The Duvernay Formation-the application of structure and simultaneous inversion for reservoir characterization and induced seismicity

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We have a 3-D, 3-C data set; we have mapped structural and stratigraphic features, and calculated key seismic attributes

This approach will be useful in optimizing drilling programs, and identify potential drilling hazards





#### Introduction

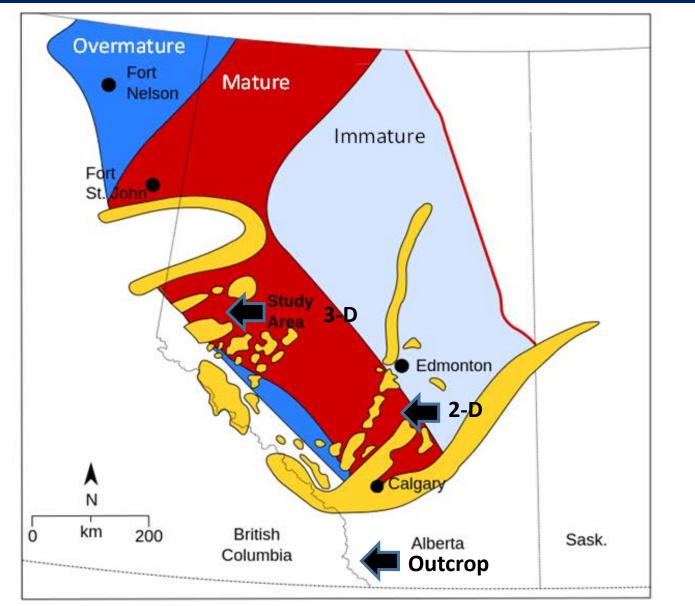
- 1 Overview of Duvernay Geology
  - a. Regional Framework
  - b. Modern Analogue
  - c. modern outcrop
  - c. Core work
  - e. Theoretical Rock properties
- 2 Current development practices
- 3 General workflow
  - a. Structural interpretation
  - b. derivation of rock properties with inversion
- 4 Conclusions and results
  - Implications of reservoir characteristics
- 5 Future Work
  - Implications of reservoir characteristics





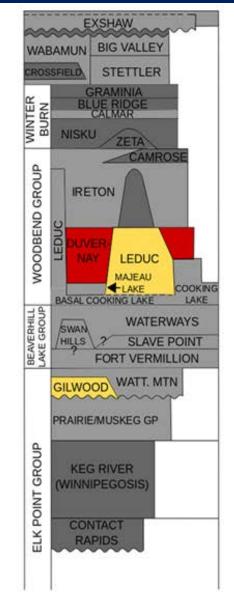


#### 1 a. Duvernay Formation mature oil window



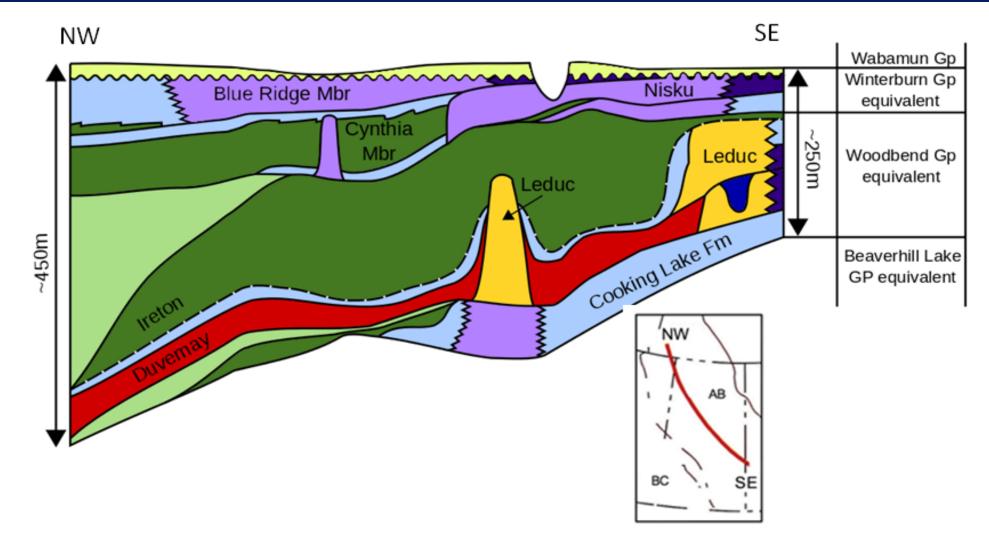
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# 1 a.Devonian Cross Section, the Duvernay shown in red





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# 1 b. Duvernay /Leduc modern analogue





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## 1 b. Duvernay /Leduc modern analogue





