
terms

$$\left[ \frac{1}{2} \left( \cos^4 \phi \sin^2 \theta \tan^2 \theta \right) \Delta \varepsilon^{(V)} + \left( \frac{4\beta^2}{\alpha^2} \cos^2 \phi \sin^2 \theta \right) \Delta \gamma + \right. \\ \left. \frac{1}{2} \left( \cos^2 \phi \sin^2 \theta + \cos^2 \phi \sin^2 \phi \sin^2 \theta \tan^2 \theta \right) \Delta \delta^{(V)} \right]$$

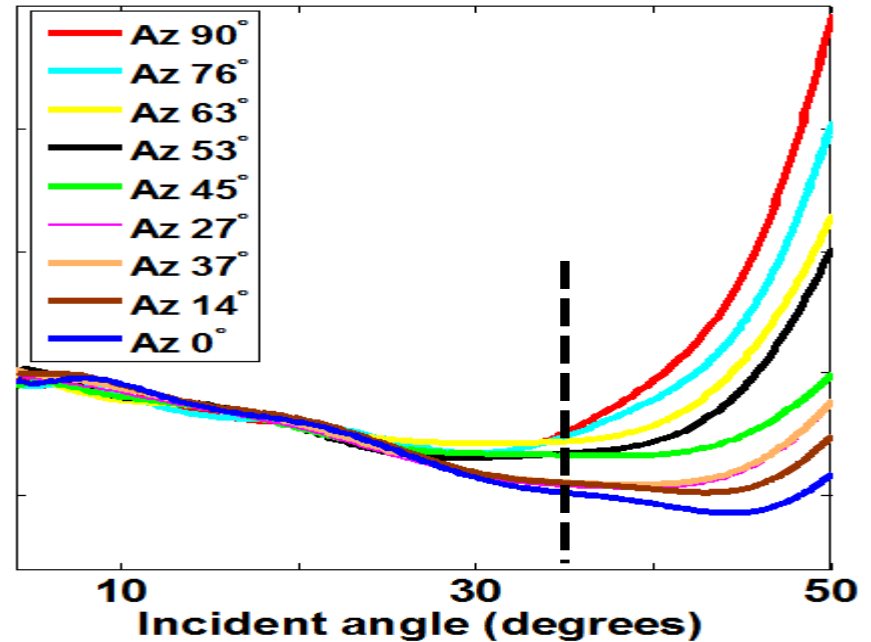
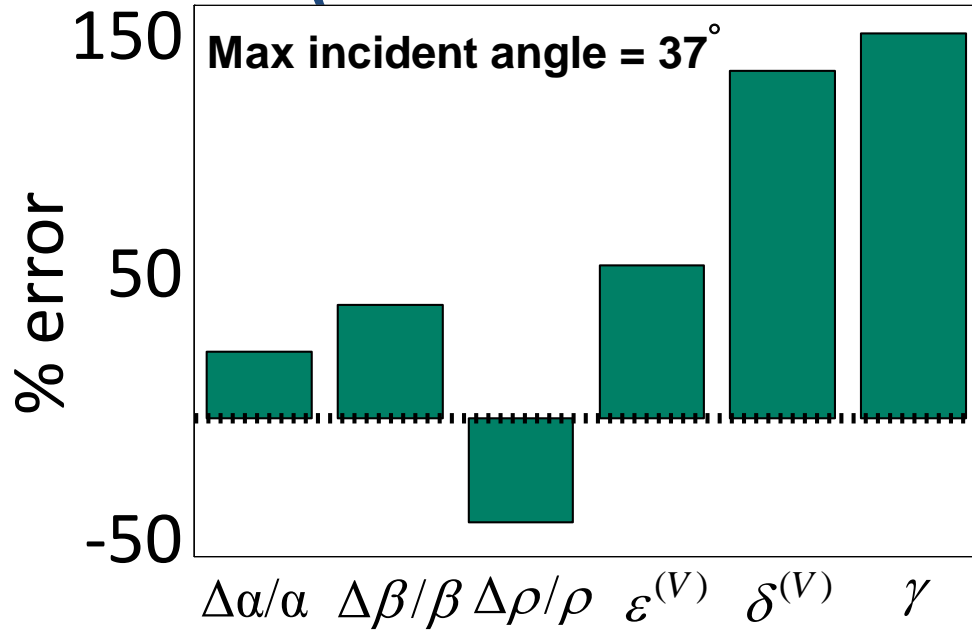
$$R \cong A \frac{\Delta \alpha}{\bar{\alpha}} + B \frac{\Delta \beta}{\bar{\beta}} + C \frac{\Delta \rho}{\bar{\rho}} + D \Delta \varepsilon^{(V)} + E \Delta \delta^{(V)} + F \Delta \gamma$$

At each offset, ray tracing using the overburden velocity model to obtain A, B, C, D, E, and F.



