



# Interpretation of a multicomponent walkaway VSP experiment

*CREWES Project*

*Department of Geoscience*

*University of Calgary*

**Bona Wu, Don Lawton and Kevin Hall**

**Nov, 2015**



# Outline

---



- **Introduction**
  - Objectives
  - Advantages of VSP data
  - Acquisition and processing of the VSP data
  
- **Interpretation**
  - Geological background of the study reservoir
  - Post-stack and pre-stack inversion of P-wave data
  - AVO analysis and modeling of P-wave data
  - PP-PS joint inversion and comparison to P-wave inversion
  
- **Summary**
  
- **Acknowledgements**

# Objective

---



## Apply multicomponent VSP data to characterize the target reservoir

- Obtain rock properties and fluid information by inversion and AVO analysis on the P-wave data
- Conduct PP-PS joint inversion, add details to P-wave interpretation

# Why 3C walkaway VSP data?

---



- **Converted-wave data enhance traditional P-wave exploration**
- **Accurate time-depth conversion of geological features**
- **High S/N, broad-band data**
- **Deterministic deconvolution**
- **Can obtain robust reflection coefficients**
- **Walkaway VSP geometry is ideal for AVO analysis**



# 3C walkaway VSP acquisition

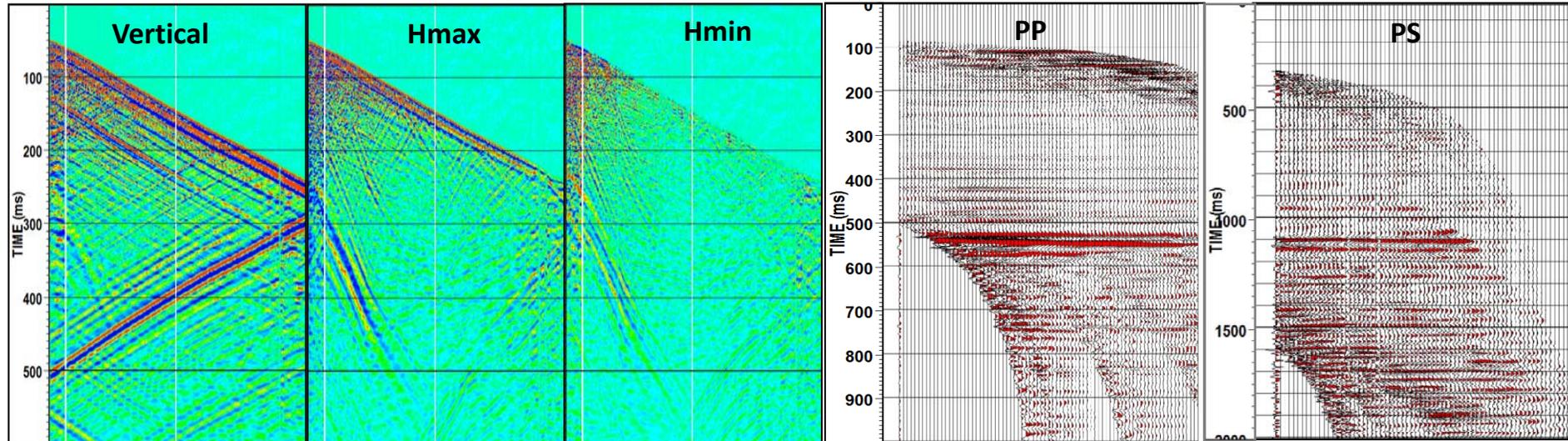


## Acquisition parameters & geometry

	Dynamite	Vibroseis
Receiver type	VectorSeis	VectorSeis
Number of receivers/spacing	220/2m	220/2m
Receiver depth (m)	55-507	55-507
Sample rate (ms)	1	1
Record length (s)	3	3
Offset (m)	11.5-1031	11.5-1031
Charge (kg)/ Sweep	0.125	EnviroVibe, 10-300Hz, over 20s, linear, one sweep per vibe point, 100/1000ms taper
Borehole	562m TD, vertical, no fluids in borehole	