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# 1 c. Duvernay Outcrop

- decomposition



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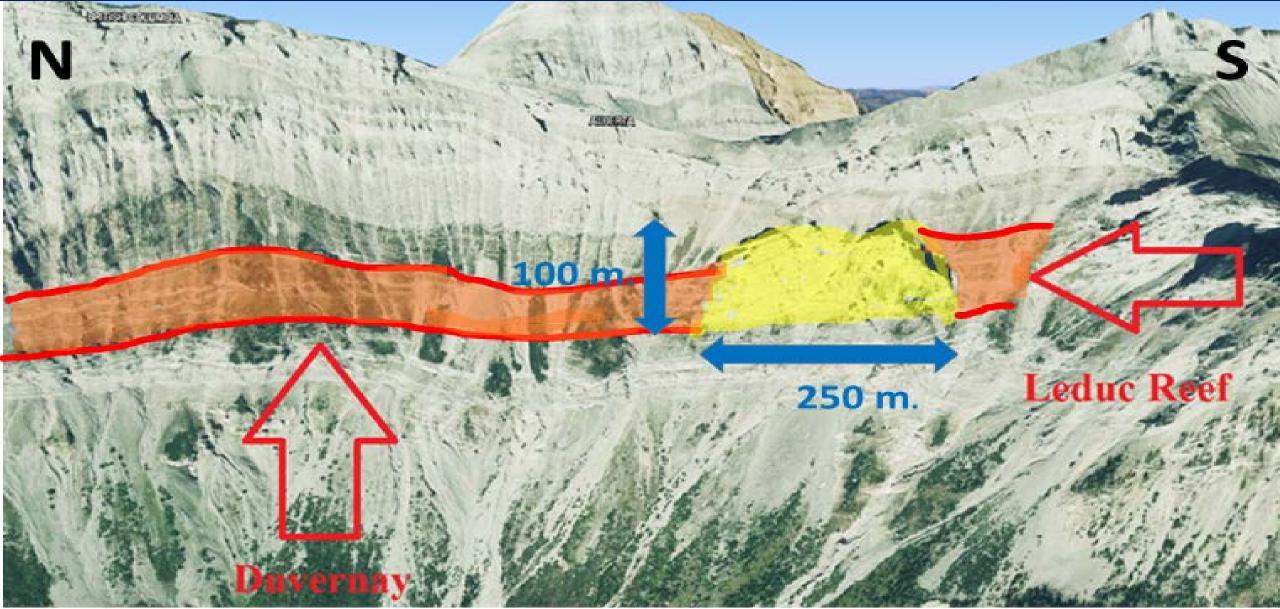
ALC: NOT



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Leduc Reel

# 1 c. Duvernay outcrop

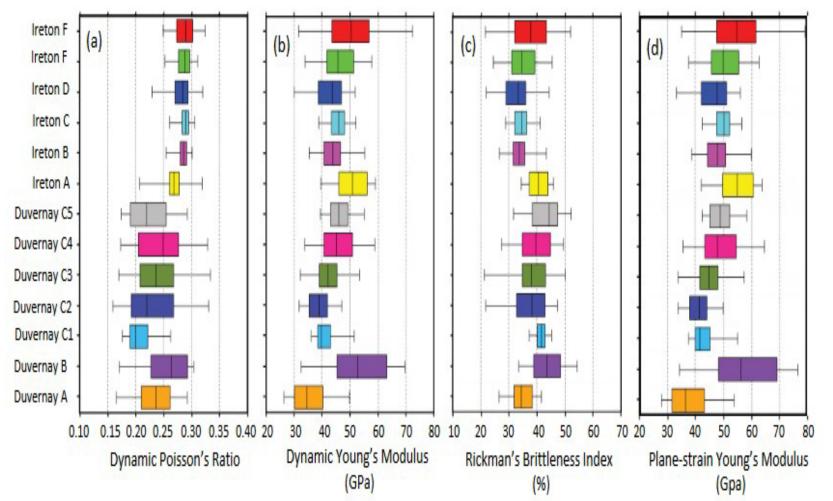




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# 1 d. Core work: Kaybob area rock properties, Duvernay



Amy D. Fox, Mehrdad Soltanzadeh Canadian Discovery Ltd. Figure 1. Mechanical properties calculated based on sonic logs for 26 wells for the Duvernay and Ireton formations: (a) dynamic Poisson's ratio, (b) dynamic Young's Modulus, (c) Rickman's brittleness Index, and (d) plane-strain Young's modulus.

