

DAS modeling for hydraulic fracture and caprock monitoring

Matt Eaid* and Kris Innanen

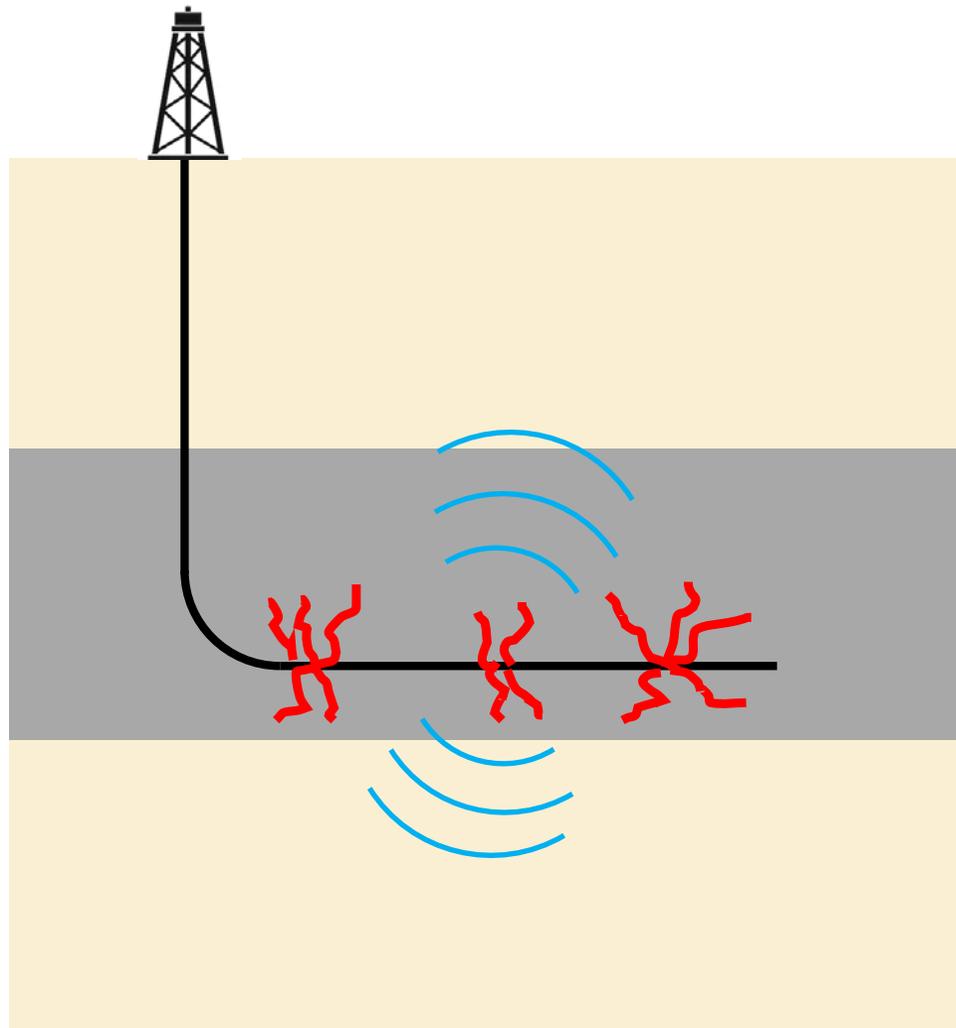
CREWES Sponsors Meeting, Banff,
December 10th, 2019