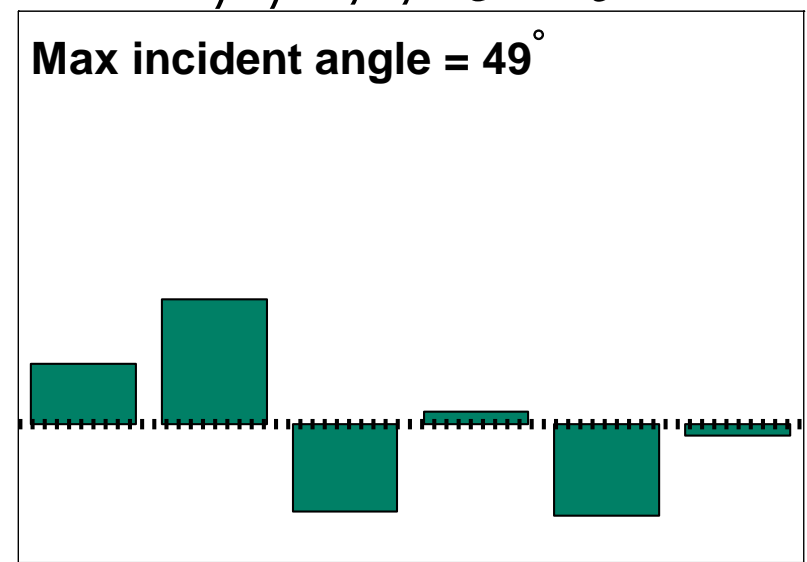
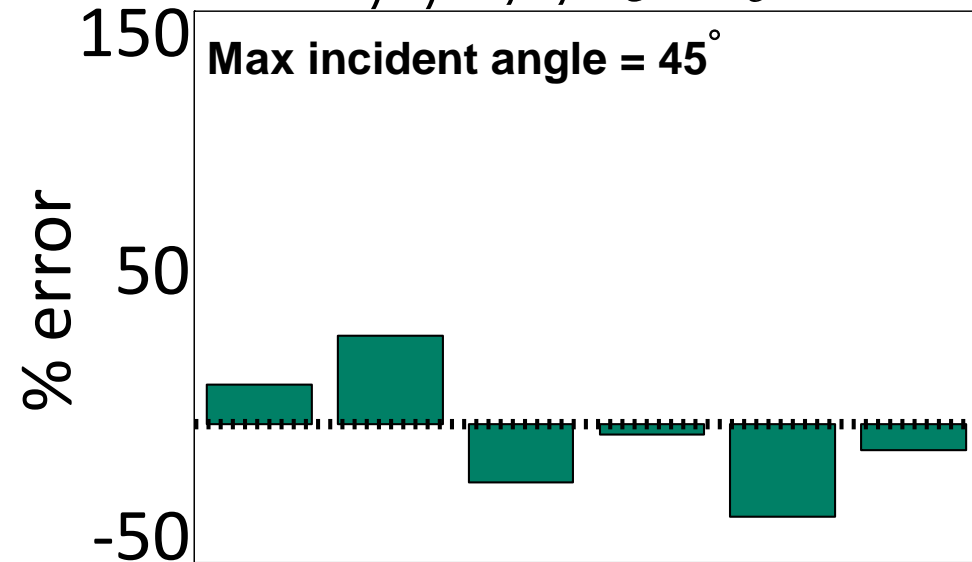