# 

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# 1 d. Youngs Modulus Posson / Ratio Calculation from Vp, Vs, $\rho$

Related equations are defined as follows:

Possion's Ratio: 
$$PR = \frac{0.5 * \left(\frac{Vp}{Vs}\right)^2 - 1}{\left(\frac{Vp}{Vs}\right)^2 - 1}$$
; Closure Stress Ratio:  $CSR = \frac{PR}{1 - PR}$ 

Young's Modulus: 
$$\mathbf{E} = \frac{2 * Z_s^2 * (1 + PR)}{Density}; \quad \rho \mathbf{E} = 2 * Z_s^2 * (1 + PR)$$

$$Brittleness: BRI = 100 * \left( w * \frac{(PR_{max} - PR)}{PR_{max} - PR_{min}} + (1 - w) * \frac{(E - E_{min})}{E_{max} - E_{min}} \right)$$

Brinell Hardness Number : BHN = 75.156 \* E + 18.21

The default impedance unit used in the equation is (m/s)\*(kg/m3); Default velocity unit is (m/s); Default density unit is (kg/m3). Input values in other units will be converted automatically.

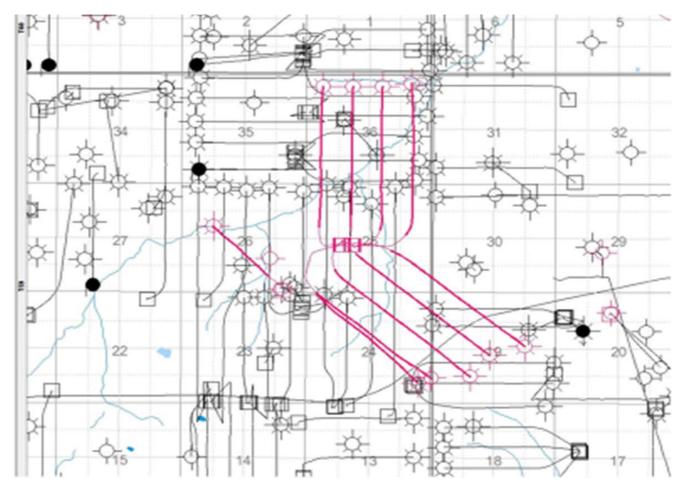


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#### 2. Current Development practices

**Duvernay Development practices** 



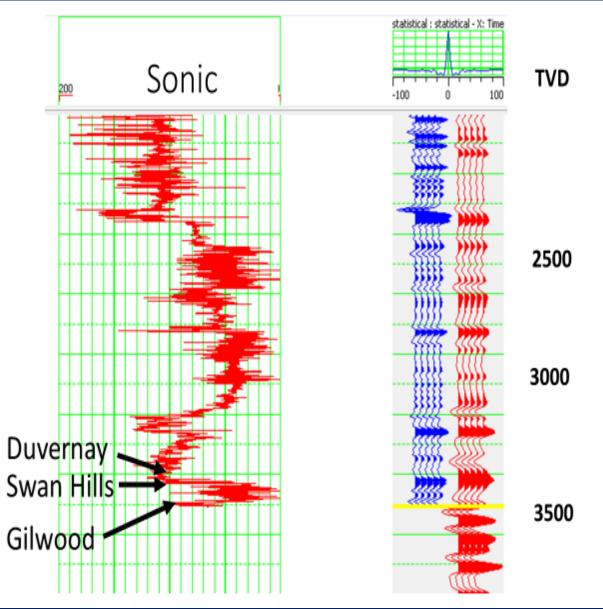


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#### Synthetic seismogram tie



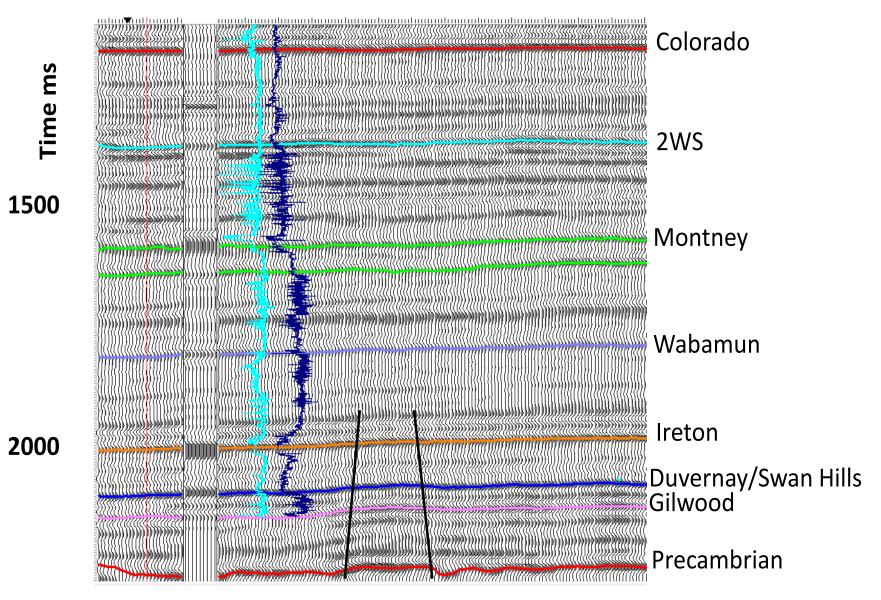


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#### 3 a. Large scale seismic data with sonic tie