# Shot record and processed image

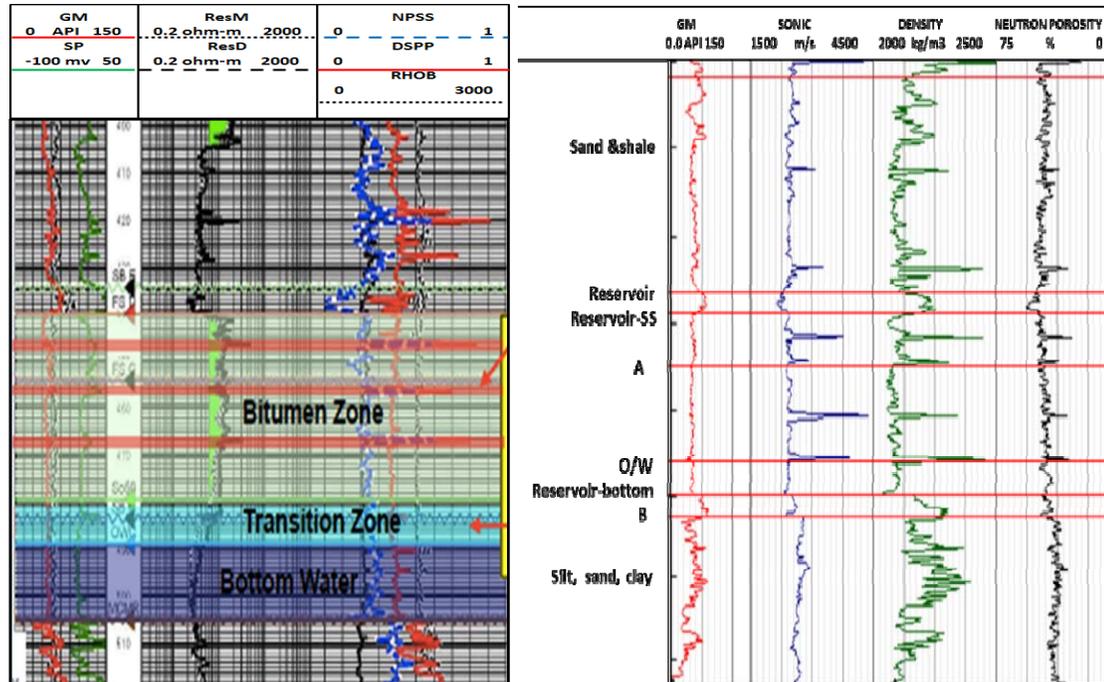


Shot record

Processed images



# Geology and well log analysis



Typical logs in study area

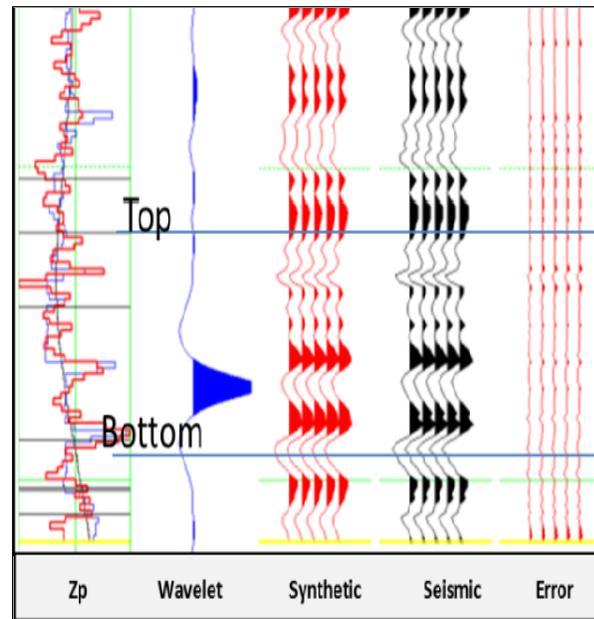
Logs from well A

- a heavy oil reservoir
- deposited as incised valleys, encased within deltaic, shoreface sands and marine muds
- relatively shallow (500 m), with unconsolidated/partially consolidated sand/shale sequence
- thickly bedded sandstone reservoir (50-75 m)
- high porosity (20-30%)