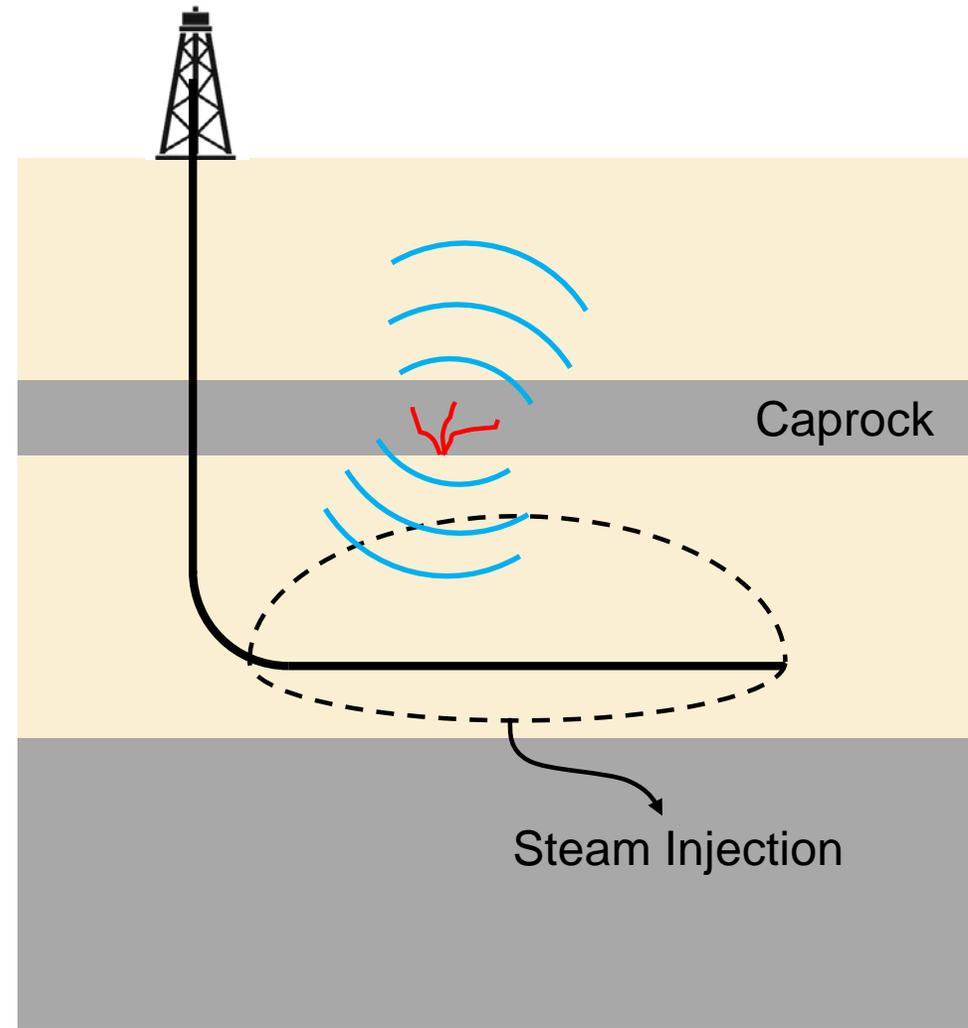
**NSERC
CRSNG**



UNIVERSITY OF CALGARY
FACULTY OF SCIENCE
Department of Geoscience



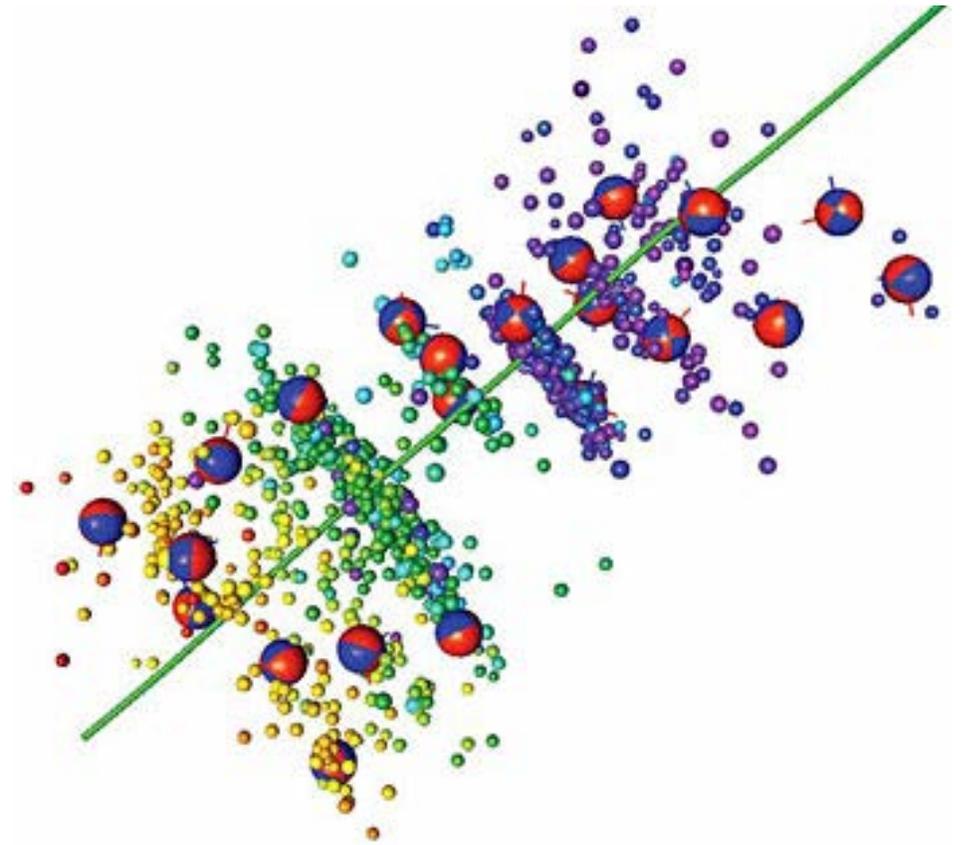
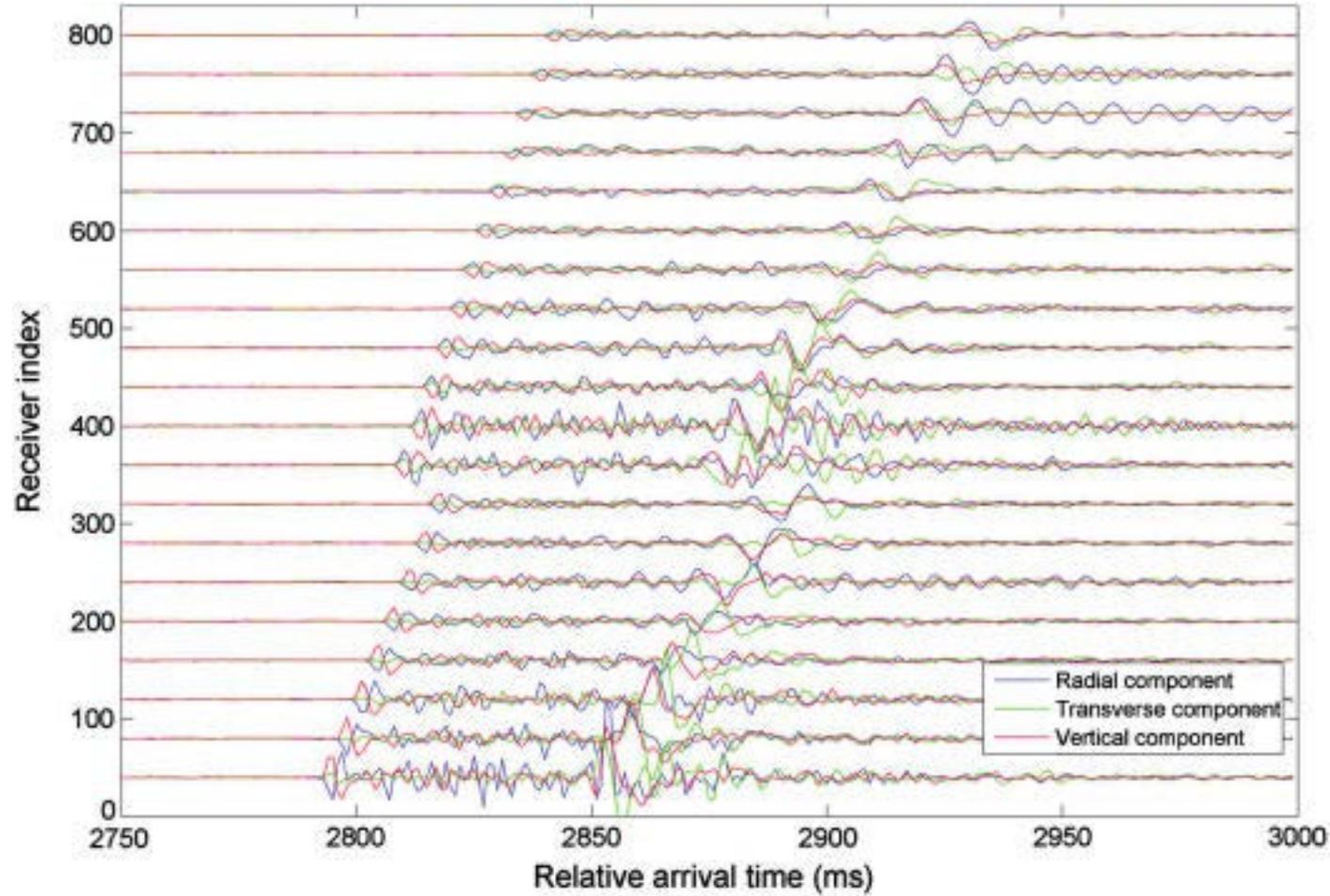
Hydraulic Fracturing



Cyclic steam stimulation

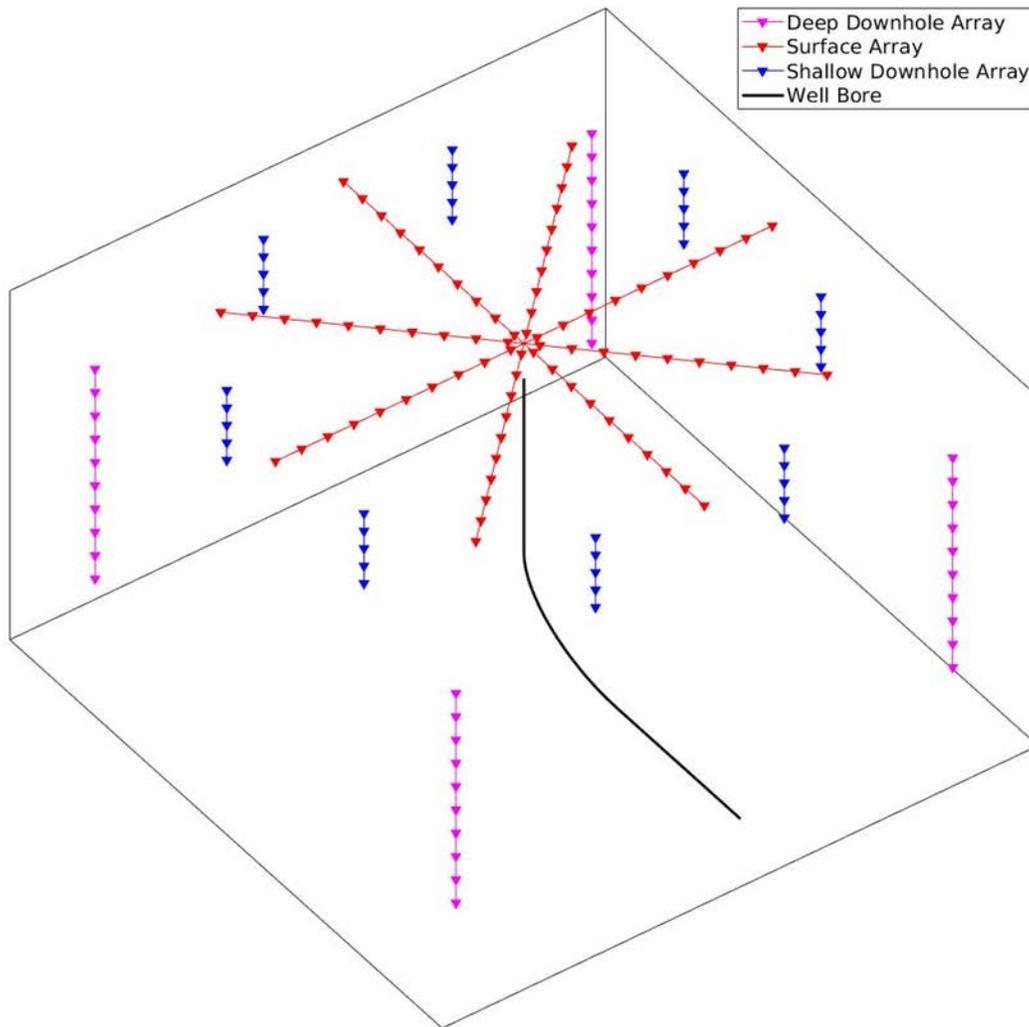


Microseismic data





Microseismic Monitoring Array Types: Geophones



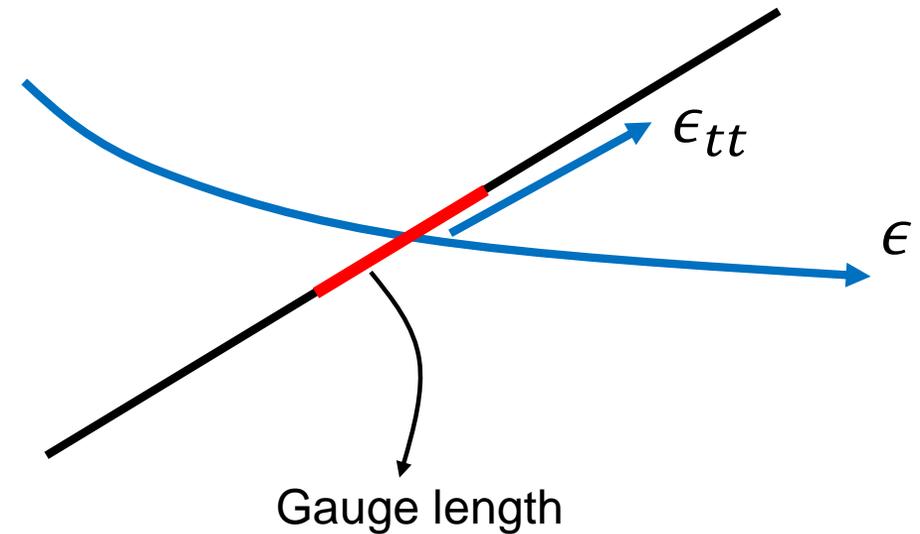
Conventionally, microseismic data has been recorded with networks of 1C and 3C geophones in three main array types:

1. Surface Arrays
2. Shallow Downhole Arrays
3. Deep Downhole arrays

Desirable geometries have the properties:

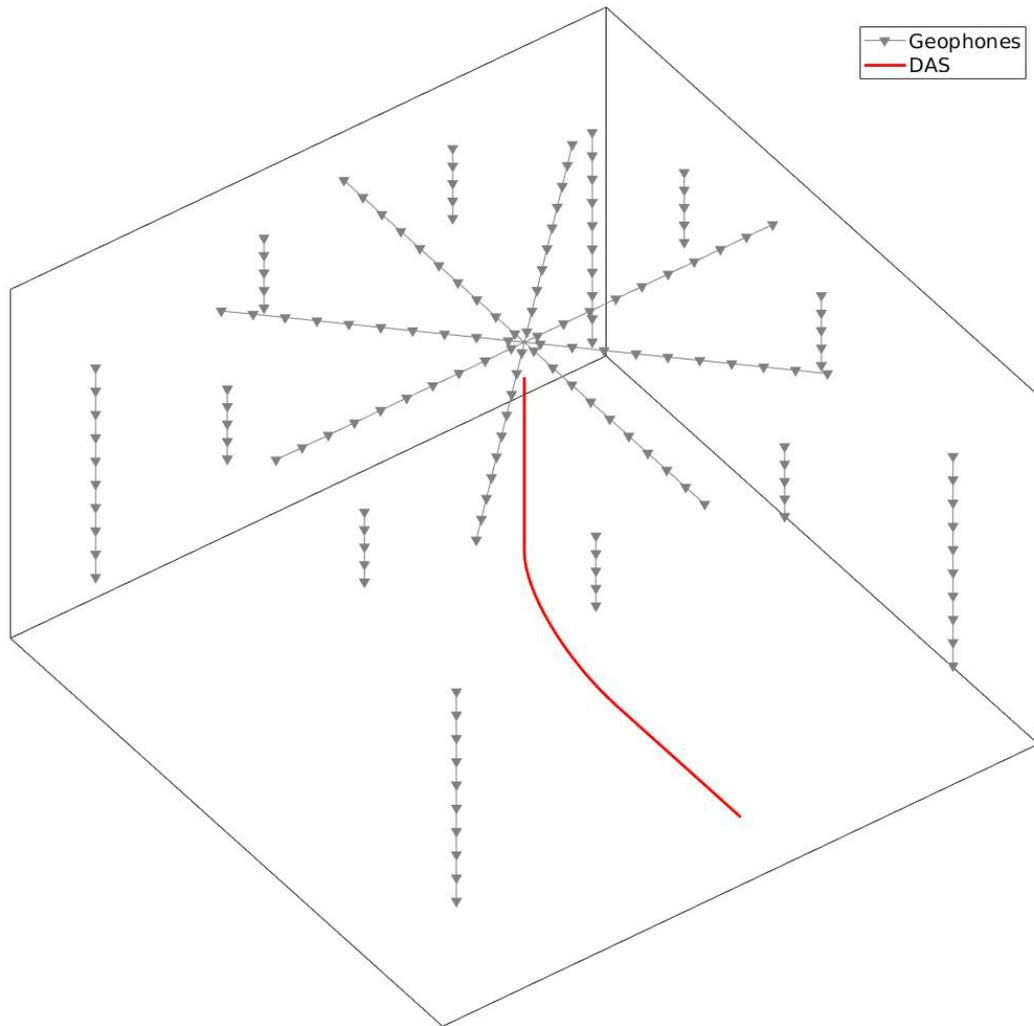
- Close proximity to treatment well
- Sample sufficiently large aperture
- Ideally cover a range of depth intervals
- Cost-effective

- DAS uses an optical fibre to make measurements of seismic strain
- Fibres are only sensitive to strain along the tangent of the fibre
- Measurements are spatially averaged over the gauge length to improve SNR





Microseismic Monitoring Array Types: DAS



Advantages

- Non-invasive: can be placed in frack well or nearby monitoring well, allowing for dual purpose wells.
- Dense spatial sampling ~ 3ft sample interval.
- Large aperture recording with 1000's of receivers.
- Ultra low frequency (near-DC) strain measurements.

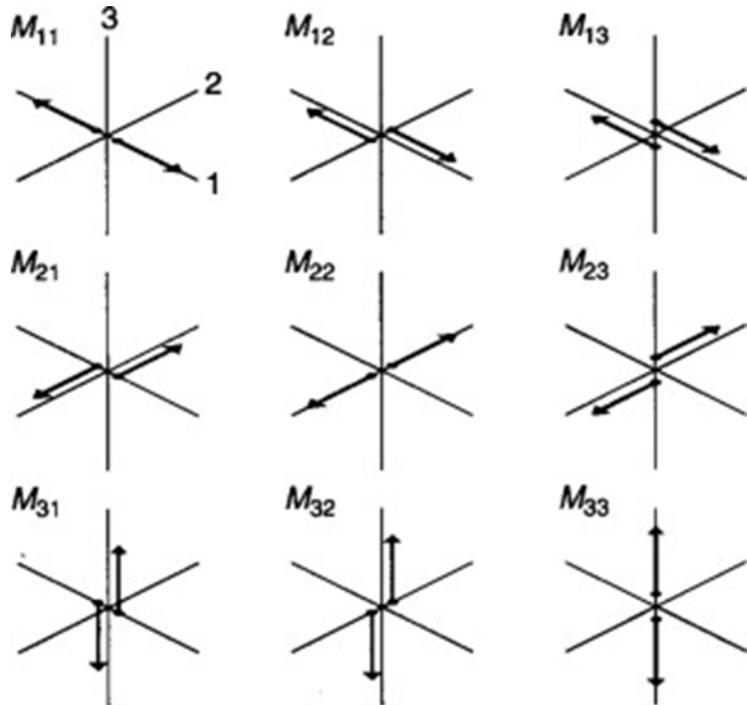
Disadvantages

- Low signal-to-noise ratio, and generally lower sensitivity.
- Single component recording.
- Expensive to deploy



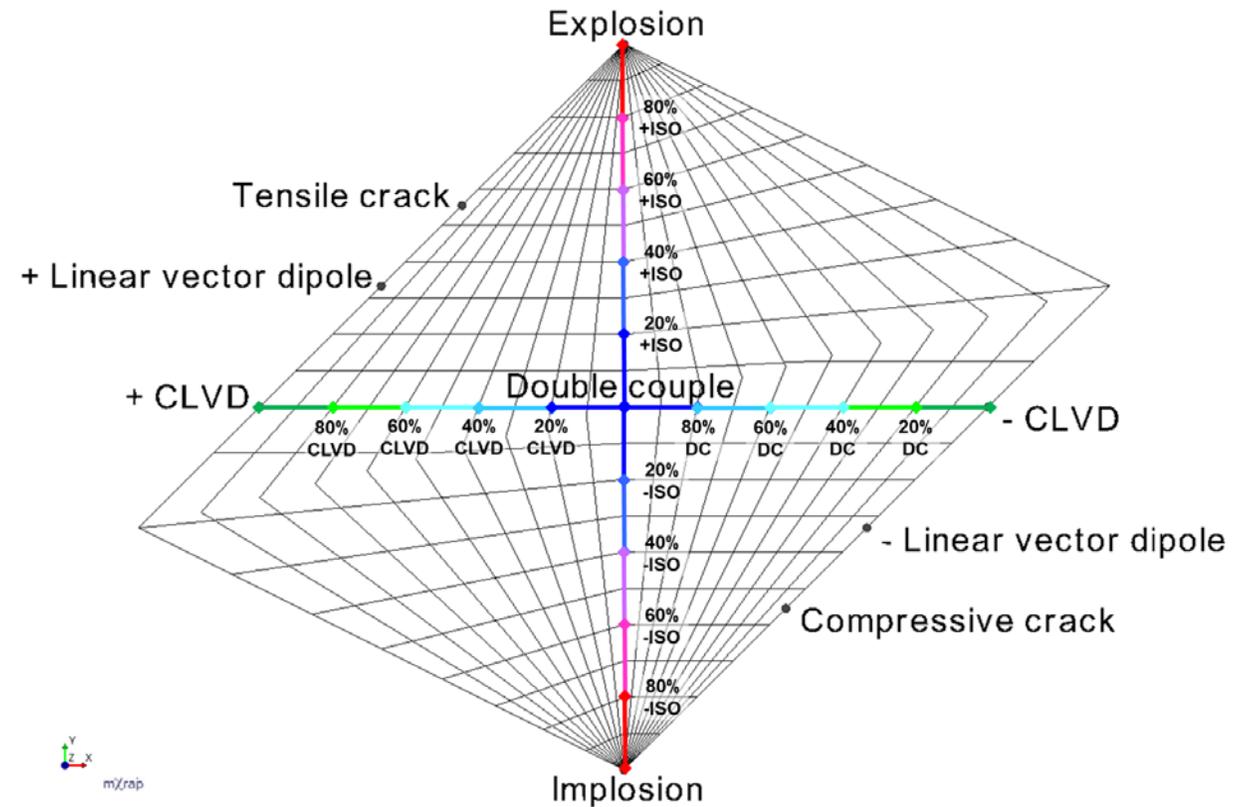
Moment Tensor Sources

Moment tensors provide a mathematical representation of the slip on a fault (fracture) during an earthquake (hydraulic fracture).