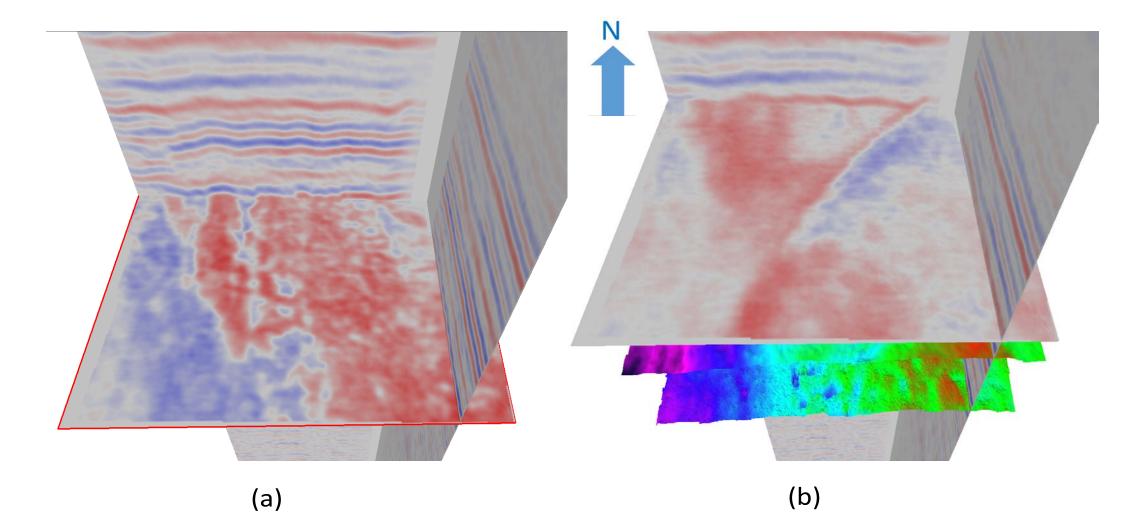


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# Chair plot through Precambrian and Swan Hills

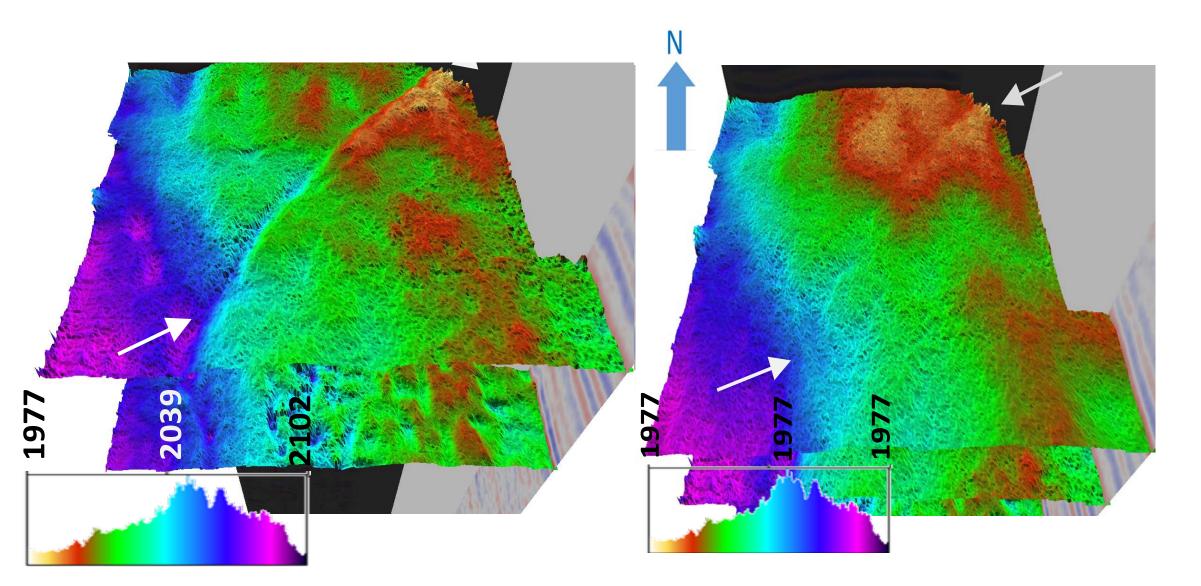




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#### Swan Hills and Ireton Structure