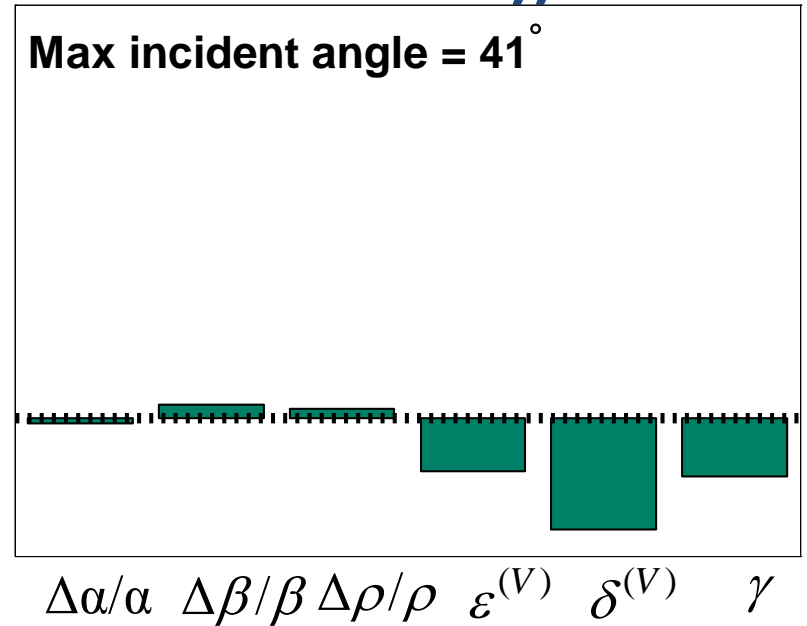
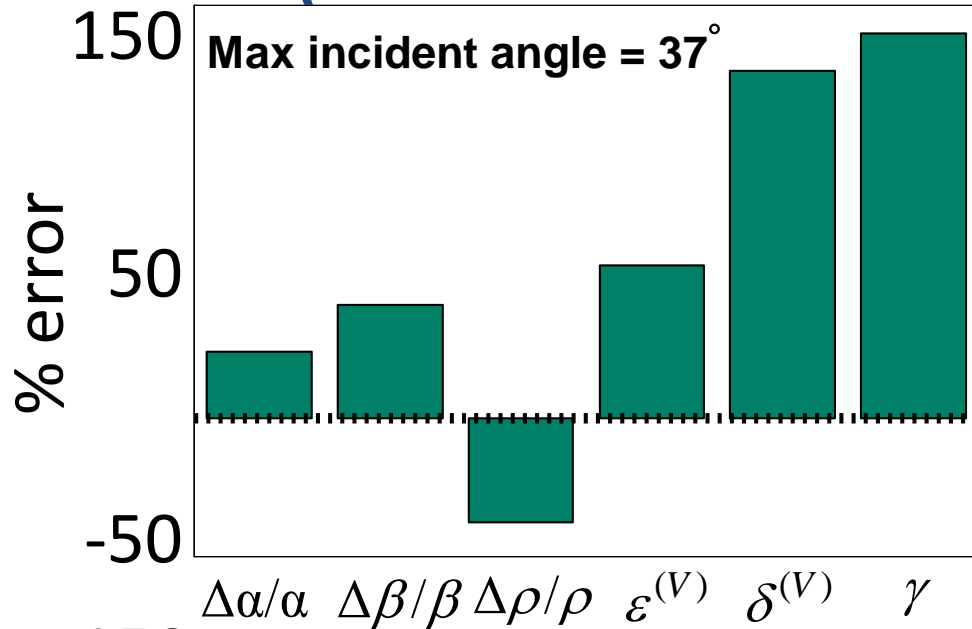
# AVAZ inversion for six parameters