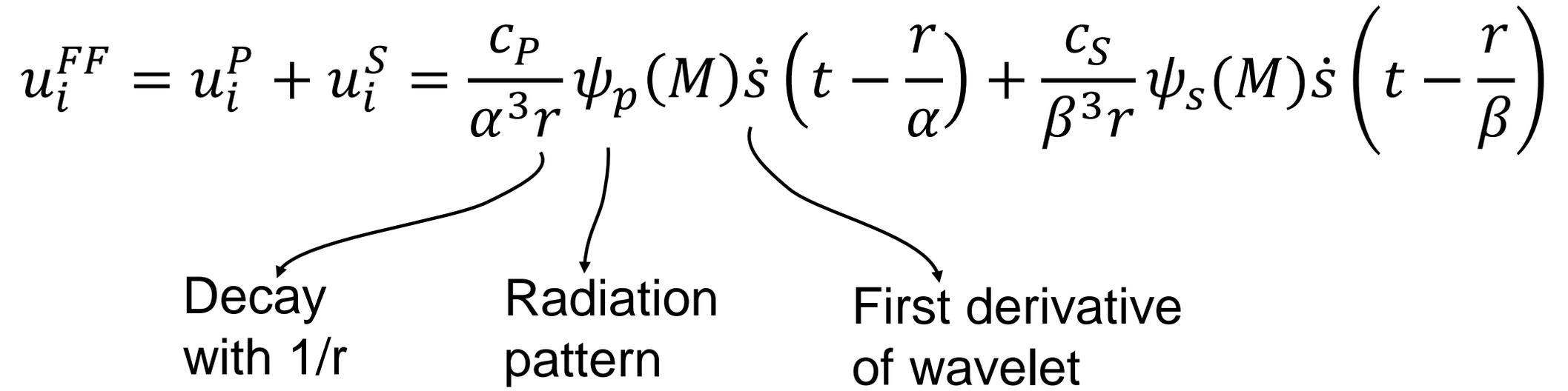
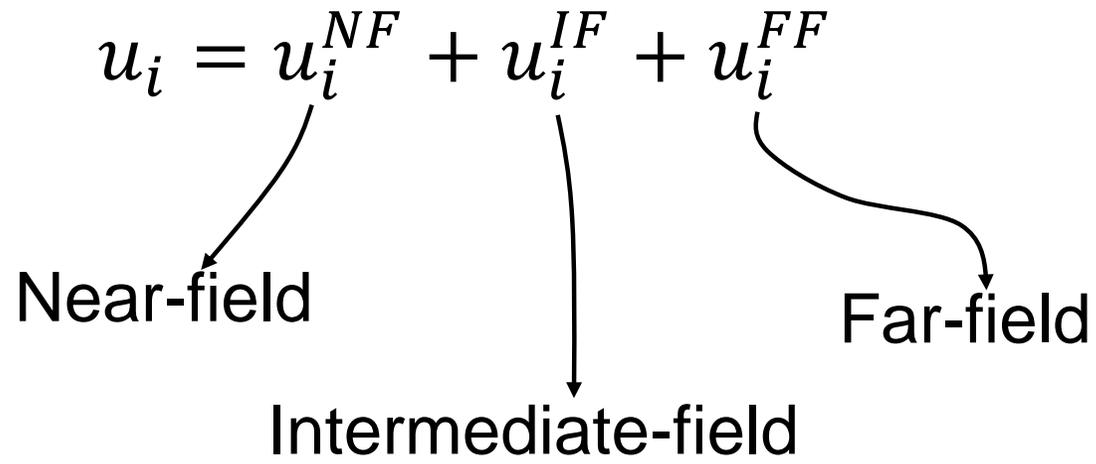
$$M = \begin{bmatrix} M_{11} & M_{12} & M_{13} \\ M_{21} & M_{22} & M_{23} \\ M_{31} & M_{32} & M_{33} \end{bmatrix}$$

$$M = M_{ISO} + M_{DC} + M_{CLVD}$$





Modeling displacement from moment tensor sources





$$\epsilon_{ij}^{FF} = \epsilon_{ij}^P + \epsilon_{ij}^S = \frac{1}{2} \left(\frac{\partial u_i^P}{\partial x_j} + \frac{\partial u_j^P}{\partial x_i} \right) + \frac{1}{2} \left(\frac{\partial u_i^S}{\partial x_j} + \frac{\partial u_j^S}{\partial x_i} \right)$$

**P-wave strain** **S-wave strain**



Analytic displacement:

$$u_i^{FF} = u_i^P + u_i^S = \frac{c_P^u}{\alpha^3 r} \psi_p(M) \dot{s} \left(t - \frac{r}{\alpha} \right) + \frac{c_S^u}{\beta^3 r} \psi_s(M) \dot{s} \left(t - \frac{r}{\beta} \right)$$

Analytic strain:

$$\epsilon_{ij}^{FF} = \epsilon_{ij}^P + \epsilon_{ij}^S = \frac{c_P^\epsilon}{\alpha^4 r} \psi_p'(M) \ddot{s} \left(t - \frac{r}{\alpha} \right) + \frac{c_S^\epsilon}{\beta^4 r} \psi_s'(M) \ddot{s} \left(t - \frac{r}{\beta} \right)$$



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Analytic displacement:

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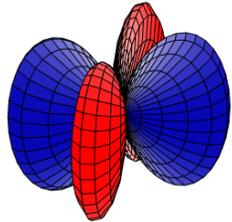
Analytic strain:

$$\epsilon_{ij}^{FF} = \epsilon_{ij}^P + \epsilon_{ij}^S = \frac{c_P^\epsilon}{\alpha^4 r} \psi'_p(M) \ddot{s} \left(t - \frac{r}{\alpha} \right) + \frac{c_S^\epsilon}{\beta^4 r} \psi'_s(M) \ddot{s} \left(t - \frac{r}{\beta} \right)$$