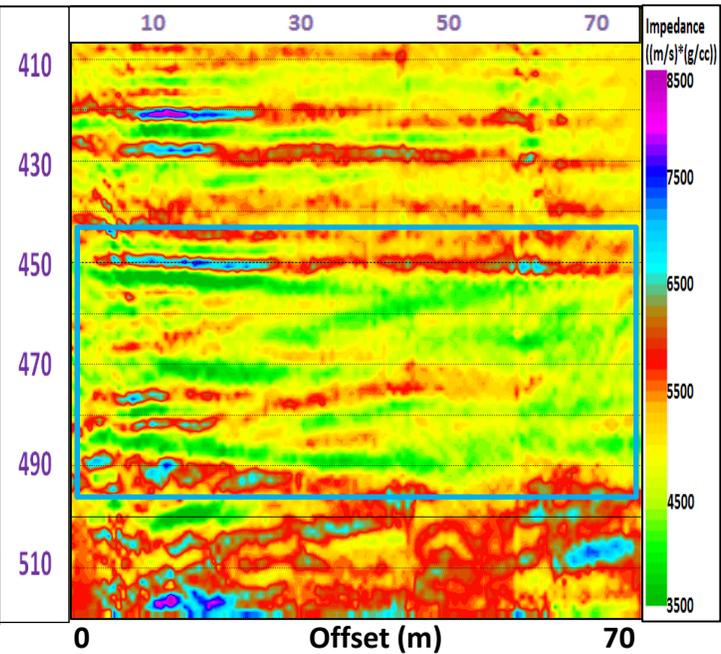
# P-wave post-stack inversion



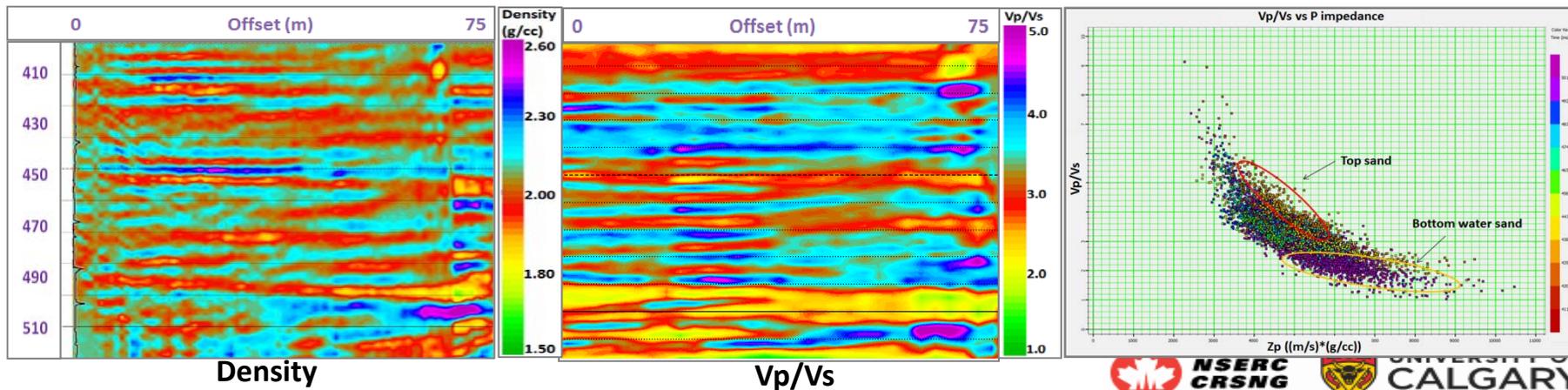
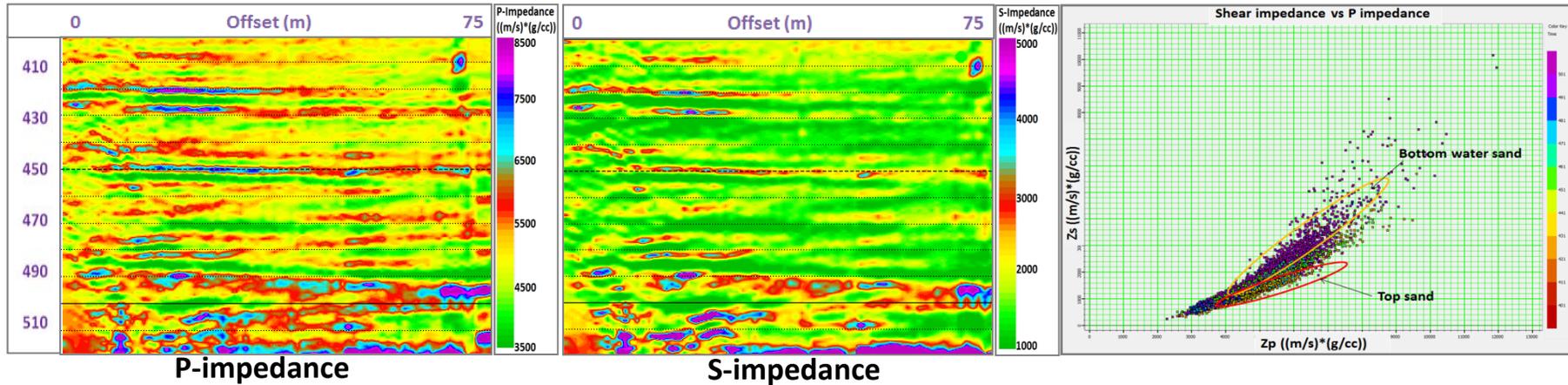
## Inversion analysis



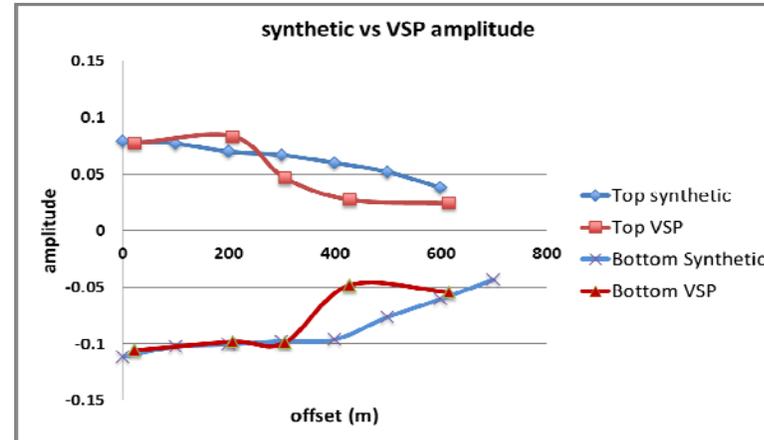
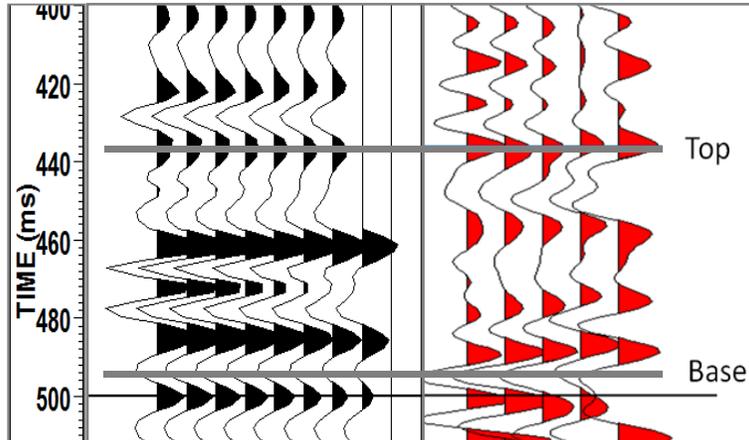
## P-impedance