(errors WRT travelttime inversion results)



# AVAZ inversion for six parameters

(errors WRT travelttime inversion results)



# AVAZ inversion for three-parameters (anisotropy parameters)

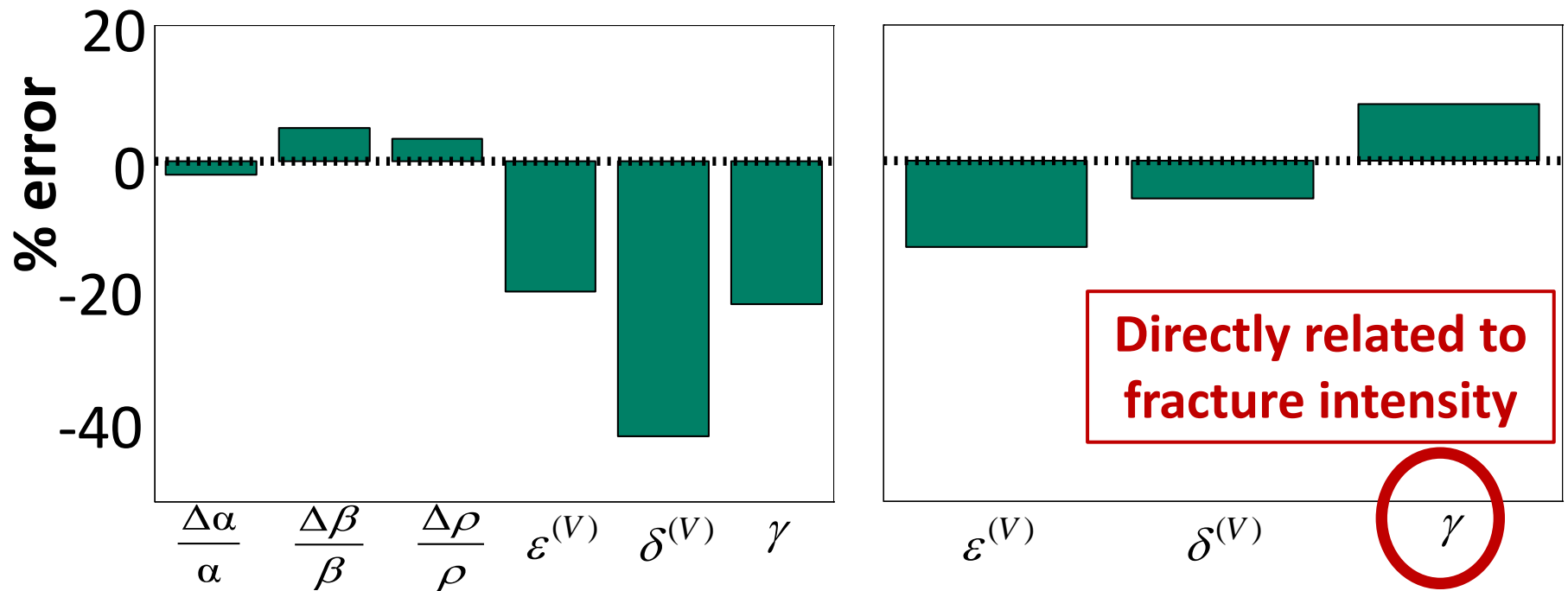
1. Determine (  $\Delta\alpha/\alpha$ ,  $\Delta\beta/\beta$ ,  $\Delta\rho/\rho$  )  
from logs, or  
from conventional AVA inversion of  
isotropic plane direction.
2. Invert for (  $\Delta\varepsilon^{(V)}$ ,  $\Delta\delta^{(V)}$ ,  $\Delta\gamma$  )  
using Rüger's equation  
constrained by results from step 1.



# AVAZ inversion

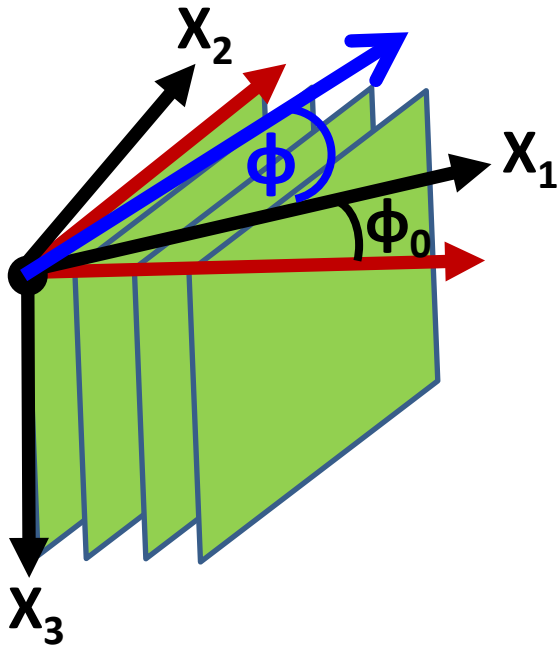
## 6-parameter vs. 3-parameter

Max incident angle =  $41^\circ$



Favourable results compared to those obtained previously by travelttime inversion