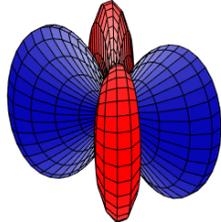


P-strain

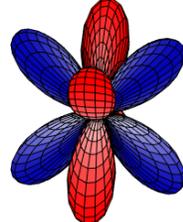
ϵ_{xx}



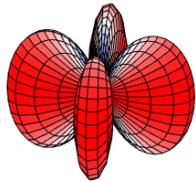
ϵ_{yy}



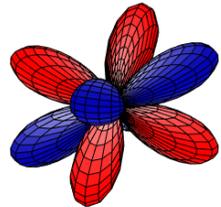
ϵ_{zz}



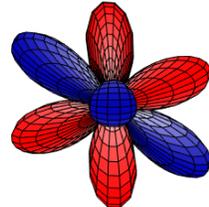
ϵ_{xy}



ϵ_{xz}

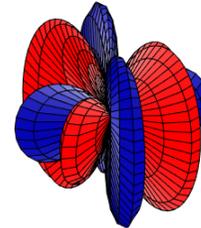


ϵ_{yz}

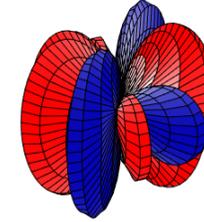


S-strain

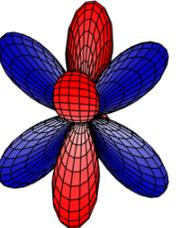
ϵ_{xx}



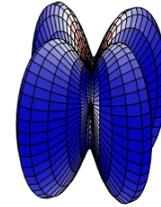
ϵ_{yy}



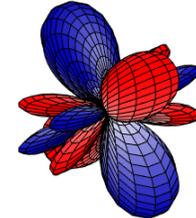
ϵ_{zz}



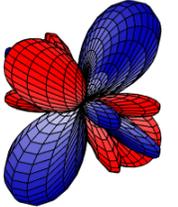
ϵ_{xy}



ϵ_{xz}



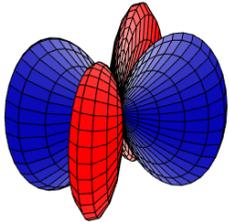
ϵ_{yz}





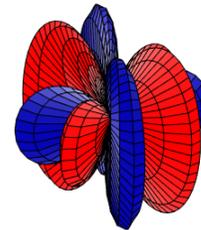
P-strain

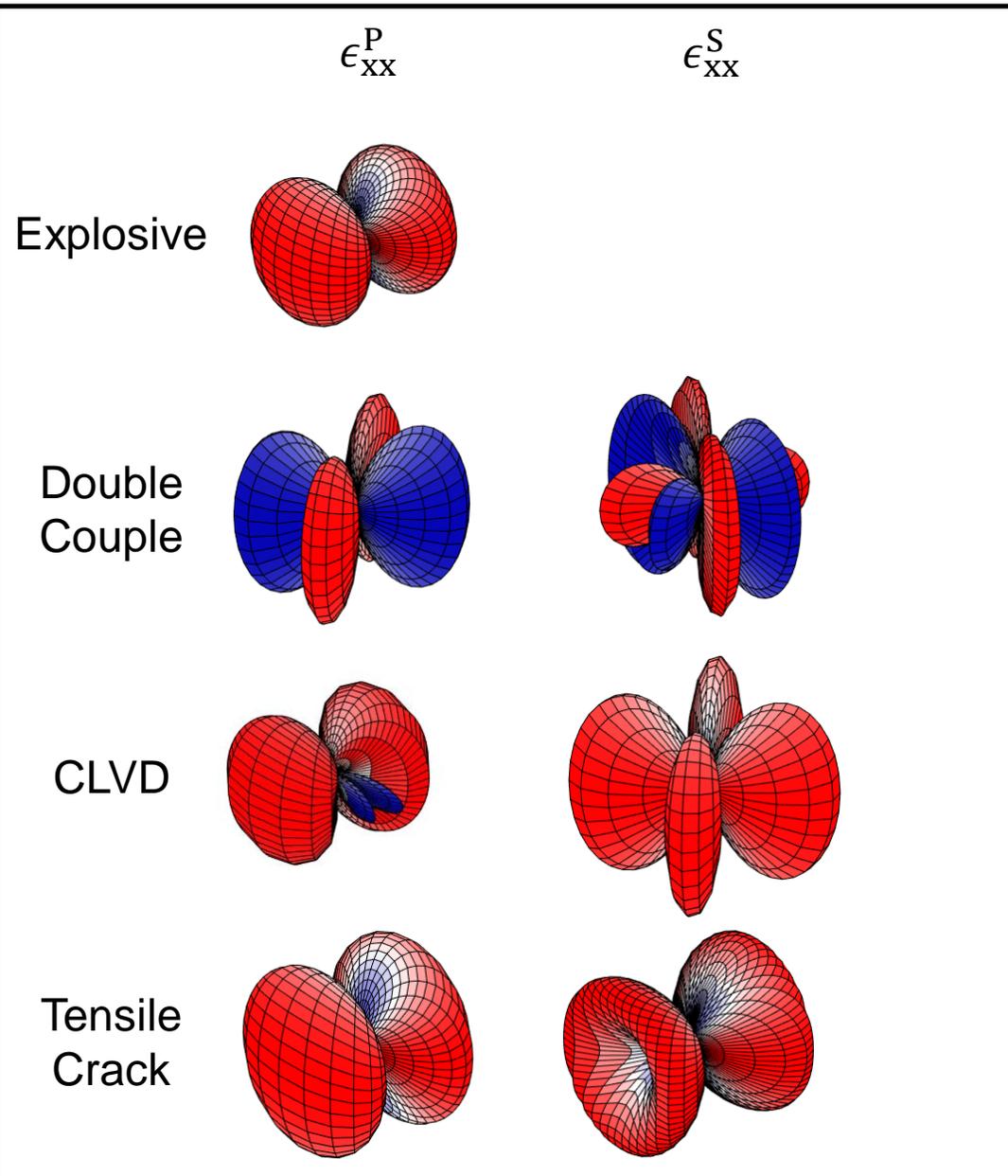
ϵ_{xx}



S-strain

ϵ_{xx}

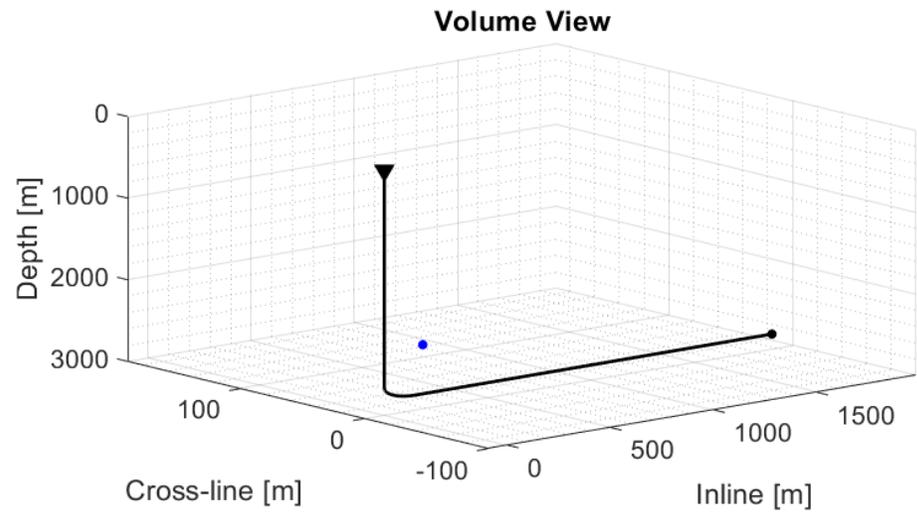
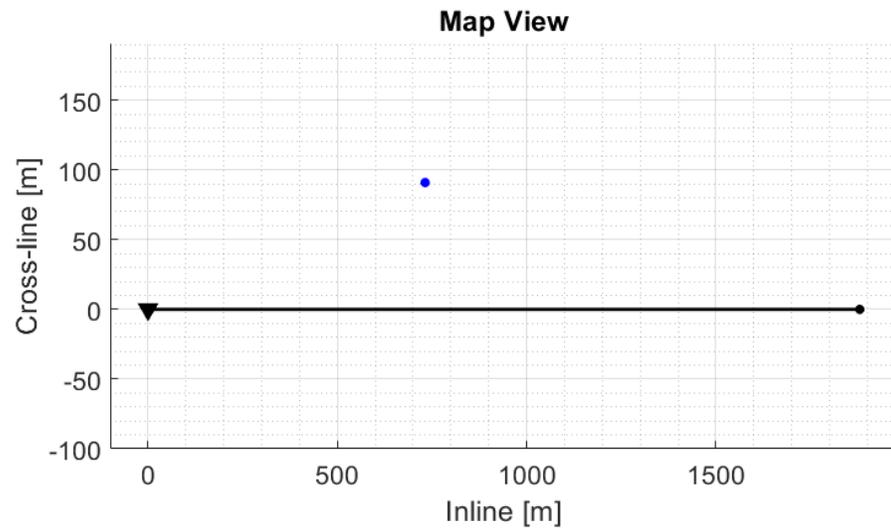
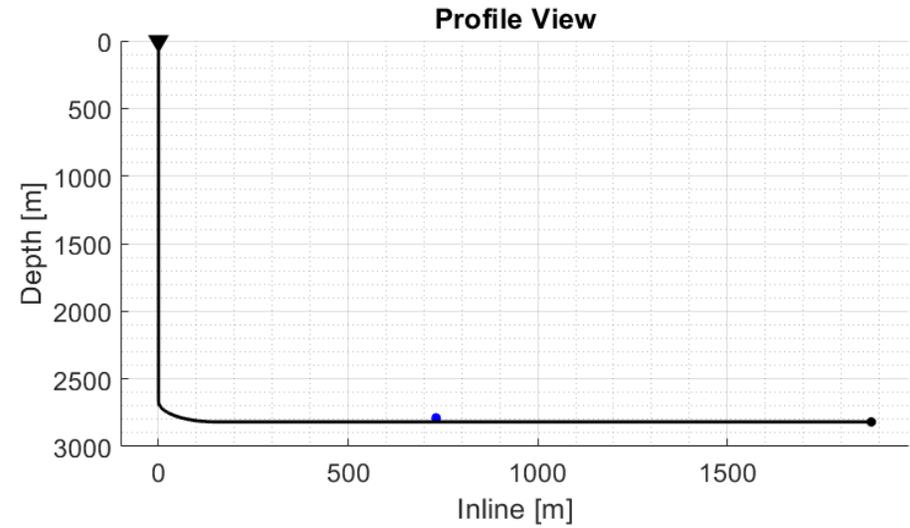
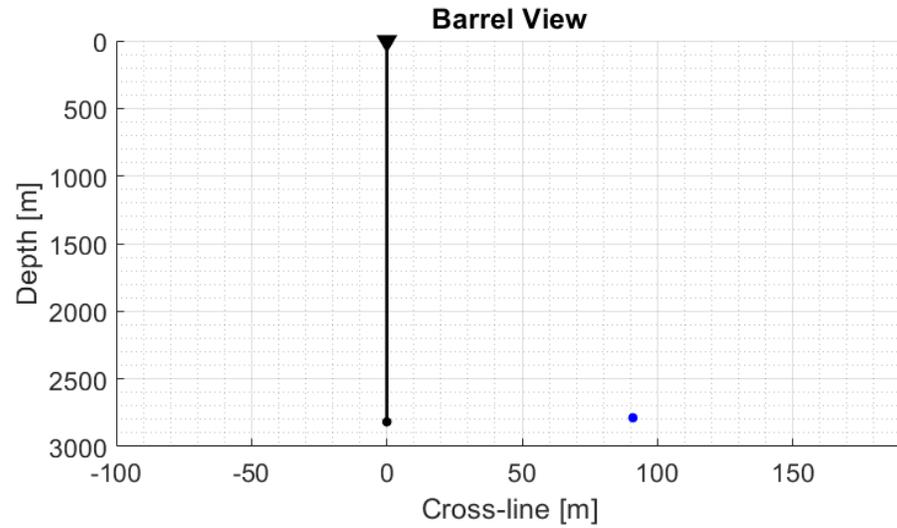