# P-wave pre-stack inversion



# P-wave AVO responses



	$V_p=2122$ m/s $V_s=1061$ m/s $\rho=2.186$ g/cc
	$V_p=2229$ m/s $V_s=1114$ m/s $\rho=2.169$ g/cc
<b>reservoir</b>	$V_p=2584$ m/s $V_s=1292$ m/s $\rho=2.117$ g/cc
	$V_p=2354$ m/s $V_s=1177$ m/s $\rho=2.086$ g/cc

Reservoir	Top	Base
Interface	shale-sand	sand-shale
Impedance change	+ve	-ve
Amplitude	+ve	-ve
Amplitude change	Decreases with offset	Decreases with offset
Poisson's ratio	Decrease	Increase
AVO classification	I	IV
	Wet sand, no gas response	



UNIVERSITY OF CALGARY

# AVO attributes



	Two-term Aki-Richard	Two-term Fatti method
Attributes	Intercept A	Rp0
	Gradient B	Rs0
Derived attributes	AVO product: A*B	Zp
	Poisson's ratio change : A+B	Zs
	Shear wave reflectivity: A-B	Lambda-Mu-Rho

Wiggins' form (1986) of Aki-Richard equation is:

$$R_{\theta} = A + B \sin^2 \theta$$

where:

$$A = \left[ \frac{\Delta V_p}{2V_p} + \frac{\Delta \rho}{2\rho} \right] \text{ and } B = \frac{\Delta V_p}{2V_p} - 4 \left[ \frac{V_s}{V_p} \right]^2 \frac{\Delta V_s}{V_s} - 2 \left[ \frac{V_s}{V_p} \right]^2 \frac{\Delta \rho}{\rho}$$

A is called the intercept, B the gradient, and the A\*B called AVO product.

Fatti et al.(1994) rewritten Aki-Richards equation as:

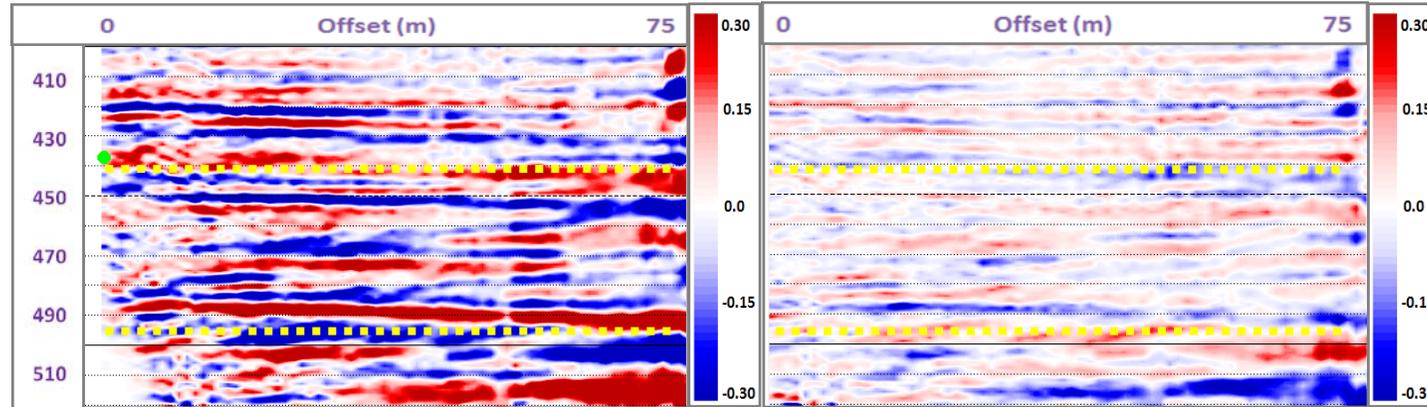
$$R_p(\theta) = c_1 R_p(0^0) + c_2 R_s(0^0)$$

$$\text{Where } R_p(0^0) = \frac{1}{2} \left[ \frac{\Delta V_p}{V_p} + \frac{\Delta \rho}{\rho} \right] \text{ and } R_s(0^0) = \frac{1}{2} \left[ \frac{\Delta V_s}{V_s} + \frac{\Delta \rho}{\rho} \right]$$

$$c_1 = 1 + \tan^2 \theta, c_2 = -8 \left( \frac{V_s}{V_p} \right)^2 \sin^2 \theta$$