# Fracture symmetry axis not known



- : fracture system
- : acquisition coordinate
- $\phi$  : source-receiver azimuth
- \(\phi\_0\) : fracture symmetry direction

$$R_{PP}^{HTI}(\theta, \phi) \cong \frac{1}{2 \cos^2 \theta} \frac{\Delta \alpha}{\bar{\alpha}} - \frac{4\beta^2}{\alpha^2} \sin^2 \theta \frac{\Delta \beta}{\bar{\beta}} + \frac{1}{2} \left( 1 - \frac{4\beta^2}{\alpha^2} \sin^2 \theta \right) \frac{\Delta \rho}{\bar{\rho}} +$$

$$\frac{1}{2} \left( \cos^4(\phi - \phi_0) \sin^2 \theta \tan^2 \theta \right) \Delta \varepsilon + \left( \frac{4\beta^2}{\alpha^2} \cos^2(\phi - \phi_0) \sin^2 \theta \right) \Delta \gamma +$$

$$\frac{1}{2} \left( \cos^2(\phi - \phi_0) \sin^2 \theta + \cos^2(\phi - \phi_0) \sin^2(\phi - \phi_0) \sin^2 \theta \tan^2 \theta \right) \Delta \delta$$

# HTI: PP reflection coefficient

Small incident angle ( $\theta < 35^\circ$ )

$$R_{PP}^{HTI}(\theta, \phi) \cong \frac{1}{2 \cos^2 \theta} \frac{\Delta \alpha}{\bar{\alpha}} - \frac{4\beta^2}{\alpha^2} \sin^2 \theta \frac{\Delta \beta}{\bar{\beta}} + \frac{1}{2} \left( 1 - \frac{4\beta^2}{\alpha^2} \sin^2 \theta \right) \frac{\Delta \rho}{\bar{\rho}} + \left( \frac{4\beta^2}{\alpha^2} \Delta \gamma + \frac{1}{2} \Delta \delta^{(v)} \right) \cos^2(\phi - \phi_0) \sin^2 \theta$$

AVO intercept

**Q = AVO gradient**

$$R_{PP}^{HTI}(\theta, \phi) \cong I + [G_1 + G_2 \cos^2(\phi - \phi_0)] \sin^2 \theta$$

Isotropic gradient

Anisotropic gradient

$$G_2 = \frac{4\beta^2}{\alpha^2} \Delta \gamma + \frac{1}{2} \Delta \delta^{(v)}$$

**gradient non-linear with respect to ( $G_1, G_2, \phi_0$ )**

# Estimate fracture orientation

( Grechka and Tsvankin (1998); Jenner (2002) )

$$\begin{aligned}
 Q &= G_1 + G_2 \cos^2(\varphi - \varphi_0) \\
 &= (G_1 + G_2) \cos^2(\varphi - \varphi_0) + G_1 \sin^2(\varphi - \varphi_0) \\
 &= W_{11} \cos^2 \phi + 2W_{12} \cos \phi \sin \phi + W_{22} \sin^2 \phi
 \end{aligned}$$

$$Q = (G_1 + G_2)y_1^2 + G_1y_2^2$$

**Coordinate system aligned with fractures**

$$\begin{cases}
 y_1 = r \cos(\phi - \phi_0) \\
 y_2 = r \sin(\phi - \phi_0)
 \end{cases}$$