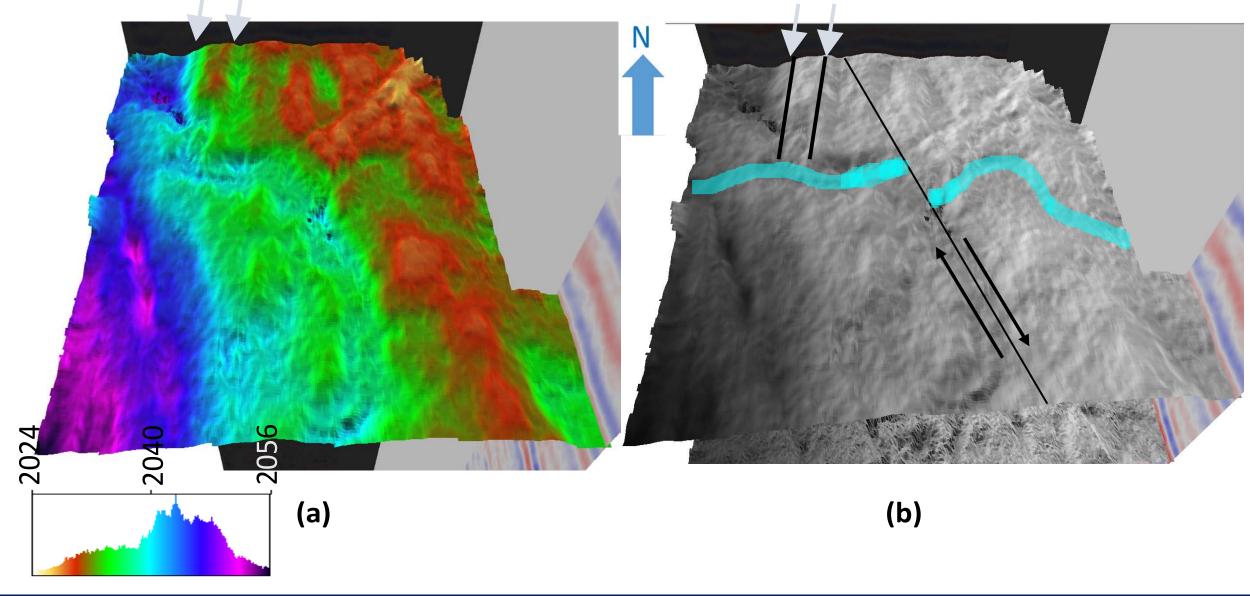




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# Fault – Time structure, Gilwood



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# 3 b.General inversion workflow

#### Elastic impedance inversion



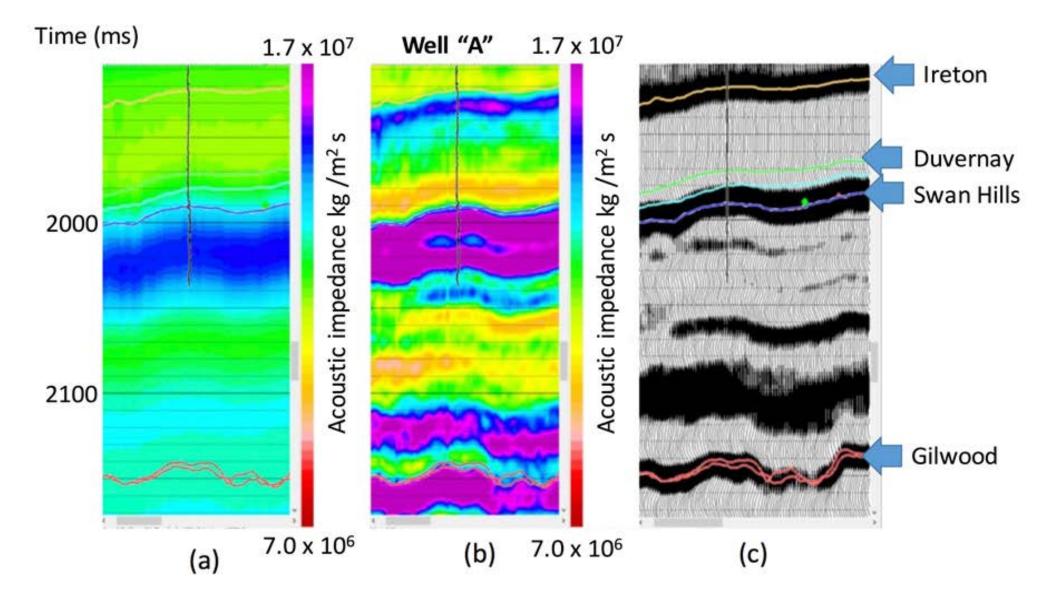
(2) Build model from picks and impedances (1) Optimally process the seismic data  $M = EI(\theta) = V_p^a V_s^b \rho^c$  $(\theta) = W(\theta) * R_{FI}(\theta)$ In elastic impedance (3) Iteratively update inversion the seismic, model until output  $EI(\theta) = V_P^a V_S^b \rho^c$ model and output are synthetic matches as shown here. original seismic data.