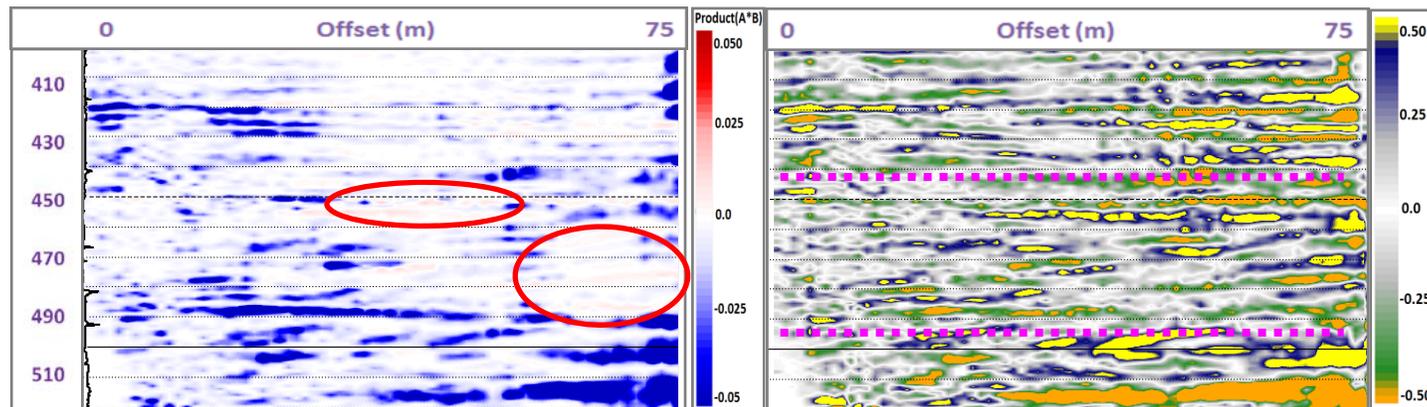


# AVO attributes analysis



Intercept

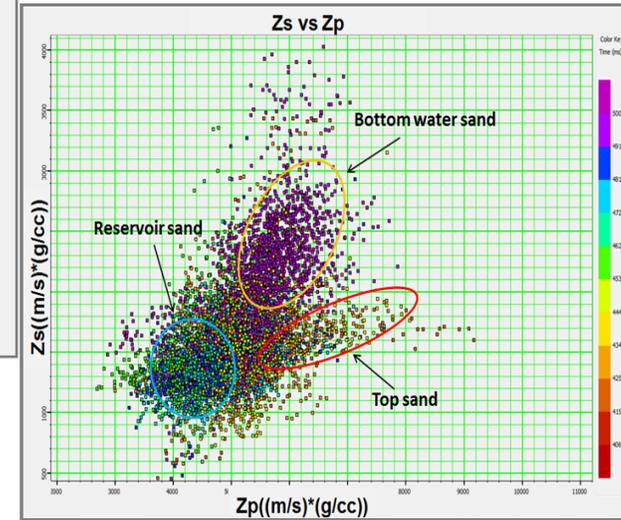
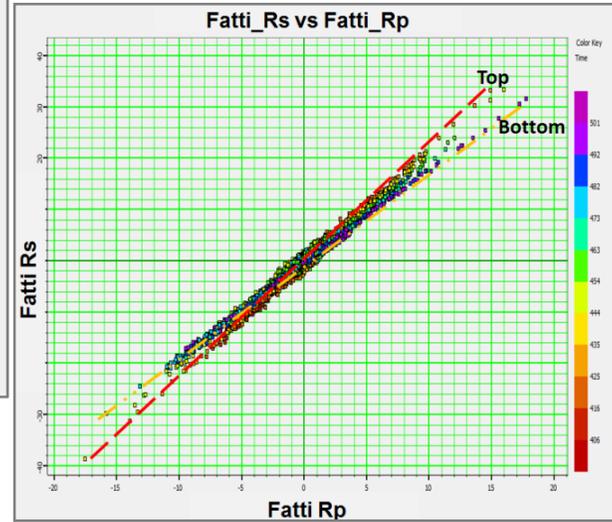
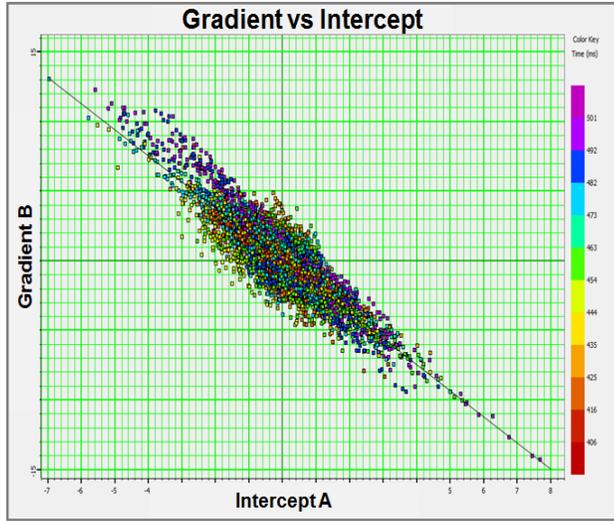
Gradient