- Distinct differences in strain radiation patterns offer insight into source mechanics
- Shaping fibre can improve the sensitivity to the radiation patterns from more strain components



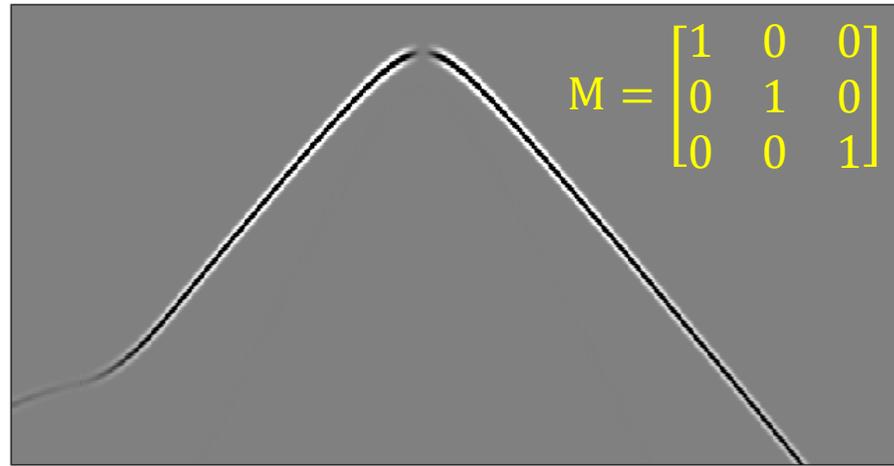
Experiment Geometry



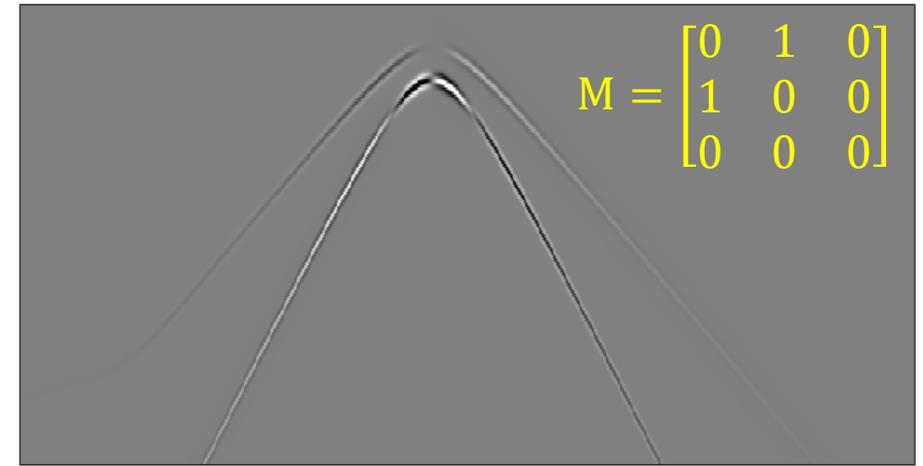


Analytic strain from 4 source types

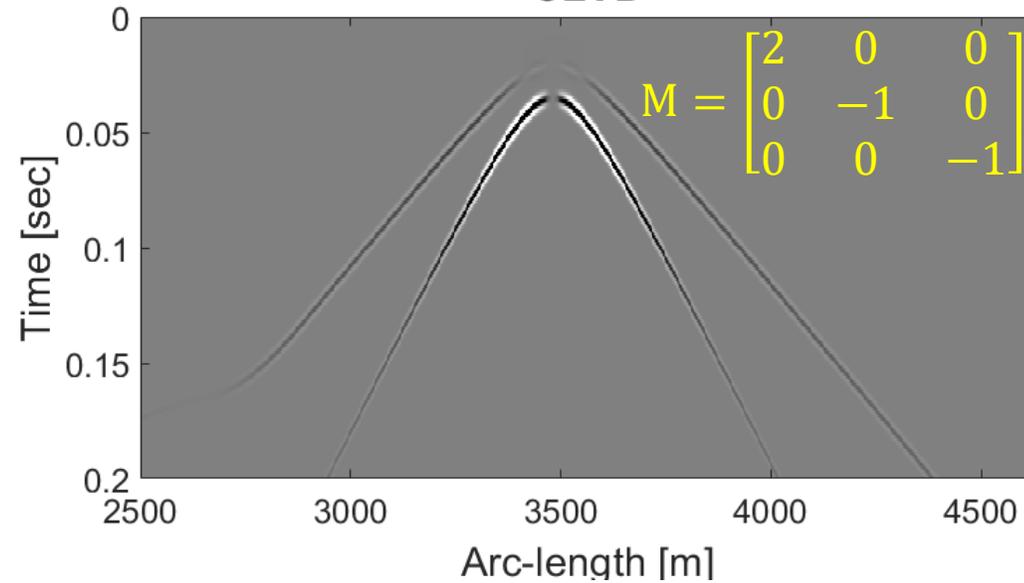