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# 3 b. Model / post stack inversion / Input data

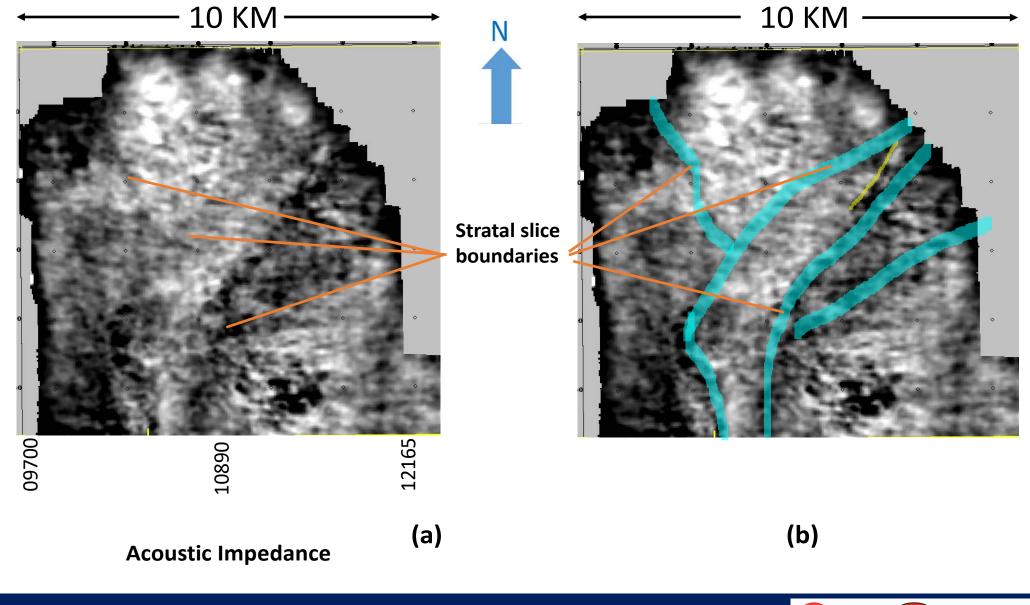




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#### Stratal slice, post stack inversion

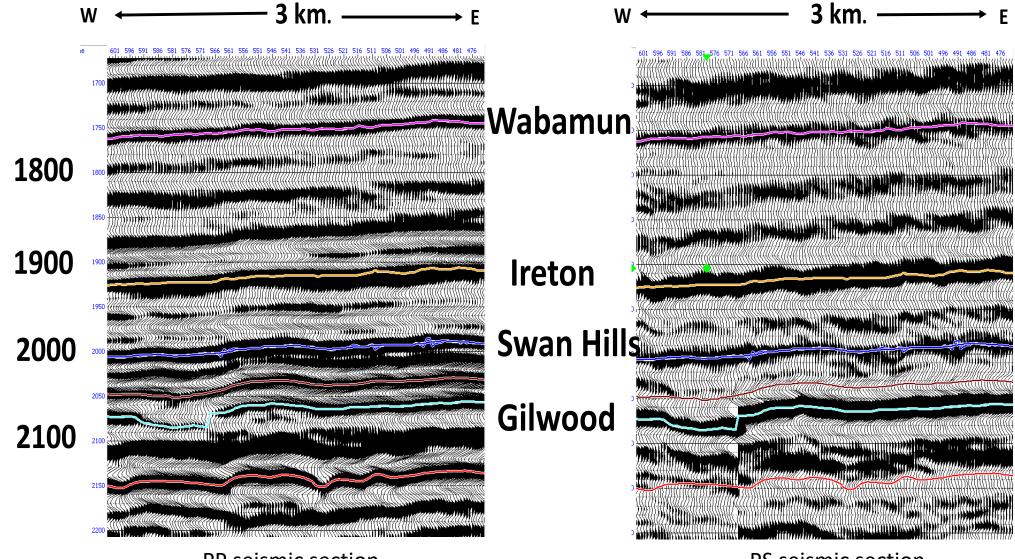


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#### PP and PS data regristration