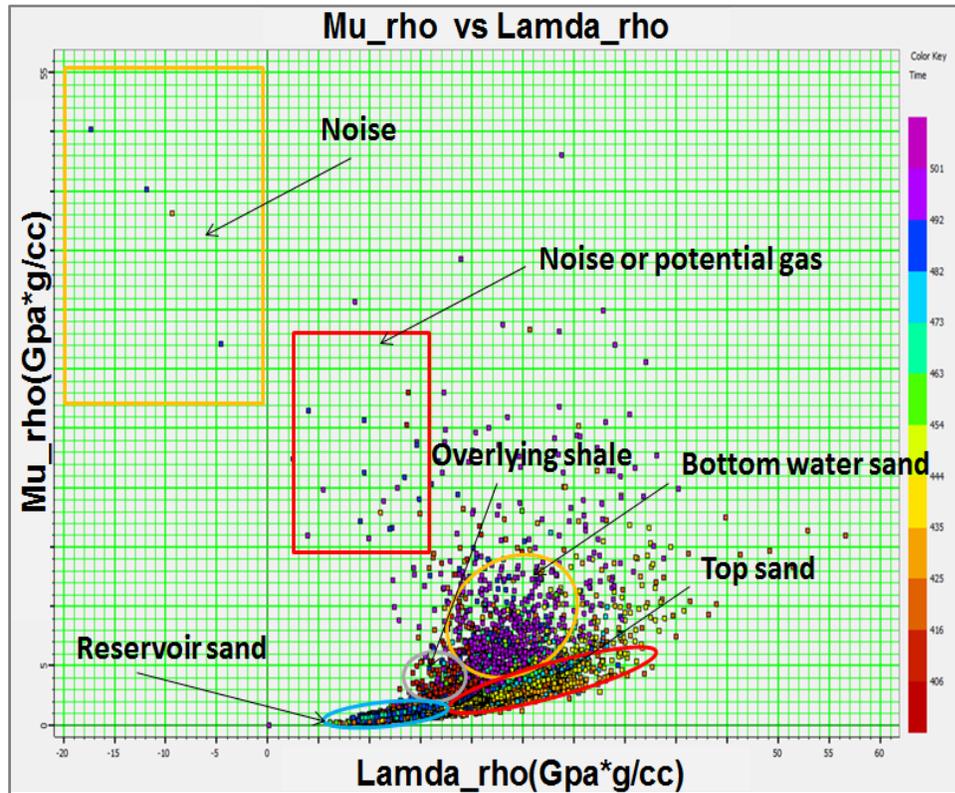
AVO product

Scaled Poisson's ratio change

# AVO attribute crossplots



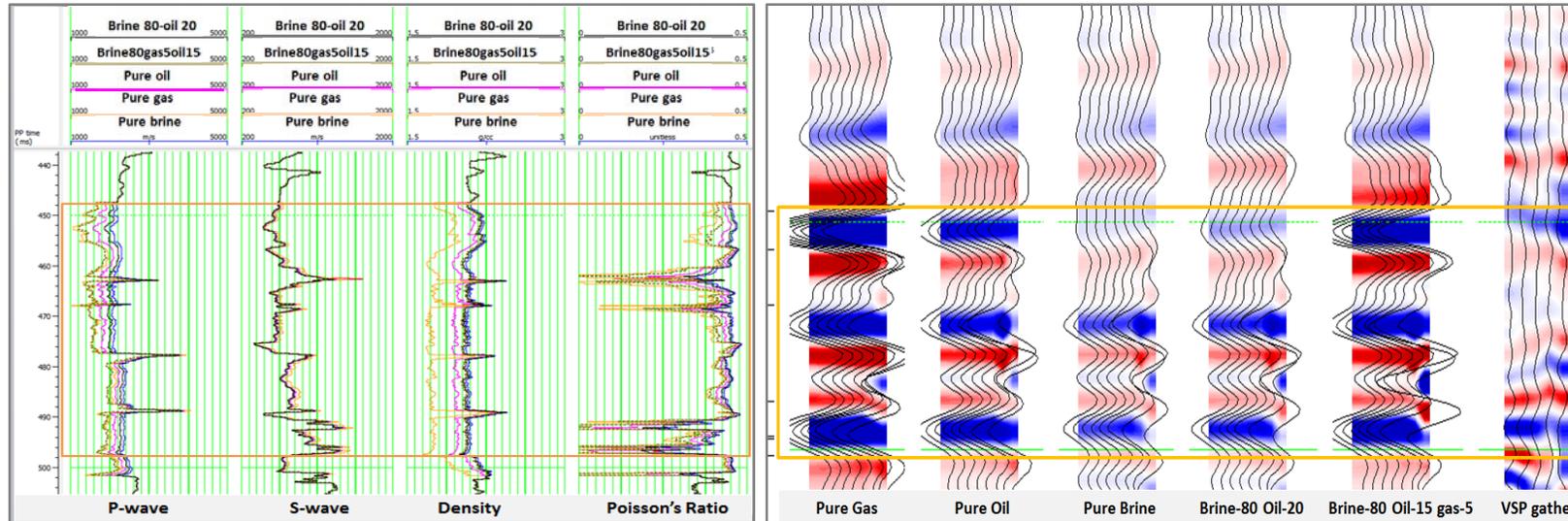
# AVO Lamda-Mu- Rho analysis



- Crossplot minimizes the effects of density
- the  $\lambda$  (incompressibility) is sensitive to pore fluid - an indicator of water vs gas