**Acquisition coordinate system**

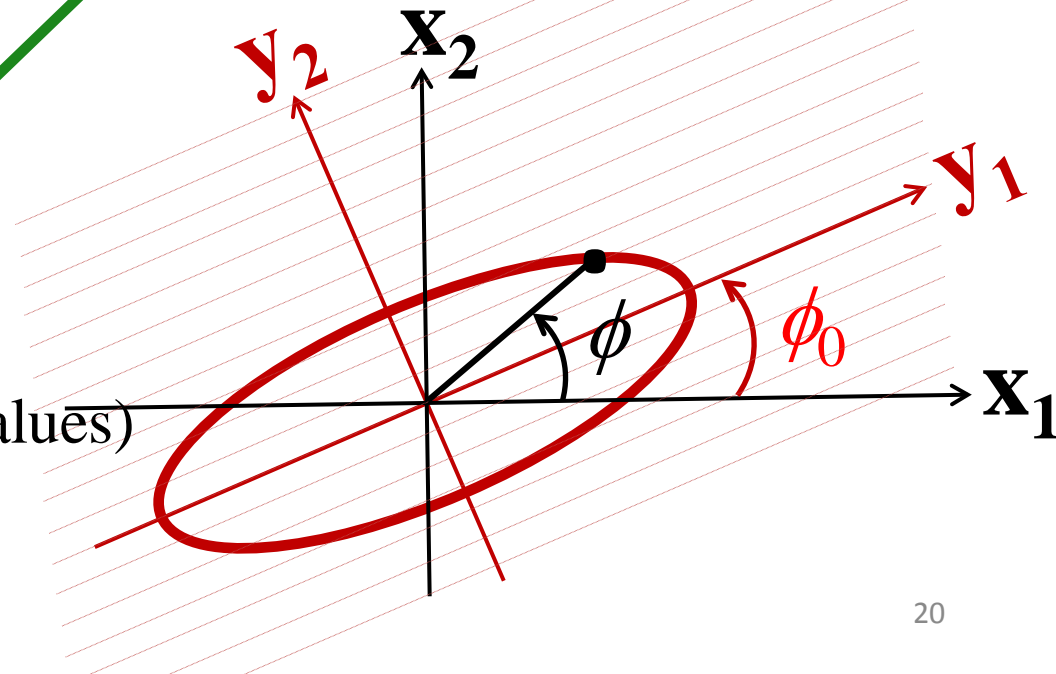
$$\begin{cases}
 x_1 = r \cos \phi \\
 x_2 = r \sin \phi
 \end{cases}$$

$$Q = W_{11}x_1^2 + 2W_{12}x_1x_2 + W_{22}x_2^2$$

$$= \begin{bmatrix} x_1 & x_2 \end{bmatrix} \begin{bmatrix} W_{11} & W_{12} \\ W_{12} & W_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$Q = \lambda_1 y_1^2 + \lambda_2 y_2^2 \quad (\lambda_{1,2} : \text{eigenvalues})$$

$$\tan(2\phi_0) = \frac{2W_{12}}{W_{11} - W_{22}}$$



# Estimate fracture orientation

( Grechka and Tsvankin (1998); Jenner (2002) )

$$\left\{ \begin{array}{l} \phi_0^{(1)} = \tan^{-1} \left( \frac{W_{11} - W_{22} + \sqrt{(W_{11} - W_{22})^2 + 4W_{12}^2}}{2W_{12}} \right) \\ \phi_0^{(2)} = \tan^{-1} \left( \frac{W_{11} - W_{22} - \sqrt{(W_{11} - W_{22})^2 + 4W_{12}^2}}{2W_{12}} \right) \end{array} \right.$$

$$\phi_0^{(2)} = \phi_0^{(1)} + \frac{\pi}{2}$$

**Accurate prediction of fracture orientation requires extra geological info, or azimuthal NMO velocity.**

# AVAZ inversion for fracture orientation ( small incident angle, $\theta < 35^\circ$ )

$$R(\theta, \phi) = I + \left( W_{11} \cos^2 \phi + 2W_{12} \cos \phi \sin \phi + W_{22} \sin^2 \phi \right) \sin^2 \theta$$