Explosive



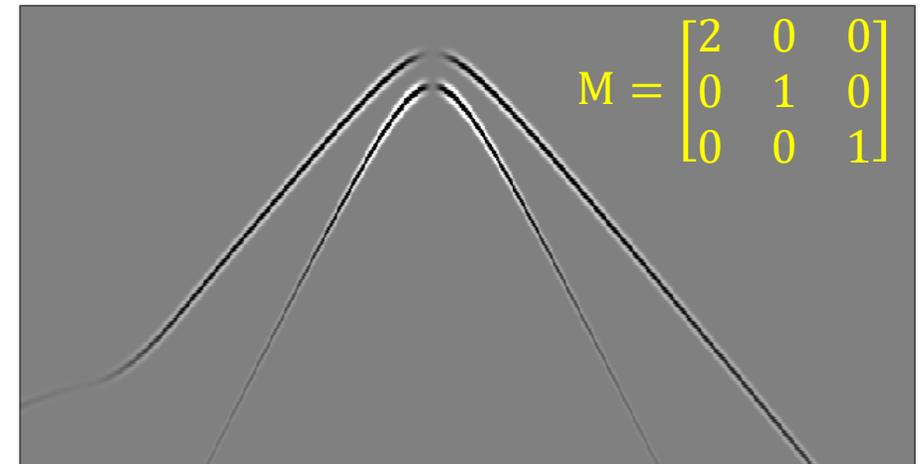
Double Couple



CLVD

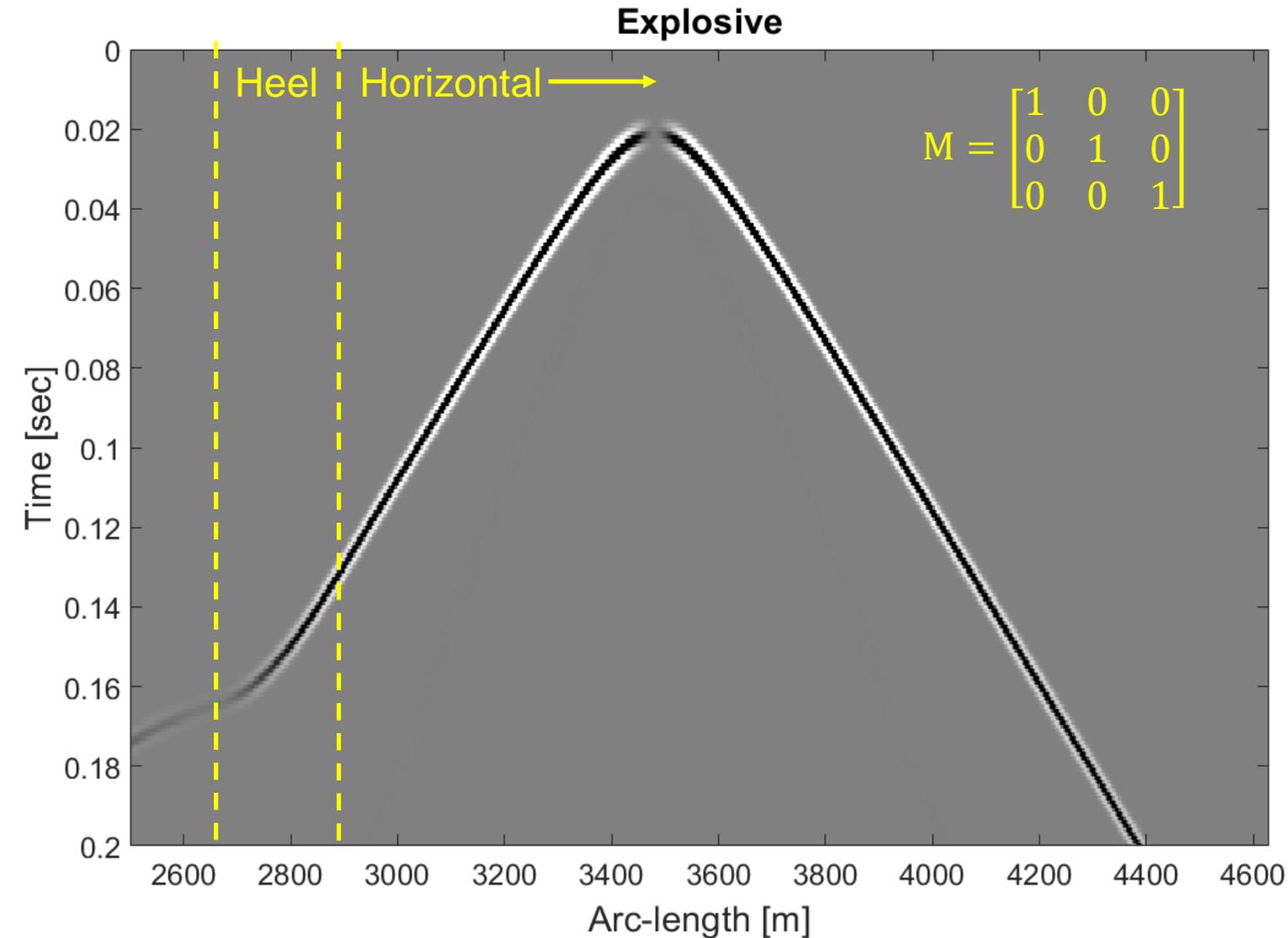


Tensile Crack

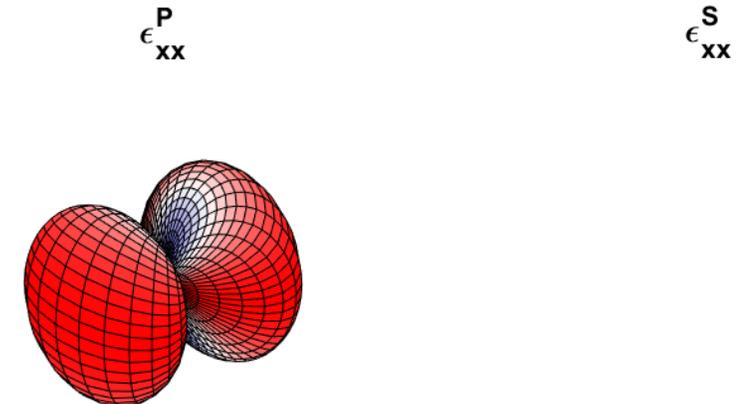




Explosive sources

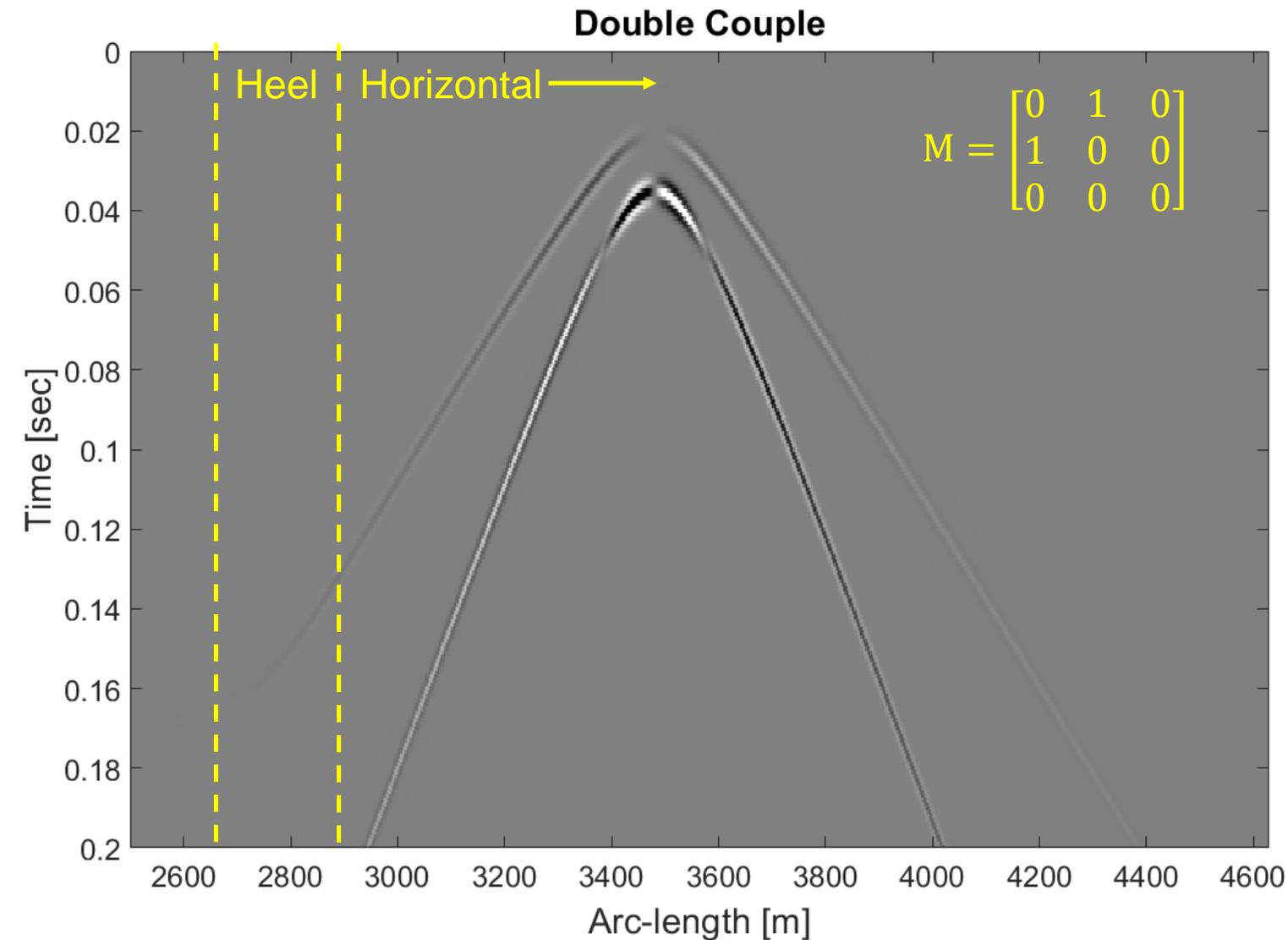


- Characterized by strong, symmetric P-wave and no S-wave
- Provides benchmark to test validity of this approach.