- the  $\mu$  (rigidity) is sensitive to rock matrix - pure rock fabric or lithology



# AVO modeling and production data

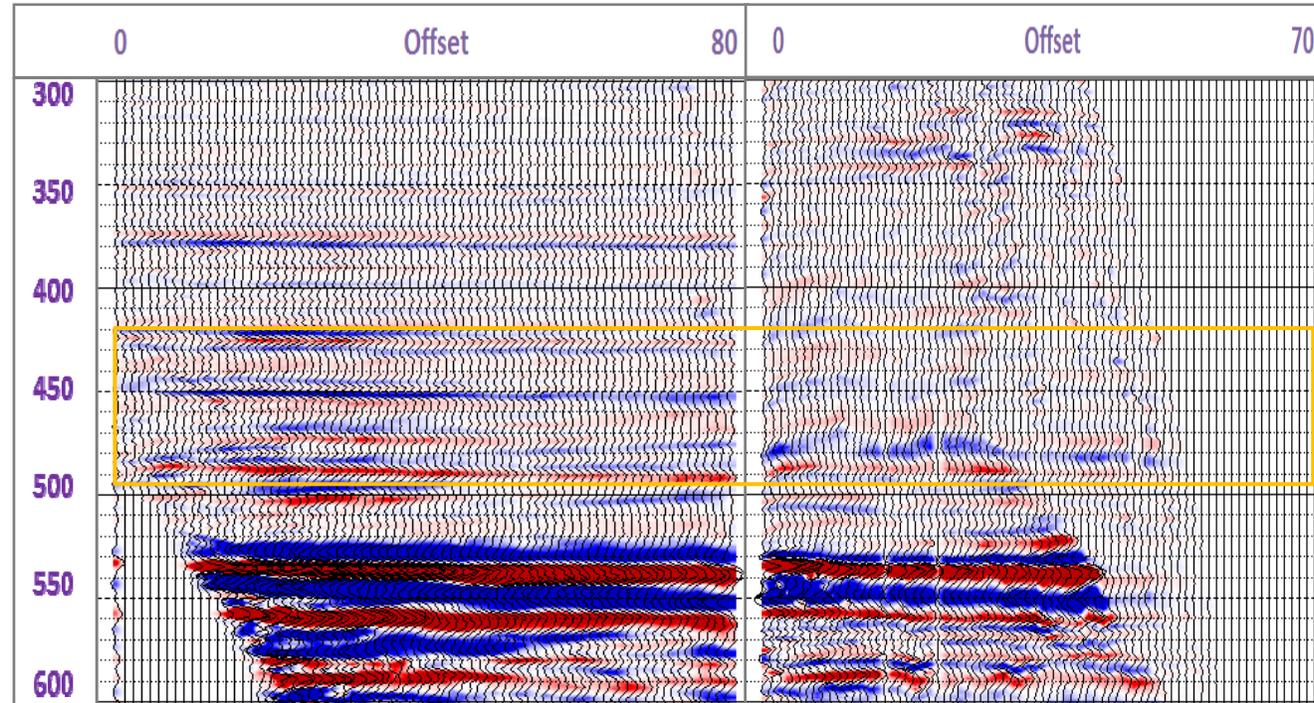


	Gas ( $c^3m^3$ )	Oil( $m^3$ )	Water ( $m^3$ )	Gas%	Oil%	Water%
F12 Mo Prod	0	434	7443	0%	5.5%	94.5%
L12 Mo Prod	8	641	7267	0.1%	8.1%	91.8%
Cumulative Prod	8	1075	14710	0.05%	6.81%	93.14%