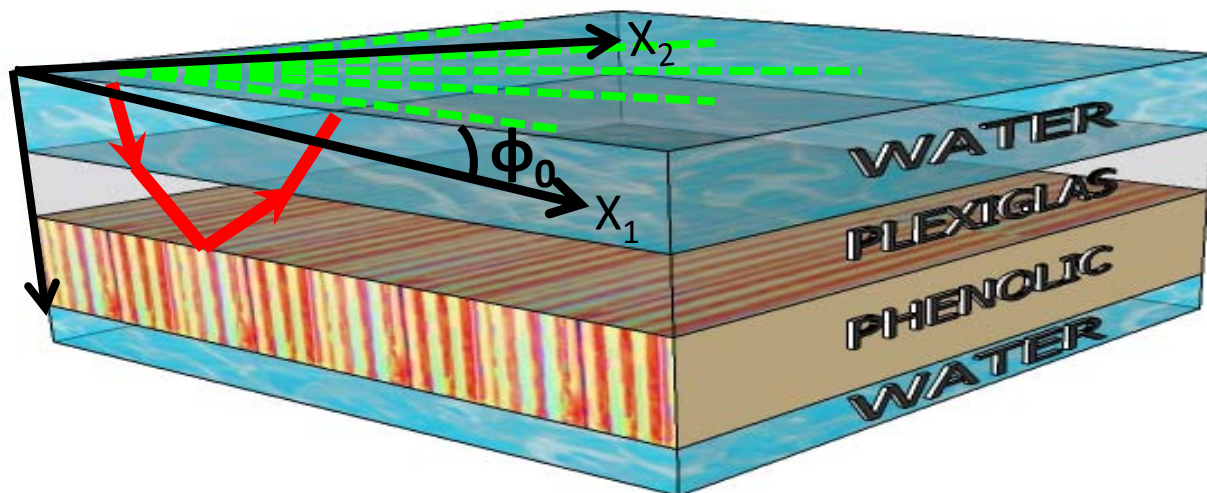
$$\begin{bmatrix} \cos^2 \phi_1 \sin^2 \theta_{11} & 2 \cos \phi_1 \sin \phi_1 \sin^2 \theta_{11} & \sin^2 \phi_1 \sin^2 \theta_{11} \\ \vdots & \vdots & \vdots \\ \cos^2 \phi_1 \sin^2 \theta_{n1} & 2 \cos \phi_1 \sin \phi_1 \sin^2 \theta_{n1} & \sin^2 \phi_1 \sin^2 \theta_{n1} \\ \vdots & \vdots & \vdots \\ \vdots & \vdots & \vdots \\ \cos^2 \phi_m \sin^2 \theta_{1m} & 2 \cos \phi_m \sin \phi_m \sin^2 \theta_{1m} & \sin^2 \phi_m \sin^2 \theta_{1m} \\ \vdots & \vdots & \vdots \\ \cos^2 \phi_m \sin^2 \theta_{nm} & 2 \cos \phi_m \sin \phi_m \sin^2 \theta_{1m} & \sin^2 \phi_m \sin^2 \theta_{1m} \end{bmatrix}_{(nm \times 3)} \begin{bmatrix} W_{11} \\ W_{12} \\ W_{22} \end{bmatrix}_{(3 \times 1)} = \begin{bmatrix} R_{11} - I \\ \vdots \\ R_{n1} - I \\ \vdots \\ \vdots \\ R_{1m} - I \\ \vdots \\ R_{nm} - I \end{bmatrix}_{(nm \times 1)}$$

**Least squares inversion for  $(W_{11}, W_{22}, W_{33})$**

# Test on physical model data, AVAZ inversion

$$\phi_0 = 30^\circ$$

$\phi_0$ : fracture symmetry axis azimuth



True $\phi_0$	$30^\circ$
Estimate $\phi_0$	$28.5^\circ$ and $118.5^\circ$

# Testing different fracture orientations

$\phi_0$ : fracture symmetry axis azimuth

True $\phi_0$	$0^\circ$	$10^\circ$	$20^\circ$	$40^\circ$	$60^\circ$	$80^\circ$	$90^\circ$
Estimate $\phi_0$	$-1.5^\circ$	$8.5^\circ$	$18.5^\circ$	$38.5^\circ$	$58.5^\circ$	$78.5^\circ$	$88.5^\circ$
	$88.5^\circ$	$98.5^\circ$	$108.5^\circ$	$128.5^\circ$	$148.5^\circ$	$168.5^\circ$	$178.5^\circ$



# Conclusions

- Rüger equation for HTI, PP reflection coefficient, can be used in an inversion for anisotropy parameters, but fracture orientation must be known.
- Knowing the fracture orientation, fracture intensity can be estimated from AVAZ inversion of large-offset data .
- Fracture orientation can be determined from AVAZ inversion of small incident angle data, but with  $90^{\circ}$  ambiguity.
- Implementation on physical model data gives results consistent with these theories.

# Acknowledgments

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