PP seismic section

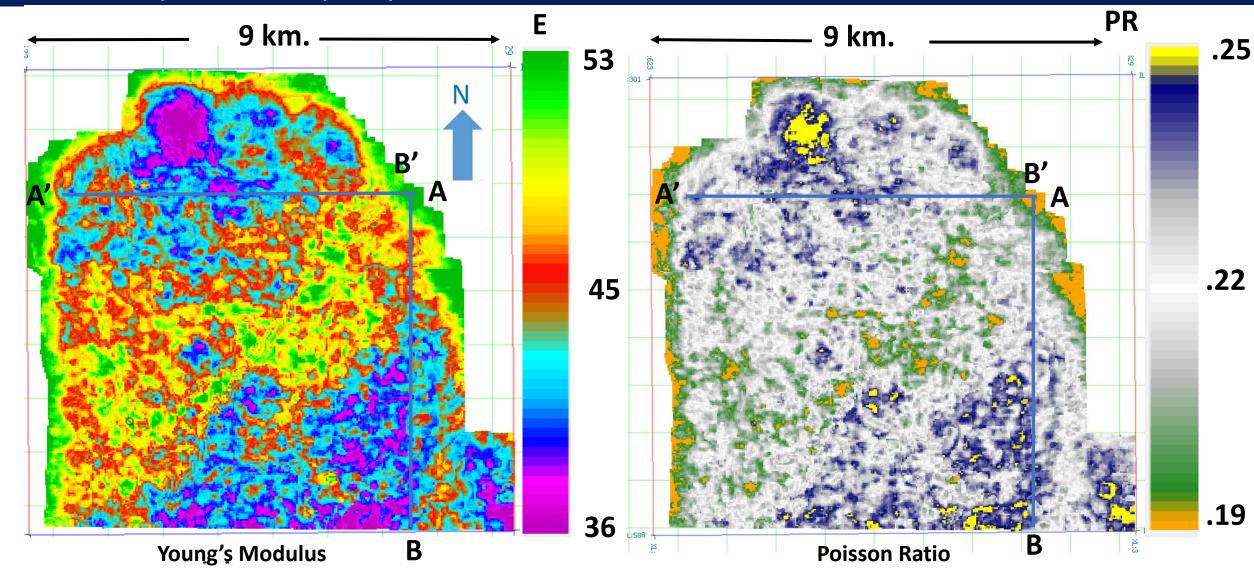
PS seismic section



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#### Duvernay elastic properties





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#### E and PR, derived and theoretical values

x 10<sup>4</sup> NIA – spheres 100% Limestone Quartz-Clay Quartz-Limestone  $\phi = 10\%$ Limestone-Clay ш 50 Young's Modulus  $\phi = 20\%$ 40 Ø**≂ 30%**  $\phi = 40\%$ 30 100% Clay Constant bulk modulus 20 Increasing bulk modulus 0.35 0.45 0 0.05 0.15 0.25 0.3 0.4 0.5 0.1 0.2 .2 .3 .1 Poisson's Ratio Poisson's Ratio