UNIVERSITY OF CALGARY

# PP-PS registration

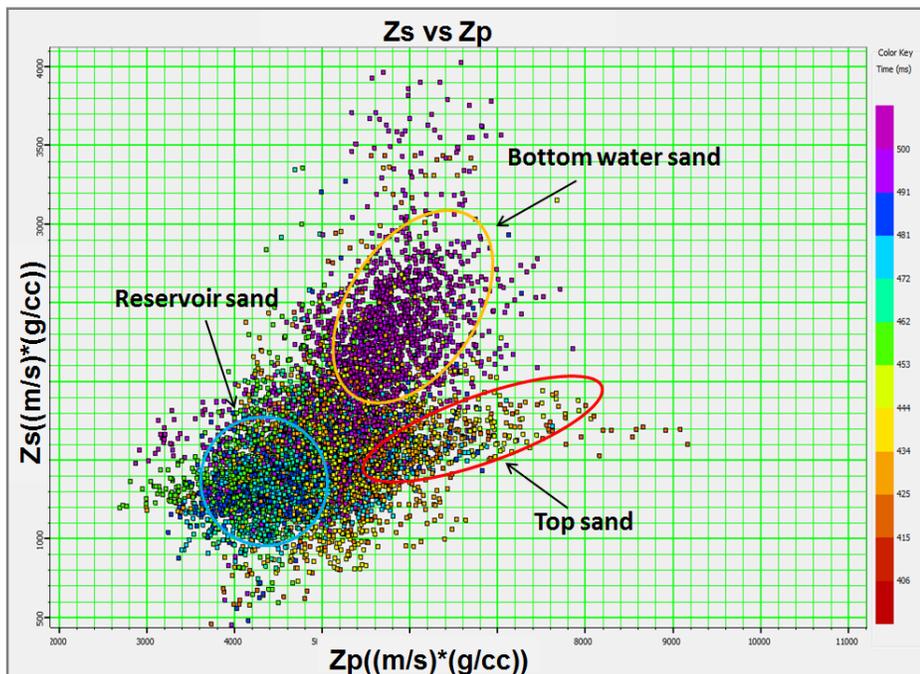


PP image

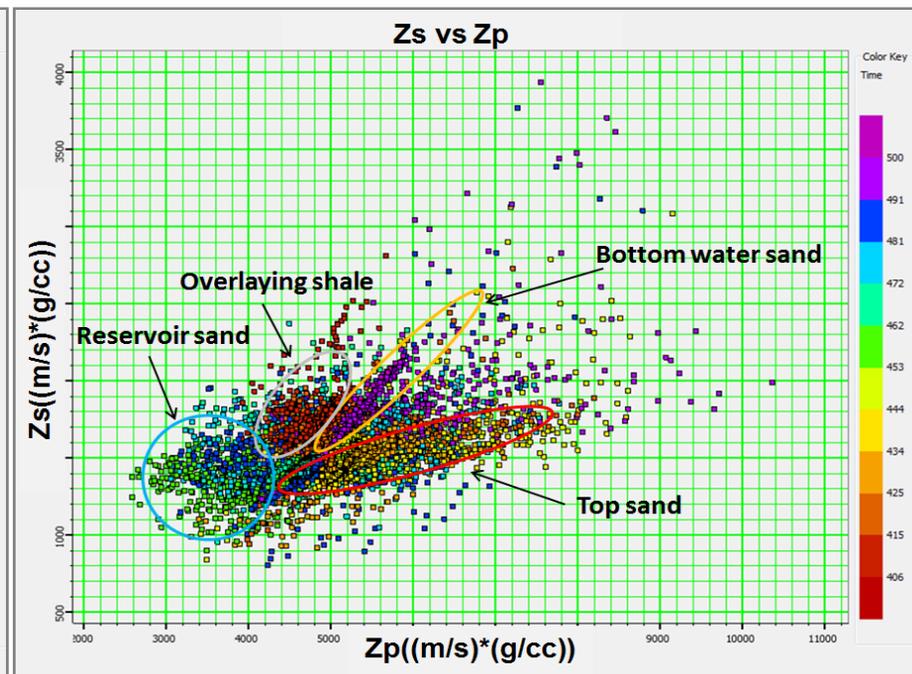
PS image



# Comparison of P-wave and PP-PS joint inversion



P-wave inversion



PP-PS joint inversion



# Summary

---



- ☑ Hydrocarbon signatures may be more visible on VSP than surface seismic data
- ☑ Inverted rock properties and crossplots, AVO Lambda-mu-rho analysis are effective tools to predict lithologies and fluids in the reservoir studied.
- ☑ AVO analysis and modeling show no gas effects in the study interval which was validated by production data.
- ☑ Converted-wave data improve the accuracy of prediction of lithology and fluid discrimination
- ☑ The limitation of S-wave data, the distance of well and VSP borehole as well as absence of S-wave log may degrade the reliability of the detailed interpretations.

# Acknowledgements

---



- **Anonymous company for providing the VSP data**
- **Eric V. Gallant for assistance with data acquisition**
- **Schlumberger(GEDCO) - VISTA processing system**
- **CGG(Hampson-Russell)- inversion/AVO software**
- **CREWES sponsors**
- **NSERC Grant # CRDPJ 379744-08**
- **CREWES professors, staff, and students**