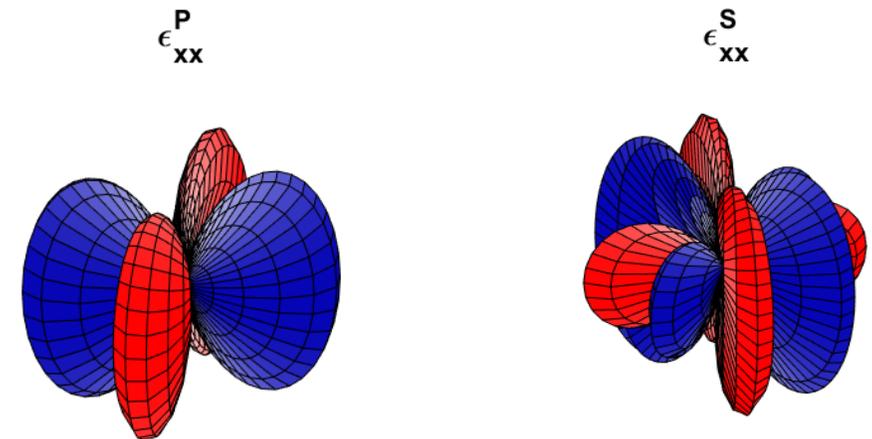




Double couple sources

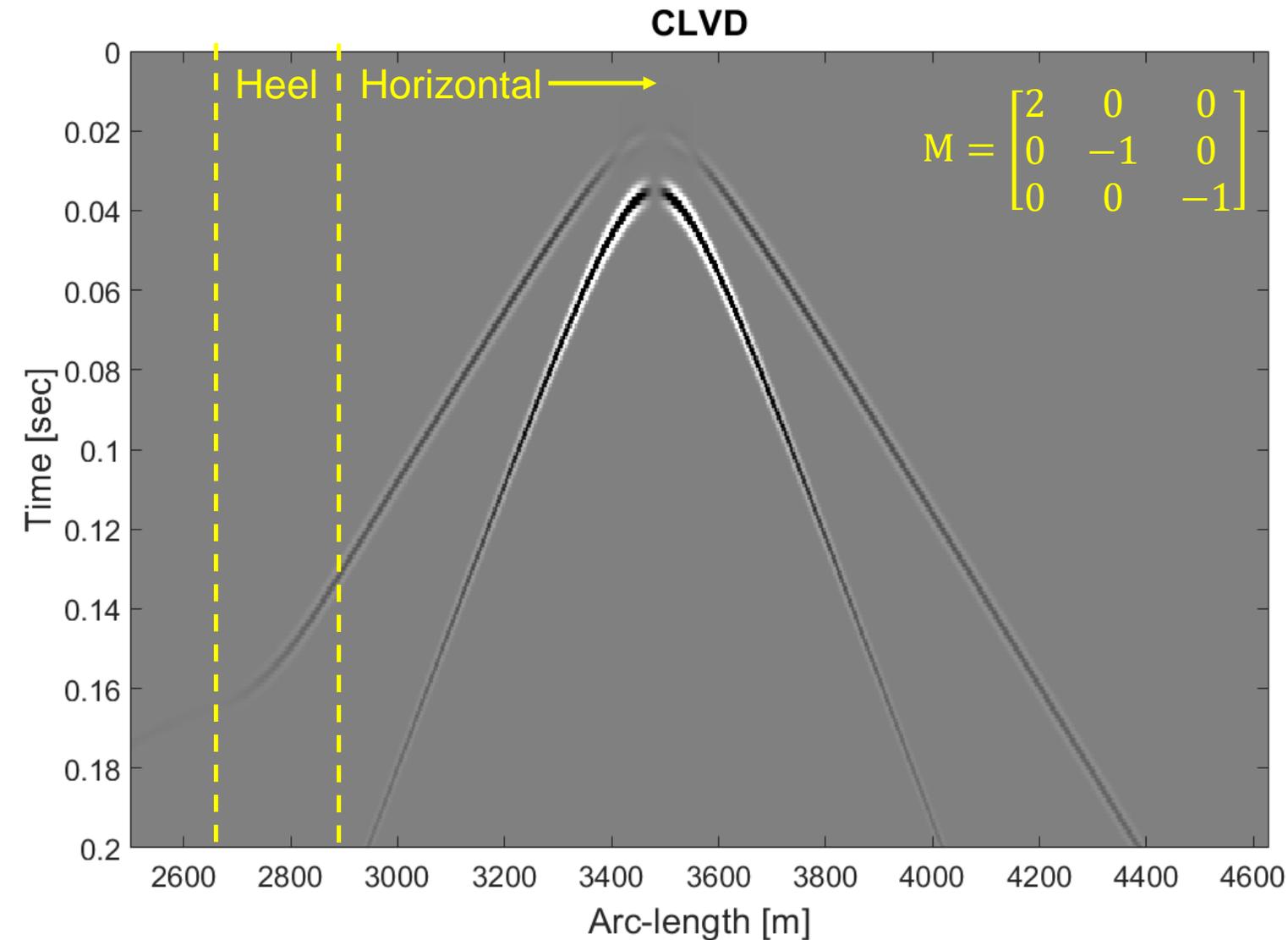


- Strong S/P wave amplitude ratio
- Polarity reversal in P-wave
- Distinct polarity pattern in S-wave

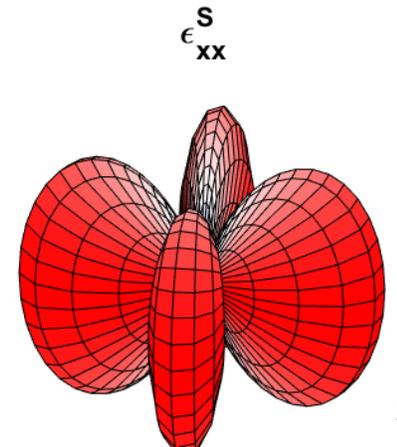
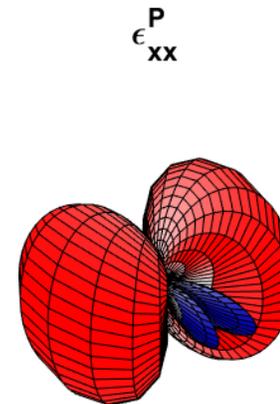




Compensated linear vector dipole sources

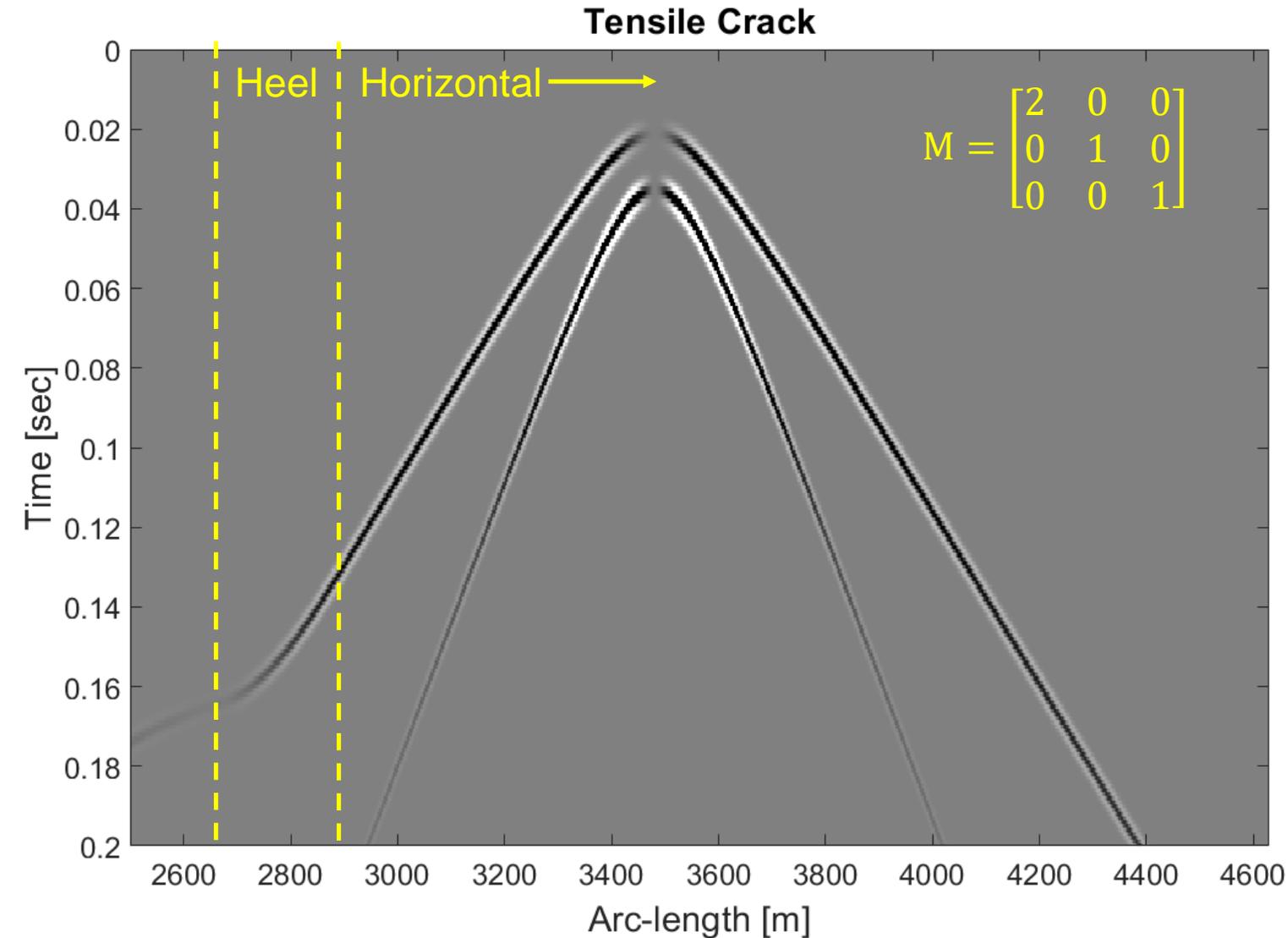


- Strong S/P wave amplitude ratio
- Near offset polarity reversal in P-wave
- Symmetric S-wave, same polarity as P-wave at long offset

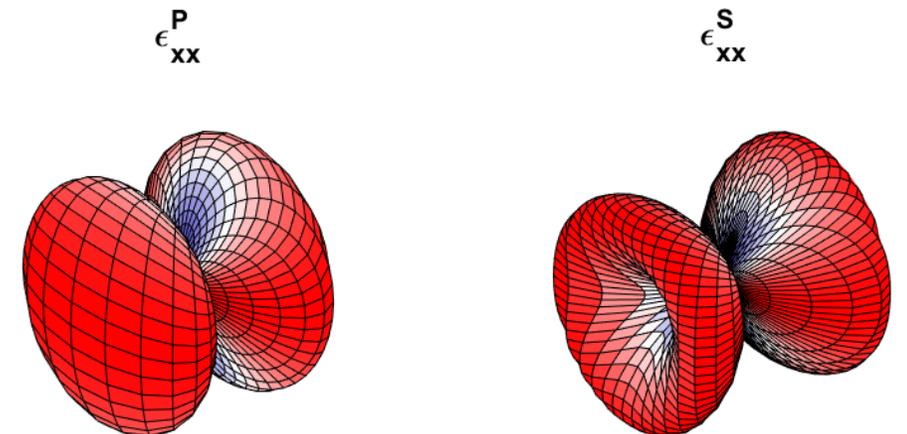




Tensile crack sources



- Balanced S/P wave amplitude ratio
- Symmetric P-wave
- Symmetric S-wave with same polarity as P-wave



- DAS provides a complementary dataset to geophones.
- Large sampling of solid angle, and close proximity to events makes DAS attractive.
- Developed a tool for the efficient appraisal of DAS and investigation of field data.
- Future work will look at using DAS data for moment tensor inversion.



- CREWES Industrial Sponsors
- NSERC (CRDPJ 461179-13)
- SEG Foundation
- CREWES Staff and Students