Cho et al. 2005

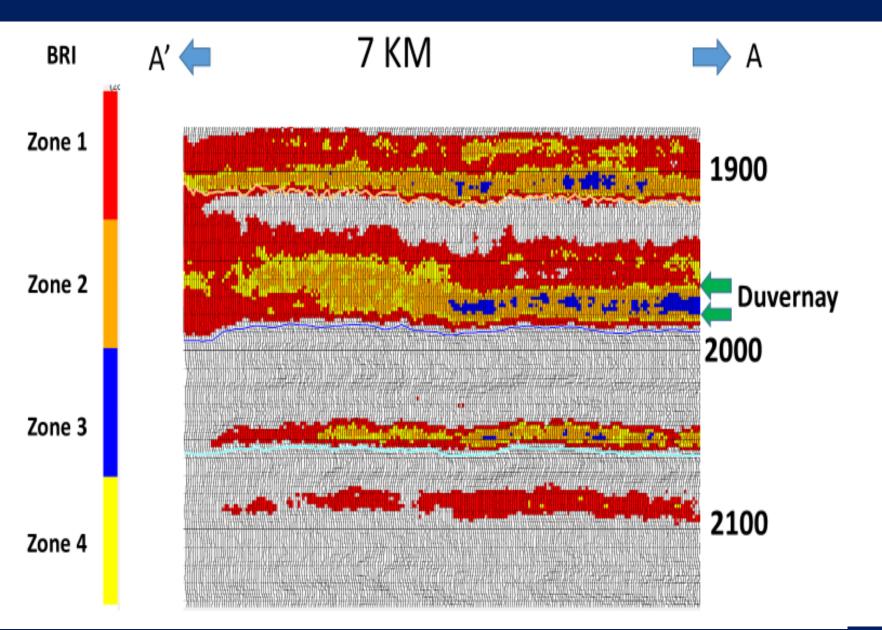
100% Quartz



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#### BRI values

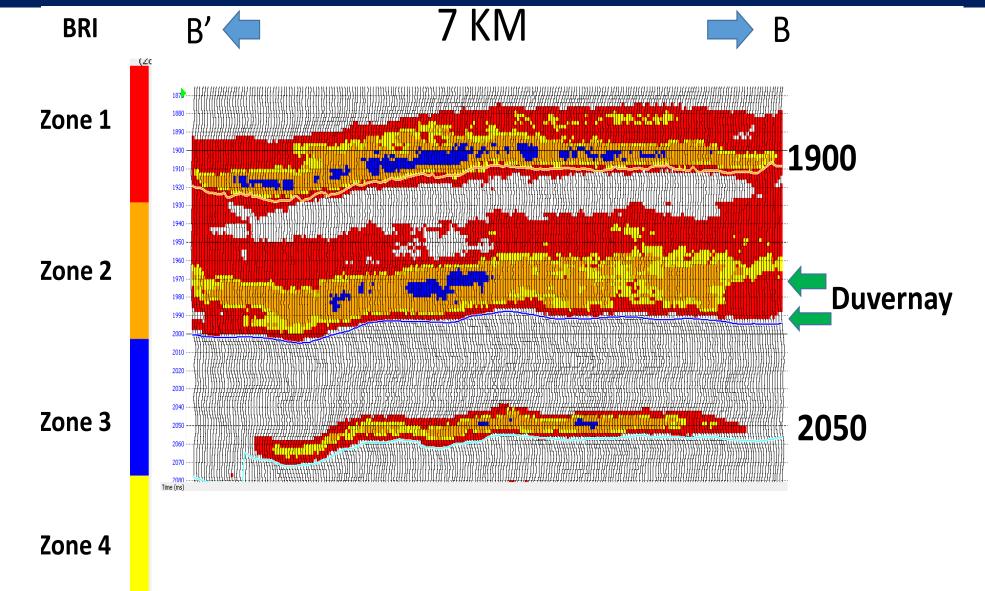




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#### **BRI** values

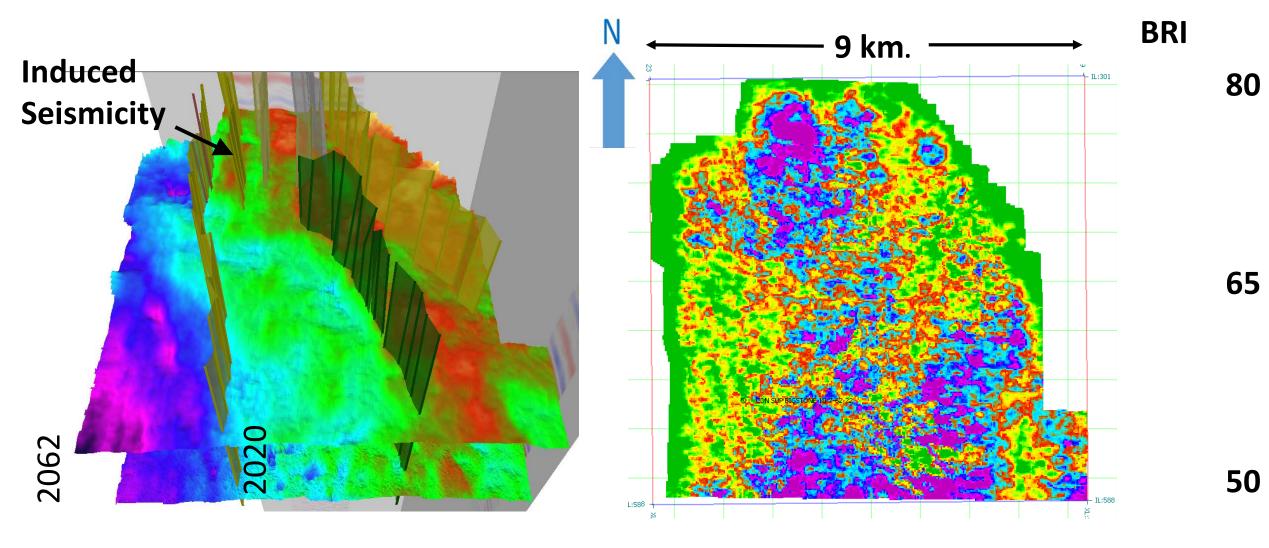




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# Gilwood Structure and Duvernay formation BRI



(a)



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(b)

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# 4. Conclusions

- Reservoir attributes can readily be extracted from prestack data
- Wells can be better positioned based on rock parameters and structure
- Reservoir characterization may be able to explain the variable fracture patters and productivity of horizontal wells
- Fault mapping can determine the potential of induced seismicity, and may explain induced earthquakes occur





# 5. Future work

- Calibrate microseismic recorded data with the PP PS mapping and reservoir characterization
- Determine which faults are responsible for induced seismicity, and identify potential geohazards.
- Analyze the AVAz response of this data, The induced Duvernay microseismic events are not aligning to the assumed regional gradient, preliminary results indicate the trends are off by 15 degrees.



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#### Software

#### • TECHNICAL SOFTWARE USED

- Geoview (HRS), pre and poststack inversion
- Geoscout, Well grid and culture data base, LAS files, production and perforation information
- Seisware, Conventional seismic interpretation
- Vista, prestack data preparation.





- Dr. Brian Russell, technical advice and consultations
- Staff and students in CREWES, MIC
- Arcus Seismic Solutions for the use of the 3-D, 3-C data.
- Divestco for providing Digital well logs.
- We thank the sponsors of CREWES and the Microseismic Industry Consortium for continued support. This work was funded by CREWES and MIC industrial sponsors and NSERC (Natural Science and Engineering Research Council of Canada) through grants CRDPJ 461179-13, CRDPJ 474748-14, IRCPJ/485692-2014, and IRCSA 485691





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# •Questions?



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